

HORNSBY SHIRE COUNCIL

ROCK MECHANICS STUDY

HORNSBY QUARRY
OLD MAN'S VALLEY

REPORT No S8463/4-AD MAY, 1990



Coffey & Partners Pty Ltd

Consulting Engineers
in the geotechnical sciences

C P Thorne,BE MEngSc FIEAust
B C Burnan,BE MEngSc PhD FIEAust MAIMM
I R Binch,DipCE MEngSc FIEAust
G K Spencer,BE MEngSc PhD MIEAust
P C Thomson
M G Philip,BE MEngSc MIEAust
T D Sullivan,BE MSc DIC MIEAust
J P MacGregor,BSc DIC MIEAust
P J N Pells,BScEng(M) MSc DIC
P J Hitchcox,ACIS MIAA AAM
J W A Gildea,AM BE MIEAust
Associates
J G Lucas,BE MIEAust
P G Redman,BE PhD MIEAust

Soil and rock engineering
engineering geology
groundwater hydrology
foundation engineering
mining geotechnics
dam engineering
computer applications
construction control & monitoring

COFFEY



Coffey & Partners Pty Ltd

your reference

our reference S8463/4-AD PLV:KMR
date 21st May, 1990

Consulting Engineers
in the geotechnical sciences

Incorporated in Queensland

12 Waterloo Road
North Ryde Sydney

PO Box 125
North Ryde New South Wales
Australia 2113

Fax (02) 888 9880
Telephone (02) 888 7444

The Shire Clerk
Hornsby Shire Council
296 Pacific Highway
HORNSBY NSW 2077

ATTENTION: MR. KEVIN SMITH

Dear Sir,

RE: ROCK MECHANICS STUDY - HORNSBY QUARRY, OLD MAN'S VALLEY

Please find enclosed 6 copies, as requested by Mr. W. Latham of our report on a rock mechanics study carried out at Hornsby Quarry, Old Man's Valley. This study was undertaken in conjunction with an extended geotechnical investigation of the Old Man's Valley proposed playing field development, the results of which will be reported separately.

Should you have any queries regarding this report please do not hesitate to contact Mr. Peter Volk or the undersigned.

For and on behalf of
COFFEY & PARTNERS PTY LTD

C.P. THORNE



Offices and NATA Registered Laboratories

Adelaide
Albury-Wodonga
Alstonville
Brisbane
Canberra
Darwin
Logan City
Melbourne
Newcastle
Perth
Sydney
Townsville
Wollongong
Rangoon, Burma
Mandalay, Burma

S8463/4-AD
21st May, 1990

2.



EXECUTIVE SUMMARY

Investigations in the vicinity of the proposed playing field development at Old Man's Valley by Coffey & Partners in 1989, concluded that additional investigations including a rock mechanics study be undertaken to further assess the stability of the eastern quarry area of the Hornsby breccia quarry.

As the toe of the proposed playing field development at Old Man's Valley will come to within 50m of the top of the present position of the eastern face of the quarry and would be within about 25m of the proposed final development profile, the stability of the quarry face is of major importance to the feasibility of the playing field development.

The aim of the rock mechanics study was to obtain additional structural data on the rock mass, both on the existing quarry face and on the rock mass behind the present face. Structural data on the quarry face was obtained by detailed line discontinuity mapping carried out along three benches. This data has been presented in the form of histograms and stereographic projections. The orientation and nature of major rock mass discontinuities beyond the eastern quarry face was investigated by three 90m, long fully cored oriented inclined boreholes.

The two boreholes located above the eastern face of the quarry confirmed that the attitude and inclination of basinal layering evident in the quarry face extends for a distance of at least 60m into the hillside. The orientation and the generally massive nature of the breccia in this area indicates that slope failure by planar sliding along bedding is unlikely. The prominent joint sets identified on the three line traverses on the quarry face were either not present or poorly developed in the rock mass behind the quarry face.

The borehole located near the south-eastern corner of the quarry indicated the presence of a broad 'transition' zone some 70m wide of material between breccia in the quarry and the Hawkesbury Sandstone. The orientation of defects and the nature of materials in this zone, is not considered to have an adverse impact on the proposed development.

In summary, the general combination of rock strength, structure and groundwater conditions in the vicinity of the Hornsby breccia quarry, is unlikely to result in an overall failure of the quarry slope, and therefore does not appear to be of general concern for the proposed development.

TABLE OF CONTENTS

	Page
EXECUTIVE SUMMARY	2
1.0 INTRODUCTION	4
2.0 PREVIOUS INVESTIGATIONS	4
3.0 RECENT INVESTIGATIONS	5
3.1 Investigation Drilling	5
3.2 Line Discontinuity Mapping	6
4.0 DESCRIPTION OF ROCK MASS	7
4.1 General	7
4.2 Lithology	7
4.3 Weathering	8
4.4 Permeability	9
4.5 Structure	9
4.5.1 Bedding	9
4.5.2 Joints	12
5.0 SLOPE STABILITY	13
6.0 CONCLUSIONS	14

References

Important Information about your Geotechnical Engineering Report

Appendix A - Borehole Logs

Appendix B - Stereographic Projections for Oriented Cored Boreholes

Appendix C - Data Histograms for Surface Line Mapping

Appendix D - Stereographic Projections for Surface Line Mapping

Appendix E - Tabulation of Bedding, Joint and Vein Orientations
- Cored Boreholes

Drawing No. S8463/4-1 - Plan of Defect Orientations

Drawing No. S8463/4-2 - Geological Cross-Sections

S8463/4-AD
21st May, 1990

4.



1.0 INTRODUCTION

This report presents the results of a rock mechanics study undertaken at the request of Hornsby Shire Council in the eastern area of the Hornsby breccia quarry. The purpose of the study was to supplement earlier preliminary investigations carried out in the area, the results of which were esented in Report No. S8463/2-AC, July 1989.

The work was undertaken in general accordance with our proposal for additional rock mechanics studies, as outlined in Appendix E of the above report. The work was commissioned by Hornsby Shire Council in a letter dated 4th October 1989.

As mentioned in previous reports, the toe of the proposed playing field development at Old Man's Valley will come to within 50m of the top of the present position of the eastern face of the quarry and would be within about 25m of the proposed final development profile for the eastern face. To further assess the stability of the eastern quarry area, the aim of the present rock mechanics study was to obtain additional structural data on the rock mass, both on the existing quarry face and on the rock mass behind the face.

2.0 Previous Investigations

In 1982, Golder & Associates (Golders) undertook a slope stability investigation of the eastern face of the Hornsby Breccia Quarry (Report No. 8267037A) for the Readymix Group. This investigation comprised the drilling of two vertical diamond drill holes, Bores G1 and G2, to 49.9m and 48.4m depth respectively. Bore G1 was located at RL41.5m near the then existing base of the quarry, and Bore G2 was located some 40m east of the top of the eastern face. The principal purpose of the drilling as outlined in Golders Preliminary Report No. 82627037 was to investigate the potential for slope failure on either a breccia/sandstone interface or alternatively along bedding or foliation planes. The report stated:

"The drilling has confirmed that synclinal bedding/foliation exists; the bedding slope being generally 5 to 10° in Bore G1 and about 50° in Bore G2. Only very few actual bedding/foliation discontinuities were observed and no fracturing along these planes was encountered. Bedding/foliation planes are therefore not considered to form a potential failure plane.

Complete joint orientation was not possible as core orienting equipment was not used during drilling of the vertical holes. Joint dip angles measured were variable however, the dominant angle of about 80° noted in Bore G1 agreed with the principal joint dip established from the joint survey of the eastern face above. The joints logged in Bore G2 indicate principal joint dips of 15 to 30° and 45 to 60°.

Most joint faces were calcite filled and no clay infilling was apparent thus indicating appreciable joint strength.

S8463/4-AD
21st May, 1990

5.



The generally moderately to widely spaced presence of jointing together with the indicated appreciable joint strength is considered to preclude failure of the slope through either a single or a series of intersecting joint planes".

Subsequent to the above investigations, Coffey & Partners Pty. Ltd. (CAP) undertook in 1989 a preliminary investigation of the quarry area which included some field mapping along creek lines and surface exposures in the area above the quarry, as well as limited geological mapping of joints and bedding exposed on the eastern quarry face. This information was presented in Report No. S8463/2-AC, July 1989 which concluded that; "On the basis of information available, Golder & Associates conclusions appears reasonable. In view of the possible ramifications if the quarry were to be extended, consideration should be given to implementing a rock mechanics study in conjunction with other work".

The present rock mechanics study was undertaken concurrently with additional geotechnical investigations being carried out in the vicinity of the Old Man's Valley playing fields, the results of which will be reported separately.

In addition to survey information previously supplied by Council for the preparation of Report No. S8463/2-AC, which was used in the preparation of this report, the following information was recently provided by Council:

- A 1:500 plan of Old Man's Valley Hornsby Site Details as at May 1989, (Drawn January 1990).
- A 1:1000 plan of Hornsby Quarry prepared by QASCO (NSW) Pty. Ltd., from aerial photography flown in February 1989, (Reference 14279).

The survey data included the location of boreholes and test pits. Other factual data supplied, including factual data in Golders report, has not been checked and this report relies on that data.

3.0 RECENT INVESTIGATIONS

3.1 Investigation Drilling

To further access the orientation and nature of major rock mass discontinuities in the quarry area, but more particularly beyond the eastern face of the quarry, recent investigations have included the drilling of three approximately 90m long, fully cored oriented inclined boreholes, namely 101, 102 and 103 (for location see Drawing No. S8463/4-1).

Boreholes 101 and 102, are located approximately 25 metres east of a point located midway along the top of the eastern quarry face. Both holes where inclined at 65° from the horizontal. Borehole 101 was oriented at 260°(magnetic) towards the quarry, whereas borehole 102 was oriented away from the quarry at approximately 80° (magnetic). The presence of a deeply

S8463/4-AD
21st May, 1990

6.



incised creek near the quarry's eastern boundary and the adjacent constantly used quarry haul road, reduced the scope for borehole site selection. As a result of these limitation, boreholes 101 and 102 were located adjacent to the quarry-playing fields access road on Council land and borehole 103 was located on a bench near the top of south-eastern corner of the quarry.

Borehole 103 was inclined at 65° from the horizontal and oriented at 142° (magnetic). This orientation was selected so as to maximise the intersection of known joint sets.

During the drilling of the boreholes core orientation was attempted at the completion of each drilling run. In areas of highly fractured rock, particularly in near surface layers in boreholes 101 and 103, core orientation was largely unsuccessful, however, in less fractured rock the technique was successful. Appendix E contains a listing of all recorded defect orientations including bedding planes, joints and veins for each of the boreholes.

3.2 Line Discontinuity Mapping

Detailed line discontinuity mapping has been carried out along three benches on the eastern quarry face. These traverses have been designated 1989/1, 1982/2 and 1989/3 and are located as shown on Drawing No. S8463/4-1. This line mapping is additional to earlier mapping, the results of which were presented in Report No. S8463/2-AC. The three traverses are located on benches at approximately RL90 (traverse 1989/1), approximately RL70 (traverse 1989/2) and approximately RL40 (traverse 1989/3).

Information gathered from the line discontinuity mapping includes the following data on defects:

- spacing,
- length,
- continuity,
- surface roughness,
- surface hardness,
- water condition and
- structural orientation.

This information has been summarised and is presented in Appendix C in histogram form for each of the three traverses. Stereographic projections are presented for each of the traverses in Appendix D. For each of the three traverses, separate histogram plots have been prepared for, the total of all defects, joints only and, bedding defects only.

The mean structural orientation of major defect sets and defect types are summarised in Table 1.

S8463/4-AD
21st May, 1990

7.



4.0 DESCRIPTION OF ROCK MASS

4.1 General

Hornsby Quarry, situated immediately west of the proposed filling at Old Man's Valley is sited within volcanic breccia, with the surrounding plateau area comprised of Hawkesbury Sandstone. The Sydney 1:100,000 Geological Series Sheet indicates that the quarry is located in the so called Hornsby Diatreme, which is dumbell shaped and elongate in a north-east/south-west direction for about 1.5km and generally less than 400m wide.

It is unknown whether the Hornsby Diatreme represents a single intrusion or a number of intrusions. As the dumbell shape alludes to the possibility of more than one intrusion, the number of intrusions, their relationships and effects on one another are unknown.

A diatreme can be defined as a pipe-like volcanic conduit filled with pyroclastic debris (tuff or lapilli tuff) and blocks of wall rock. Diatremes in the Sydney Basin are generally considered to have resulted from violent intrusions of molten magma into surrounding country rocks.

Drawing No. S8463/4-1 shows the interpolated boundary between the volcanic breccia of the diatreme and the Hawkesbury Sandstone. The location of this boundary has been assessed based on previous field mapping by CAP and on borehole information from past and present studies by CAP and Golders. The steepness of the boundary is uncertain. Crawford et al (Reference 2) has indicated that the boundary in other diatremes of the Sydney Basin is commonly characterised by steep sandstone walls.

The two inclined boreholes, 101 and 102 fully penetrated volcanic breccia, as did the boreholes G1 and G2 drilled by Golders. Borehole 103 however, unexpectedly intersected alternating bands of sandstone/siltstone and breccia from near the surface to a depth of about 75m, where undisturbed sedimentary rock is believed to have been intersected. The inferred orientation of the bedding, both within the breccia and the sandstone/siltstone blocks (?) appears to rapidly vary, both with rock type and depth. This geologically complex area, has been interpreted as representing a 'transition zone' between the relatively massive breccia exposed in the quarry and the undisturbed sandstone at the boundary of the diatreme. As shown on Drawing No. S8463/4-2, the 'transition zone' in the vicinity of borehole 103 may be up to 70m wide.

4.2 Lithology

The volcanic breccia at Hornsby is generally comprised of a heterogeneous mix of grey to grey-green angular to subrounded fragments of volcanic rock cemented within a fine grained dark grey tuffaceous matrix. As shown on the borehole logs, the breccia consists of bands of finer grained breccia interlayered with medium to coarse grained breccia. Within the coarser layers in particular, there is often a scattering of irregular to subrounded fragments of coal, siltstone and sandstone up to 180mm thick. In addition to the fragments of sedimentary rock within the breccia, clasts of dolerite were also noted, particularly in boreholes 101 and 102.

S8463/4-AD
21st May, 1990

8.



The presence of irregular to subrounded fragments of sedimentary rock and dolerite within the breccia, helps to confirm the violent intrusive nature of diatreme formation. In addition, within borehole 101 imbrication of breccia fragments indicates flow of molten magma.

Fragments of volcanic rock within the breccia mainly range from 1 to 10mm in size, although fragments up to 400mm were noted in outcrops. The fragment to matrix ratio generally ranges from about 70:30 to 40:60. Fragments of sedimentary rock within the breccia are more frequent in borehole 101 than in nearby borehole 102, further indicating the heterogeneous nature of the breccia.

Borehole 103 located within the 'transition-zone' near the margins of the diatreme, shows a high proportion of sedimentary rock fragments within the breccia bands with fragments of sandstone up to 180mm across.

Throughout the breccia there is irregular calite veining, as well as calate infillings along joints and bedding partings. The majority of the joints are coated with at least a veneer of calcite.

The breccia is generally of high to very high strength when fresh, with the finer grained breccia of slightly higher strength than the medium to coarse grained breccia.

4.3 Weathering

Boreholes 101 and 102 intersected what may be regarded as essentially fresh breccia below depths of about 12 to 13m. In borehole 101, a number of iron-stained joints were intersected to a depth of 65.8m, whereas in borehole 102 which was drilled away from the quarry, the number of iron-stained joints were considerably fewer with the deepest iron-stained joint intersected at a depth of about 32m.

In borehole 101 a number of iron-stained joints had associated narrow bands of slightly weathered breccia and these have been designated as slightly weathered bands on the borehole logs. However, as mentioned above, the rock mass below about 13m may generally be regarded as fresh, with iron-stained joints.

Borehole 103 located above the south-eastern corner of the quarry intersected essentially fresh sandstone from about 12m. The base of extremely to moderately weathered sandstone and breccia occurs at about 9m.

On the eastern quarry face, the approximate boundary between the variably weathered breccia and the underlying essentially fresh breccia occurs along or near the bench located at RL90m.



4.4 Permeability

Although no water pressure testing or other permeability testing as such was carried out during the investigation, the losses of drill water during drilling give some indication as to the permeability characteristics of the rock mass. During the drilling of borehole 101, a number of highly fractured zones were intersected in which complete drill water loss was experienced. These conditions were unexpected and were not apparent from previously available subsurface data. Complete drill water losses were recorded on fourteen occasions during the drilling of borehole 101, with the majority of the losses recorded in the upper half of the hole. For precise locations see the borehole logs in Appendix A. When complete drill water losses were experienced, the hole was cemented. Partial drill water losses were also recorded at twelve locations most of which are in the upper half of the hole.

In comparison with borehole 101, borehole 102 recorded complete drill water losses on only three occasions, at depths 10.3m, 17.0m and 65.5m with only one partial drill water loss at 58.9m. Borehole 103 did not experience any noticeable losses of drill water over its full length.

In summary, it appears that the rock mass in the vicinity of borehole 101, which is located nearest to the quarry face, has a number of highly permeable fractured zones. The permeability of these zones may have increased as a result of the opening up of fractures either from the relief of stresses associated with excavation or from blasting.

Observation of the upper three benches of the eastern quarry face (down to approximately RL40m) did not reveal any significant zones of seepage which indicate that water levels in the adjacent breccia may have been effectively drawn down to near quarry floor level. Observation of piezometric levels in boreholes in the vicinity of Councils playing fields support this view, with water levels in some boreholes at depths greater than 50m.

4.5 Structure

4.5.1 Bedding

Within Hornsby Quarry the volcanic breccia of the Hornsby Diatreme shows a particularly well defined basinal layering. This is particularly evident on the eastern face of the quarry where the strata dips steeply to the south-east on the northern half of the face, flattening out to almost horizontal in the central area before steepening on the southern face where the dip is to the north-east.

S8463/4-AD
21st May, 1990

10.



The results of the mapping of bedding planes, particularly along Line Mapping Traverses 1989/1, 1989/2 and 1989/3 is shown on Drawing No. S8463/4-1. The mapping indicates that the dip of the bedding planes in the quarry ranges from less than 10° up to 75° . As shown on the stereographic plots for bedding presented in Appendix D, the bedding orientations generally plot along an arc, reflecting the basinal layering in the breccia. Beds in the northern half of the quarry face mostly dip towards the east-south-east at about 8° to 32° whereas beds on the southern half of the quarry face mostly dip towards the north-east at about 15 to 25° . Towards the centre of the eastern quarry face, the number of bedding plane intersections were fewer on each of the traverses, but more particularly on Traverse 1989/3. This was in part due to the massive nature of the breccia in these locations.

The data histograms for the three line mapping traverses presented in Appendix C, indicates that the majority of bedding partings were 6 to 20m in length discrete to semi-continuous, with ridges and stained. The increase in spacing between bedding measurements for traverses 1989/1 and 2 and 1989/3 is however, largely the result of coarser screening applied to traverse 1989/3.

Towards the south-east corner of the quarry, particularly in the area below borehole 103, the breccia appears to be more massive than elsewhere in the quarry. The relatively few bedding planes in this area may either indicate the presence of a thick breccia layer conformable with the strata in the remainder of the quarry, or alternatively, it may represent the northern extremity of the 'transition zone' shown on Drawing No. S8463/4-2.

Bedding or foliation was generally indistinct in much of the breccia intersected in inclined cored boreholes 101 and 102. Appendix E presents a tabulation of bedding plane orientations obtained by core orientation. As shown, relatively few measurements were obtained and the results show a surprisingly wide scatter of orientations. Bedding planes measured in borehole 101 below depths of 58m, generally indicated dip directions to the south, south-west and west at angles ranging from 5° to 29° . These orientations appear to conflict with the relatively consistent trends shown on the line mapping traverses which are located a distance of 40m to the west, and with the bedding angles recorded in borehole G1.

S8463/4-AD
21st May, 1990

11.



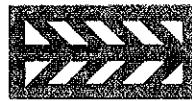
TABLE 1
SUMMARY OF MAJOR DEFECT SET ORIENTATIONS

DATA SOURCE	DEFECT TYPE	DEFECT SET	MEAN ORIENTATION	
			DIP (deg)	DIP DIRECTION (deg)
Line Mapping Traverse 1989/1	J	A	80	265
	J	B	85	167
	J	C	75	234
	B	D	8	108
	B	D'	25	032
Line Mapping Traverse 1989/2	J	A	82	274
	J	B	80	203
	J	C	80	245
	B	D	32	160
	B	D'	15	043
Line Mapping Traverse 1989/3	J	A	82	268
	J	B	83	168
	J		84	254
	B	D	11	094
Borehole 101	J	B(?)	65	145
	J	E	84	060
	J		80	015
	B		9	205
	V	E	73	055
Borehole 102	J	F	35	340
	J		34	026
	J	A(?)	54	267
	B		23	012
	V	F	44	320
Borehole 103	J	F	55	348
	B		10	108

J - Joint
 B - Bedding
 V - Vein

S8463/4-AD
21st May, 1990

12.



Bedding plane orientations obtained in borehole 102 show relatively consistent trends, with dips to the north-east and south-east (i.e. into the hillside) at angles ranging from 8° to 28° . These orientations appear consistent with measurements obtained for the three line mapping traverses and they indicate that for at least the upper 25m of borehole 102, the orientation of the bedding is away from the quarry.

Previous investigations by Golders indicated that in borehole G2 below depths of about 30m, bedding plane dips of 48° and 50° were noted. No evidence of such high angle bedding was noted in boreholes 101 or 102. In addition, these boreholes were generally indistinctly bedded with very few bedding plane partings.

4.5.2 Jointing

Line mapping along three benches on the eastern quarry face, namely Traverses 1989/1, 2 and 3 has confirmed the existence of two major joint sets identified during previous studies. As shown on the stereographic plots presented in Appendix D and as summarised in Table 1, the principal joint set (designated defect set A) dips at 82° with a dip direction of 270° . The minor joint set (designated defect set B) is also steeply dipping at about 83° , with a dip direction of about 180° . In addition to these orthogonal joint sets, a subordinate joint set (defect set C) steeply dipping at 80° , with a dip direction of 245° was identified on Traverse 1989/2. This subordinate joint set was also present on Traverses 1989/1 and 3 but was not as pronounced.

Observations of the lower benches below Traverse 1989/3 on the eastern quarry face indicated similar joint orientations to those outlined above. Observations of defect set A indicated a spacing between joints typically ranging from 0.6m to 2m. Defect set B has a similar spacing between joints to set A and are distinctive in outcrop. Towards the lower central part of the quarry, a number of the more continuous joints belonging to defect set B were points of minor seepages.

Throughout the quarry and in the three boreholes the majority of the joints were planar and rough and either clean or coated/infilled with calcite. Borehole 101 had a number of limonite stained joints to a depth of 65.8m, but in general the majority of the joints were planar, rough and calcite coated.

Joint sets identified in each of the three boreholes did not show any consistent pattern, compared with the joint sets identified in the line mapping. The steeply dipping orthogonal sets identified on the eastern quarry face were not present in the boreholes.

In borehole 101 the major joint set may reflect defect set B identified on the quarry face and in borehole 102 the third largest joint set may reflect joint set A, however, these correlations may be just coincidental. Contrasting with the above, borehole 102 identified two major relatively shallow dipping joint sets with dip angles of 34° and 35° and dip

S8463/4-AD
21st May, 1990

13.



directions of 340° and 026°, respectively. These low angle joints did not appear to be well developed in the quarry face, which indicates that either they were masked by other rock mass defects or alternatively the orientation of defects in the vicinity of borehole 102 is different to that of the defects on the quarry face.

As very few joint measurements were made in borehole 103, it is difficult to obtain a reliable picture of the jointing in the area, however, from the few measurements it appears that joints in the sandstone dip to the north-north-west at an angle of about 55°.

The orientation of the calcite veins as measured in boreholes 101 and 102 have as expected a general tendency to parallel the major joint directions.

5.0 SLOPE STABILITY

The bedding planes within the breccia, which reflect basinal layering, are potential planes of weakness within the rock mass. In the past, a number of planar slope failures have taken place along these bedding planes, as evidenced by the extensive 65° face on the southern side of the quarry. A smaller number of minor planar slope failures, also along bedding planes have occurred on the northern quarry face. Therefore, the orientation of bedding in the eastern quarry area near the toe of the proposed playing field development is critical in the overall assessment of slope stability.

As mentioned in Section 4.5.1 the bedding plane orientations measured in the upper parts of borehole 102 are consistent with the measurements obtained from the line mapping, that is, they dip away from the quarry. The bedding in this area is therefore considered to be favourably oriented with respect to possible bedding plane failures. In addition, the generally massive nature of the breccia in the area behind the present quarry face further indicates that slope failure by planar sliding along bedding is unlikely.

The wide variation in bedding orientations recorded below depths of 58m in borehole 101 may represent a discrete contorted zone which was not apparent in nearby Line Mapping Traverse 1989/3 or in borehole G1. As this possible zone occurs well below the proposed development, and set back some distance from the quarry face, it is not considered to have an adverse impact on the overall stability of the slope.

Line mapping confirmed the presence of orthogonal joint sets in the quarry, with the major set striking north-south, dipping 80° west and the minor set striking east-west and dipping 83° south.

As shown on Drawing Nos. S8463/4-1 and 2, the breccia/sandstone contact is believed to pass along or near to the southern boundary of the present quarry. Borehole 103 is located in a highly variable 'transition zone' between the relatively massive breccia in the quarry and the undisturbed sandstone at the boundary of the diatreme. The strength of the siltstones, silty sandstones and sandstone within the breccia in this 'transition zone' vary from very low to high, whereas the breccia itself is generally of high



strength. No reliable bedding or joint orientations were obtained in borehole 103 above the breccia/sandstone contact at 75m. Below 75m, the joints appear to be dipping at angles of about 70° with dip directions between 331° and 009° . Should the joints in the "transition zone" be of a similar orientation to those in the intact sandstone, then the jointing within the 'transition zone' is considered to be oriented favourably with respect to possible failure of the slope below the proposed development.

As most joint faces within the breccia are planar, rough and calcite coated, with little or no clay infillings, the rock mass could be expected to have appreciable joint strengths. In addition, as the spacing between joints and bedding plane defects is generally moderately to widely spaced, failure of the slope through either a discrete defect plane or a series of intersecting defects is highly unlikely.

The eastern quarry face appears to be well drained in that no significant areas of groundwater seepage were observed on the quarry face down to about RL40. Below this depth a number of joints, belonging to defect set B show signs of minor seepage. This conclusion is supported in that boreholes located in the playing field area above the quarry have piezometric levels up to 50m below the surface.

The proposed filling is unlikely to significantly load the quarry face as it now stands, nor is it likely to adversely affect groundwater conditions behind the face. The installation of drainage measures in and around the proposed playing field development will limit the amount of water entering the slope.

6.0 SUMMARY AND CONCLUSIONS

The recent investigations into the stability of the eastern quarry area in the vicinity of the proposed playing field development has identified the following major features:

- A broad 'transition zone' some 70m wide located along the southern side of the quarry believed to be comprised of a chaotic mix of sedimentary blocks and volcanic breccia. Jointing in this area is believed to be steeply dipping to the north.
- A general continuation of the bedding/basinal layering orientation as observed on the central area of the eastern quarry face for at least 60m eastwards into the hillside and for at least the upper 50m of the present quarry.
- Major joint sets identified on the eastern quarry face were either not present or poorly defined in the area beyond the existing quarry face.
- The eastern quarry face and adjacent rock mass appears to be well drained.

S8463/4-AD
21st May, 1990

15.



As the proposed playing field development is unlikely to significantly load the quarry face as it now stands, and with the general combination of rock strength, structure and groundwater conditions, the overall failure of the quarry slope does not appear to be of general concern for the proposed development.

Provided any future blasting adjacent to the final quarry outline is designed to produce sound slopes with minimal blast induced fractures then the above information indicates that the eastern quarry face should remain stable to the depths and at the slopes proposed.

[Handwritten signature]
For and on behalf of
COFFEY & PARTNERS PTY LTD

REFERENCES

1. Coffey & Partners Pty. Ltd., Hornsby Shire Council. Report on Proposed Filling Old Man's Valley, Hornsby. Report No. S8463/2-AC, July 1989.
2. Crawford et al "Diatremes of the Sydney Basin in A Guide to the Sydney Basin", Geological Survey of NSW, Bulletin No. 26, 1980.
3. Golder Associates Pty. Ltd, 'Supplementary Report to the Readymix Group on Slope Stability Study, Eastern Face, Hornsby Quarry. Report No. 8267037A, August 1982.

IMPORTANT INFORMATION ABOUT YOUR GEOTECHNICAL ENGINEERING REPORT

More construction problems are caused by site subsurface conditions than any other factor. As troublesome as subsurface problems can be, their frequency and extent have been lessened considerably in recent years, due in large measure to programs and publications of ASFE/The Association of Engineering Firms Practicing in the Geosciences.

The following suggestions and observations are offered to help you reduce the geotechnical-related delays, cost-overruns and other costly headaches that can occur during a construction project.

A GEOTECHNICAL ENGINEERING REPORT IS BASED ON A UNIQUE SET OF PROJECT-SPECIFIC FACTORS

A geotechnical engineering report is based on a subsurface exploration plan designed to incorporate a unique set of project-specific factors. These typically include: the general nature of the structure involved, its size and configuration; the location of the structure on the site and its orientation; physical concomitants such as access roads, parking lots, and underground utilities, and the level of additional risk which the client assumed by virtue of limitations imposed upon the exploratory program. To help avoid costly problems, consult the geotechnical engineer to determine how any factors which change subsequent to the date of the report may affect its recommendations.

Unless your consulting geotechnical engineer indicates otherwise, *your geotechnical engineering report should not be used:*

- When the nature of the proposed structure is changed, for example, if an office building will be erected instead of a parking garage, or if a refrigerated warehouse will be built instead of an unrefrigerated one;
- when the size or configuration of the proposed structure is altered;
- when the location or orientation of the proposed structure is modified;
- when there is a change of ownership, or
- for application to an adjacent site.

Geotechnical engineers cannot accept responsibility for problems which may develop if they are not consulted after factors considered in their report's development have changed.

MOST GEOTECHNICAL "FINDINGS" ARE PROFESSIONAL ESTIMATES

Site exploration identifies actual subsurface conditions only at those points where samples are taken, when they are taken. Data derived through sampling and subsequent laboratory testing are extrapolated by geo-

technical engineers who then render an opinion about overall subsurface conditions, their likely reaction to proposed construction activity, and appropriate foundation design. Even under optimal circumstances actual conditions may differ from those inferred to exist, because no geotechnical engineer, no matter how qualified, and no subsurface exploration program, no matter how comprehensive, can reveal what is hidden by earth, rock and time. The actual interface between materials may be far more gradual or abrupt than a report indicates. Actual conditions in areas not sampled may differ from predictions. *Nothing can be done to prevent the unanticipated, but steps can be taken to help minimize their impact.* For this reason, most experienced owners retain their geotechnical consultants through the construction stage, to identify variances, conduct additional tests which may be needed, and to recommend solutions to problems encountered on site.

SUBSURFACE CONDITIONS CAN CHANGE

Subsurface conditions may be modified by constantly-changing natural forces. Because a geotechnical engineering report is based on conditions which existed at the time of subsurface exploration, *construction decisions should not be based on a geotechnical engineering report whose adequacy may have been affected by time.* Speak with the geotechnical consultant to learn if additional tests are advisable before construction starts.

Construction operations at or adjacent to the site and natural events such as floods, earthquakes or groundwater fluctuations may also affect subsurface conditions and, thus, the continuing adequacy of a geotechnical report. The geotechnical engineer should be kept apprised of any such events, and should be consulted to determine if additional tests are necessary.

GEOTECHNICAL SERVICES ARE PERFORMED FOR SPECIFIC PURPOSES AND PERSONS

Geotechnical engineers' reports are prepared to meet the specific needs of specific individuals. A report prepared for a consulting civil engineer may not be adequate for a construction contractor, or even some other consulting civil engineer. Unless indicated otherwise, this report was prepared expressly for the client involved and expressly for purposes indicated by the client. Use by any other persons for any purpose, or by the client for a different purpose, may result in problems. *No individual other than the client should apply this report for its intended purpose without first conferring with the geotechnical engineer. No person should apply this report for any purpose other than that originally contemplated without first conferring with the geotechnical engineer.*

A GEOTECHNICAL ENGINEERING REPORT IS SUBJECT TO MISINTERPRETATION

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a geotechnical engineering report. To help avoid these problems, the geotechnical engineer should be retained to work with other appropriate design professionals to explain relevant geotechnical findings and to review the adequacy of their plans and specifications relative to geotechnical issues.

BORING LOGS SHOULD NOT BE SEPARATED FROM THE ENGINEERING REPORT *

Final boring logs are developed by geotechnical engineers based upon their interpretation of field logs (assembled by site personnel) and laboratory evaluation of field samples. Only final boring logs customarily are included in geotechnical engineering reports. *These logs should not under any circumstances be redrawn* for inclusion in architectural or other design drawings, because drafters may commit errors or omissions in the transfer process. Although photographic reproduction eliminates this problem, it does nothing to minimize the possibility of contractors misinterpreting the logs during bid preparation. When this occurs, delays, disputes and unanticipated costs are the all-too-frequent result.

To minimize the likelihood of boring log misinterpretation, give contractors ready access to the complete geotechnical engineering report prepared or authorized for their use. Those who do not provide such access may proceed un-

der the *mistaken* impression that simply disclaiming responsibility for the accuracy of subsurface information always insulates them from attendant liability. Providing the best available information to contractors helps prevent costly construction problems and the adversarial attitudes which aggravate them to disproportionate scale.

READ RESPONSIBILITY CLAUSES CLOSELY

Because geotechnical engineering is based extensively on judgment and opinion, it is far less exact than other design disciplines. This situation has resulted in wholly unwarranted claims being lodged against geotechnical consultants. To help prevent this problem, geotechnical engineers have developed model clauses for use in written transmittals. These are *not* exculpatory clauses designed to foist geotechnical engineers' liabilities onto someone else. Rather, they are definitive clauses which identify where geotechnical engineers' responsibilities begin and end. Their use helps all parties involved recognize their individual responsibilities and take appropriate action. Some of these definitive clauses are likely to appear in your geotechnical engineering report, and you are encouraged to read them closely. Your geotechnical engineer will be pleased to give full and frank answers to your questions.

OTHER STEPS YOU CAN TAKE TO REDUCE RISK

Your consulting geotechnical engineer will be pleased to discuss other techniques which can be employed to mitigate risk. In addition, ASFE has developed a variety of materials which may be beneficial. Contact ASFE for a complimentary copy of its publications directory.

* For further information on this aspect reference should be made to "Guidelines for the Provision of Geotechnical Information in Construction Contracts" published by The Institution of Engineers Australia, National Headquarters, Canberra, 1987.

Published by



8811 Colesville Road/Suite G106/Silver Spring, Maryland 20910/(301) 565-2733

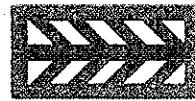
Reprinted by Coffey & Partners Pty Ltd. 1989

0788/3M



APPENDIX A

S8463/4-AD
3rd April, 1990



APPENDIX A

BOREHOLE LOGS

descriptive terms soil and rock

SOIL DESCRIPTIONS

Classification of Material based on Unified Classification System (refer SAA Site Investigation Code AS1726-1975 Add. No. 1 Table D1).

Moisture Condition based on appearance of soil

dry	Looks and feels dry; cohesive soils usually hard, powdery or friable, granular soils run freely through hands.
moist	Soil feels cool, darkened in colour; cohesive soils usually weakened by moisture, granular soils tend to cohere, but one gets no free water on hands on remoulding.
wet	Soil feels cool, darkened in colour; cohesive soils weakened, granular soils tend to cohere, free water collects on hands when remoulding.

Consistency based on unconfined compressive strength (Qu) (generally estimated or measured by hand penetrometer)

term	very soft	soft	firm	stiff	very stiff	hard
Qu kPa	25	50	100	200	400	

If soil crumbles on test without meaningful result, it is described as **friable**.

Density Index (generally estimated or based on penetrometer results).

term	very loose	loose	medium dense	dense	very dense
density index ID %	15	35	65	85	

ROCK DESCRIPTIONS

Weathering based on visual assessment

term	criterion
Fresh:	Rock substance unaffected by weathering.
Slightly Weathered:	Rock substance affected by weathering to the extent that partial staining or partial discolouration of the rock substance usually by limonite has taken place. The colour and texture of the fresh rock is recognisable; strength properties are essentially those of the fresh rock substance.
Moderately Weathered:	Rock substance affected by weathering to the extent that staining extends throughout whole of the rock substance and the original colour of the fresh rock is no longer recognisable.
Highly Weathered:	Rock substance affected by weathering to the extent that limonite staining or bleaching affects the whole of the rock substance and signs of chemical or physical decomposition of individual minerals are usually evident. Porosity and strength may be increased or decreased when compared to the fresh rock substance, usually as a result of the leaching or deposition of iron. The colour and strength of the original fresh rock substance is no longer recognisable.
Extremely Weathered:	Rock substance affected by weathering to the extent that the rock exhibits soil properties - i.e. it can be remoulded and can be classified according to the Unified Classification System, but the texture of the original rock is still evident.

Strength based on point load strength index, corrected to 50 mm diameter - $I_{50}(50)$ (refer I.S.R.M., Commission on Standardisation of Laboratory and Field Tests, Suggested Methods for Determining the Uniaxial Compressive Strength of Rock Materials and the Point Load Strength Index, Committee on Laboratory Tests Document No. 1). (Generally estimated: x indicates test result).

classification	extremely low	very low	low	medium	high	very high	extremely high
I_{50} MPa	0.03	0.1	0.3	1	3	10	

The unconfined compressive strength is typically about $20 \times I_{50}$ but the multiplier may range, for different rock types, from as low as 4 to as high as 30.

Defect Spacing

classification	extremely close	very close	close	medium	wide	very wide	extremely wide
spacing m	0.03	0.1	0.3	1	3	10	

Defect description uses terms contained on AS1726 table D2 to describe nature of defect (fault, joint, crushed zone, clay seam (etc.) and character (roughness, extent, coating etc.).

graphic symbols soil and rock

SOIL



- Asphaltic Concrete or Hotmix
- Concrete
- Topsoil
- Fill
- Peat, Organic Clays and Silts (Pt, OL, OH)
- Clay (CL, CH)
- Silt (ML, MH)
- Sandy Clay (CL, CH)
- Silty Clay (CL, CH)



- Gravelly Clay (CL, CH)
- Sandy Silt (ML)
- Clayey Sand (SC)
- Silty Sand (SM)
- Sand (SP, SW)
- Clayey Gravel (GC)
- Silty Gravel (GM)
- Gravel (GP, GW)

ROCK



- Claystone (massive)
- Siltstone (massive)
- Shale (laminated)
- Sandstone (undifferentiated)
- Sandstone, fine grained
- Sandstone, coarse grained
- Conglomerate



- Limestone
- Coal
- Dolerite, Basalt
- Tuff
- Porphyry
- Granite
- Pegmatite



- Schist
- Gneiss
- Quartzite
- Talus
- Alluvium

SEAMS

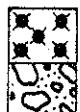


- Seam >0.1 m thick
(on a scale 1:50)
- Seam 0.01 m to 0.1 m thick
(on a scale 1:50)

INCLUSIONS (Special purposes only)



- Rock Fragments
- Swamp

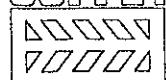


- Ironstone Gravel, Laterite
- Shale Breccia in Sandstone

Water Level



Surfaces ————— Known Boundary ————— Probable Boundary ————— ? ————— ? Possible Boundary



engineering log - borehole

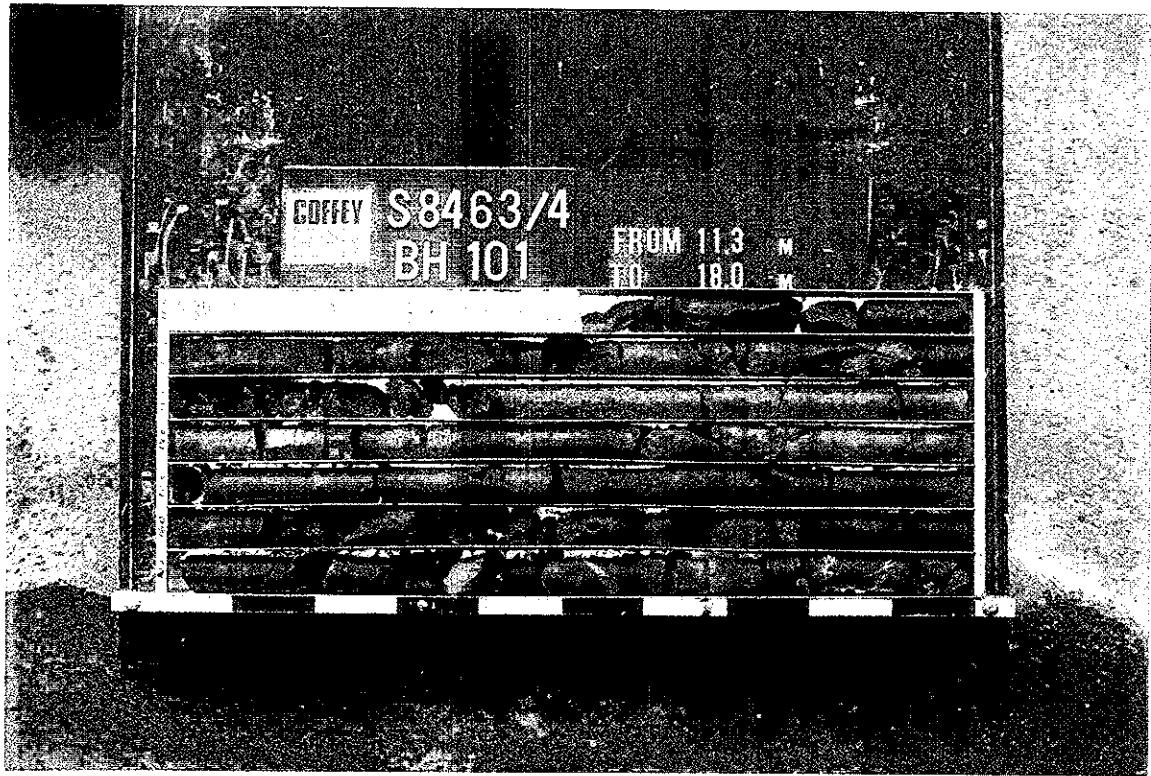
HORNSBY SHIRE COUNCIL								slope: -65 DEG R.L.Surface: 102.9 m			
OLD MANS VALLEY								bearing: 260. datum: AHD			
drill model and mounting: PIONEER B40											
borehole location: E 308518.10 N 1269889.83											
method 1 2 3	penetration support	water	notes samples, test,etc	R.L. metres	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics colour, secondary and minor components	moisture condition	consistency/ density index	structure and additional observations
R		C					CL	FILL: CLAY: medium plasticity, red brown sand & gravel, fine to coarse grained	M	100 200 300 400	FILL, contains breccia boulders
				102	1						
				101	2						
				100	3						
				99	4		CL	GRAVELLY CLAY: medium plasticity, yellow brown gravel & sand, fine to coarse grained			RESIDUAL(?)
				98	5						
				97	6		GC	CLAYEY GRAVEL: fine to coarse grained, grey brown, sand fine to coarse grained, & clay			EW BRECCIA(?)
				96	7						
				95	8						
METHOD		SUPPORT		NOTES samples and tests		CLASSIFICATION SYMBOLS AND SOIL DESCRIPTION		CONSISTENCY/DENSITY INDEX			
AS	auger screwing*	C	casing	U50	undisturbed sample 50 mm diameter	D	disturbed sample	VS	very soft		
AD	auger drilling*	M	mud	N	standard penetration test:	S	soft				
R	roller/Itricone	N*	SPT + sample recovered	Nc	SPT with solid cone	F	firm				
W	washbore	V	vane shear	V	vane shear	SI	stiff				
CT	cable tool	P	pressumeter	P	pressumeter	VSI	very stiff				
HA	hand auger	Bs	bulk sample	Bs	bulk sample	H	hard				
DT	diafuge	R	refusal	R	refusal	Fb	friable				
*bit shown by suffix						VL	very loose				
B	blank bit					L	loose				
V	V bit					MD	medium dense				
T	TC bit					D	dense				
e.g.	ADT					VD	very dense				
PENETRATION		WATER		MOISTURE							
1	no resistance	*	not measured	D	dry						
2	ranging to refusal			M	moist						
3				W	wet						
				Wp	plastic limit						
*bit shown by suffix		water level									
		water outflow									
		water inflow									

COFFEY S 8463/4

BH 101

FROM 11.3 M

TO 18.0 M





borehole no:

101

sheet 2 of 13

office job no: S8463/4

engineering log - borehole

client: HORNSBY SHIRE COUNCIL principal: project: OLD MANS VALLEY borehole location: E 308518.10 N 1269889.83							hole commenced: 4.12.89 hole completed: 4.12.89 logged by: SRM checked by: PLV			
drill model and mounting: PIONEER B40 hole diameter: 76mm				slope: -65 DEG bearing: 260.		R.L. Surface: 102.9 m datum: AHD				
method 1 2 3	penetration water	notes samples, test,etc	R.L. metres	depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics colour, secondary and minor components	moisture condition	consistency/ density index hand penetrometer meter	structure and additional observations
R	C			95		GC	CLAYEY GRAVEL: fine to coarse grained, grey brown, sand fine to coarse grained, & clay moderately to highly weathered breccia	M	100 200 300 400	EW BRECCIA(?)
				94			COMMENCED CORING AT 11.3m			
				93						
				11						
				92	12					
				91	13					
				90	14					
				89	15					
				16						
METHOD		SUPPORT		NOTES		CLASSIFICATION		CONSISTENCY/DENSITY INDEX		
AS	auger screwing*	C	casing	USQ	undisturbed sample 50 mm diameter	SYMBOLS AND SOIL DESCRIPTION	VS	very soft		
AD	auger drilling*	M	mud	D	disturbed sample	based on unified classification system	S	soft		
R	roller/tricone	PENETRATION 1 2 3	no resistance ranging to refusal	N	standard penetration test:	F	firm			
W	washbore			N*	SPT + sample recovered	SI	stiff			
CT	cable tool			Nc	SPT with solid cone	VSI	very stiff			
HA	hand auger			V	vane shear	H	hard			
DT	diatube			P	pressuremeter	Fb	friable			
*bit shown by suffix				Bs	bulk sample	VL	very loose			
B	blank bit			R	refusal	L	loose			
V	V bit					MD	medium dense			
T	TC bit					D	dense			
e.g.	ADT					VD	very dense			
WATER		WATER		MOISTURE						
*	not measured		water level	D	dry					
				M	moist					
				W	wet					
				Wp	plastic limit					



borehole no:

101

sheet 3 of 13

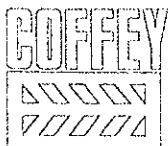
engineering log - cored borehole

client: principal: project: borehole location:	HORNSBY SHIRE COUNCIL OLD MANS VALLEY E 308513.88 N 1269888.05	hole commenced: hole completed: logged by: checked by:	14.11.89 30.11.89 SRM PLV
drill model and mounting: barrel type and length:	PIONEER B40 TRUCK NQ 3.0m	slope: fluid:	-65 DEG WATER
drilling information			
method case-lift water	rock substance	rock mass defects	
R.L. depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering Est. Strength point load test Is(50) MPa
			defect spacing mm 3000 3000 3000
			defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
95 9 94 10 93 11			
Continued from non-core borehole			
NQ	NO CORE: 0.3m	SW	JT PL Fe stained, smooth
92 12	BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.	FR	JT PL Fe stained
91 13	cement put in hole to seal water loss		JT PL Fe stained crushed layer 30mm thick IR fracturing associated with JT PL
14			Broken zone 200mm thick
90 15	BRECCIA: fine to medium grained, light grey, indistinct bedding. BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding, large clasts of sandstone	D A T30 2.80	2 intersecting JT PL some calcite series of 6 parallel PL RO JT 20mm spacing calcite vein 14.2 - 14.3 JT PL smooth calcite fracturing around IR JT 60mm JT PL RO Fe stained 3 closed JT PL RO, parallel, 30mm spacing JT IR CU
89 16			some calcite

General Defect Description:
JT PL RO

METHOD	WATER LEVEL	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screening	V water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	V water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	*		MW -moderately	L -low	SM -seam
W washbore	not measured	Drilling Water	HW -highly	M -medium	CL -clay
NMLC core drilling			EW -extremely	H -high	RO -rough
NQ,HQ core drilling				VH -very high	DC -decomposed
casing used	partial loss	core recovered (hatching indicates material)			PL -planar
barrel withdrawn	complete loss	no core recovered			IR -irregular





borehole no:

101

sheet 4 of 13

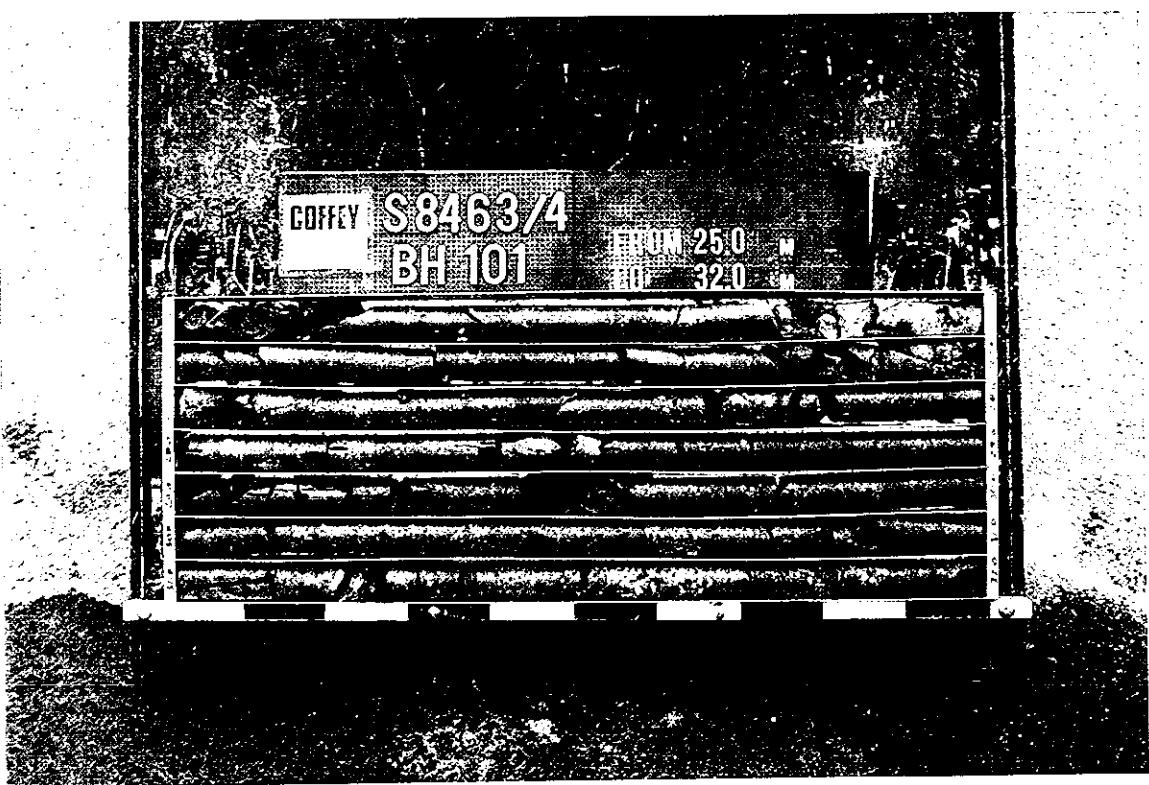
engineering log - cored borehole

client:		HORNSBY SHIRE COUNCIL						Office Job No.: 3640574	
principal:		OLD MANS VALLEY						hole commenced:	14.11.89
project:		E 308513.88 N 1269889.05						hole completed:	30.11.89
borehole location:								logged by:	SRM
drill model and mounting:			PIONEER B40 TRUCK			slope:		-65 DEG	R.L Surface:
barrel type and length:			NQ 3.0m		fluid:	WATER		bearing:	260.
drilling information			rock substance			rock mass defects			
method	core-loss	depth metres	graphic log	substance description	weathering	Est. Strength	point load test ls(50) MPa	defect spacing mm	defect description
case-lift	water	R.L.		rock type: grain characteristics colour, structure, minor components					type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ		88		BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding, large clasts of sandstone	SW				JT PL clean crushed zone 120mm thick fractured zone and broken zone 200mm thick
		17			FR				JT PL smooth fractured layer 30mm thick
		87		BRECCIA: fine to medium grained, light grey, thinly bedded, calcite nodules on bedding plane					JT PL RO some calcite IR fracturing associated with JT fracturing layer 20mm thick
		16		BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.					JT (2) intersecting PL RO IR fracturing associated with JT broken zone 200mm
		86							JT PL RO some calcite 2 parallel PL JT
		19			SW				JT PL RO with broken zone fissured zone IR from 17.6 - 17.9m with calcite filling
		85			FR				JT PL crushed broken zones with JT IR RO from 18.2-16.0m
		20			SW				
		84		BRECCIA: medium to coarse grained, light grey, - grey, thinly bedded, graded bedding	FR				IR fracturing 70mm zone zone of JT IR RO crushed seam 30mm thick crushed & fragmented zone 120mm thick Broken zone with JT IR RO
		21			SW				JT PL smooth broken zone 60mm thick
		83		BRECCIA: medium to coarse grained, light grey, indistinct bedding, large clasts of siltstone and sandstone	FR				JT PL smooth broken layer 40mm thick fragmented zone 100mm thick containing calcite and Fe stains 2 parallel JT PL
		22			SW				fractured zone 50mm thick broken zone 100mm thick JT PL smooth
		82		BRECCIA: fine to medium grained, light grey, indistinct bedding.	FR				JT PL RO 20.25 - 20.4m contains calcite filling fragmented zone 40mm thick
		23		BRECCIA: medium to coarse grained, grey, light grey, indistinct bedding, large clasts of siltstone, sandstone and coal					JT PL RO calcite JT closed PL RO
									JT PL smooth JT PL smooth JT PL smooth
									JT PL RO calcite and Fe stain JT PL RO Fe stained fragmented zone 15mm thick
									JT PL RO Fe stained fractured layer 80mm thick with Fe staining
									JT PL smooth, calcite Fe stain
									Broken layer Fe stained
									JT PL smooth
									JT PL RO Fe stained
									calcite vein 2mm thick PL
									JT PL smooth Fe stained
									calcite vein 4mm thick PL
									JT PL smooth Fe stained
									broken layer
									fractured and fragmented zone 150mm thick

General Defect Description:

General
JF PL RO

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	= water level	FR -fresh	EL -extremely low	JT -joint
AD	auger drilling	D -diametral	SW -slightly	VL -very low	PT -parting
R	roller/tricone	A -axial	MW -moderately	L -low	SM -seam
W	washbore	*	HW -highly	M -medium	CL -clay
NMLC	core drilling	Drilling Water	VH -very high	H -high	RO -rough
NQ,HQ	core drilling	partial loss	EW -extremely	EH -extremely high	DC -decomposed
II	casing used	core recovered (hatching indicates material)	PL -planar	IR -irregular	PL -planar
	barrel withdrawn	no core recovered			IR -irregular



engineering log cored borehole

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308513.88 N 1269889.06

hole commenced: 14.11.89
 hole completed: 30.11.89
 logged by: SRM
 checked by: BLV

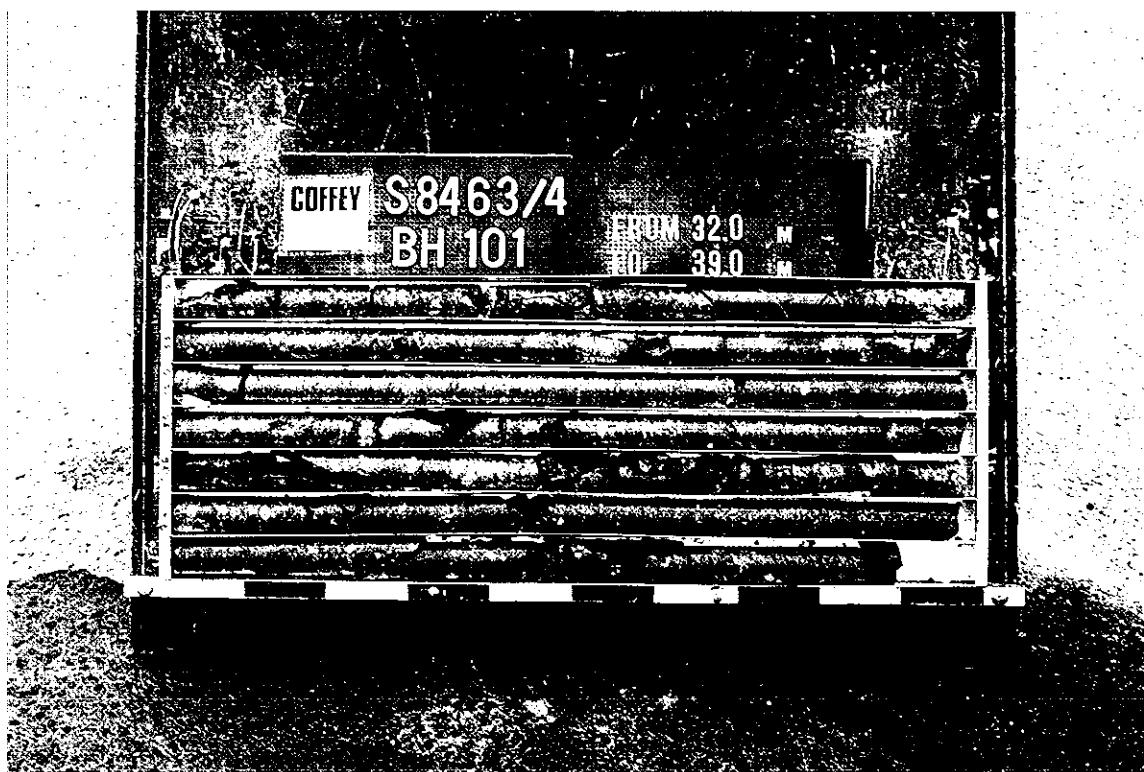
drill model and mounting: PIONEER B40 TRUCK slope: -65 DEG R.L.Surfaces: 102.9 m
 barrel type and length: NO. 3.0m fluid: WATER bearing: 260. datum: AHD

barrel type and length: NQ 3.0m trufo: WATER bedding: 200' 0.000m. ARI

drilling information rock substance rock mass defects

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS	
AS	auger screwing		water level	D -diametral	FR -fresh	JT -joint
AD	auger drilling		water inflow	A -axial	SW -slightly	PT -parting
R	roller/tricone		not measured		VL -very low	SM -seam
W	washbore		Drilling Water		L -low	CL -clay
NMLC	core drilling		partial loss	core recovered (hatching indicates material)	MW -moderately	RO -rough
NQ,HQ	core drilling casing used barrel withdrawn		complete loss		HW -highly	DC -decomposed
				no core recovered	EW -extremely	PL -planar
					EH -extremely high	IR -irregular



BIAVOL - 4



borehole no:

101

sheet 5 of 13

engineering log cored borehole

drilling information							rock substance							rock mass defects						
method	core-lift	water	RL	depth metres	graphic log score	substance description	weathering	Est. Strength	point load test ls(50)	defect spacing mm	defect description									
NQ						BRECCIA: medium to coarse grained, grey, indistinct bedding, large clasts of siltstone / sandstone	FR			30 300 3000 30000	JT (3) parallel 20mm spacing PL									
				73	33	BRECCIA: fine grained, grey, indistinct bedding,					JT IR calcite									
						BRECCIA: medium to coarse grained, light grey, indistinct bedding, large clasts of siltstone/sandstone some fine grained zones (boulders) to 33.7m					broken zone 30mm thick									
				72	34						JT PT smooth									
						BRECCIA: medium to coarse grained, light grey, grey, thinly bedded bedding distinguished by variations in grain size					calcite vein 1mm thick Pt									
				71	35						JT PL calcite smooth									
				70	36		SW				JT PL RO Fe									
							FR				broken zone 10mm thick									
				69	37		SW													
											JT PL RO Fe associated with Jf's									
				68	38		FR				JT PL RO Fe									
							SW				JT IR RO Fe closed at bottom									
				67	39						JT PL smooth									
											fractured zone 150mm Fe									
				40		Hole cemented due to water loss.					JT PL									
											broken layer 50mm thick									
											JT IR closed									
											broken zone 50mm thick									
											fractured zone 50mm thick									
											JT PL smooth calcite									
											fractured/broken zone 200mm thick									
											Hole cemented due to water loss									
											calcite vein <1mm thick									
											JT PL smooth									
											JT PL smooth calcite									
General Defect Description: JT PL RO																				
METHOD																				
AS	auger screwing	▽	water level			POINT LOAD TEST														
AD	auger drilling	▽	water inflow	D	-diametral	FR	-fresh													
'R	roller/tricone	▽	not measured	A	-axial	SW	-slightly													
W	washbore	*	Drilling Water	MW	-moderately	L	-low													
NMLC	core drilling	*	partial loss	H	-highly	M	-medium													
NQ,HQ	core drilling	△	complete loss	VH	-very high	H	-high													
	casing used			EW	-extremely	VH	-very high													
	barrel withdrawn					EH	-extremely high													



BH 101 - 5



borehole no:

101

sheet 7 of 13

office job no: S8463-4

engineering log - cored borehole

client: principal: project: borehole location:	HORNSBY SHIRE COUNCIL OLD MANS VALLEY E 308513.88 N 1269889.05	hole commenced: hole completed: logged by: checked by:	14.11.89 30.11.89 SRM PLV								
drill model and mounting:	PIONEER B40 TRUCK	slope:	-65 DEG								
barrel type and length:	NQ 3.0m	fluid:	WATER								
drilling information	rock substance	slope:	R.L. Surface: 102.9 m								
	bearing: 260 datum: AHD										
method	core lift water	R.L. depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength Is(50) MPa	point load test Is(50) MPa	defect spacing mm	rock mass defects	defect description type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below	
NQ					FR				D A 0.300.40		
		66	41	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, large clasts of siltstone/sandstone	MW					calcite veins <1mm thick	
		65	42		SW					JT PL RO Fe broken zone Fe 200mm thick	
		64	43	BRECCIA: medium to coarse grained, grey, thinly bedded, bedding indicated by imbrication	FR					JT IR RO Fe 70deg DD.67deg calcite veins <1mm thick 32deg DD.357deg	
		63	44		SW					JT IR RO calcite 30deg DD.342deg	
		62	45	BRECCIA: fine to medium grained, light grey, indistinct bedding.	FR				D A 0.502.50	JT PL RO calcite 69deg DD.79deg	
		61	46	BRECCIA: medium to coarse grained, grey, thin bedded, some clasts of coal, siltstone and sandstone with some fine grained bands, boulders up to 100mm thick						fractured zone 50mm calcite Fe 76deg DD.79deg	
		60	47	BRECCIA: medium grained, grey, dark grey, indistinct bedding.						JT PL RO Fe 74deg DD.99deg	
		48		BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, clasts of coal, siltstone and sandstone						fractured zone 50mm	
				some fine grained bands (boulders) to 100mm thick						JT PL RO calcite 80deg DD.295deg	
										calcite vein <1mm thick 82deg DD.302deg	
										calcite fissures <1mm thick	
										Hole cemented to seal drill water loss at 44.4m	
										JT PL RO calcite 73deg DD.167deg	
										{some pyrite on JT surface	
										JT PL smooth calcite 38deg DD.22deg	
										calcite veins IR RO <1mm thick	
										JT PL RO calcite	
										JT PL RO some calcite & pyrite	
										calcite veins <1mm thick	
										calcite pods 5mm dia.	
										JT PL RO calcite fill 1mm thick	
										SM crushed CT 25mm thick	
										calcite vein <1mm thick	
										calcite vein IR <1mm thick	

General Defect Description:
JT PL RO

METHOD	WATER LEVEL	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	water level	D - diametral A - axial	FR - fresh	EL - extremely low	JT - joint
AD auger drilling	water inflow		SW - slightly	VL - very low	PT - parting
R roller/tricone	not measured		MW - moderately	L - low	SM - seam
W washbore	Drilling Water		HW - highly	M - medium	CL - clay
NMLC core drilling	partial loss		EW - extremely	H - high	RO - rough
NQ,HQ core drilling	complete loss	core recovered (hatching indicates material)		VH - very high	DC - decomposed
TIE casing used		no core recovered		EH - extremely high	PL - planar
barrel withdrawn					IR - irregular



BH 101-6



borehole no:

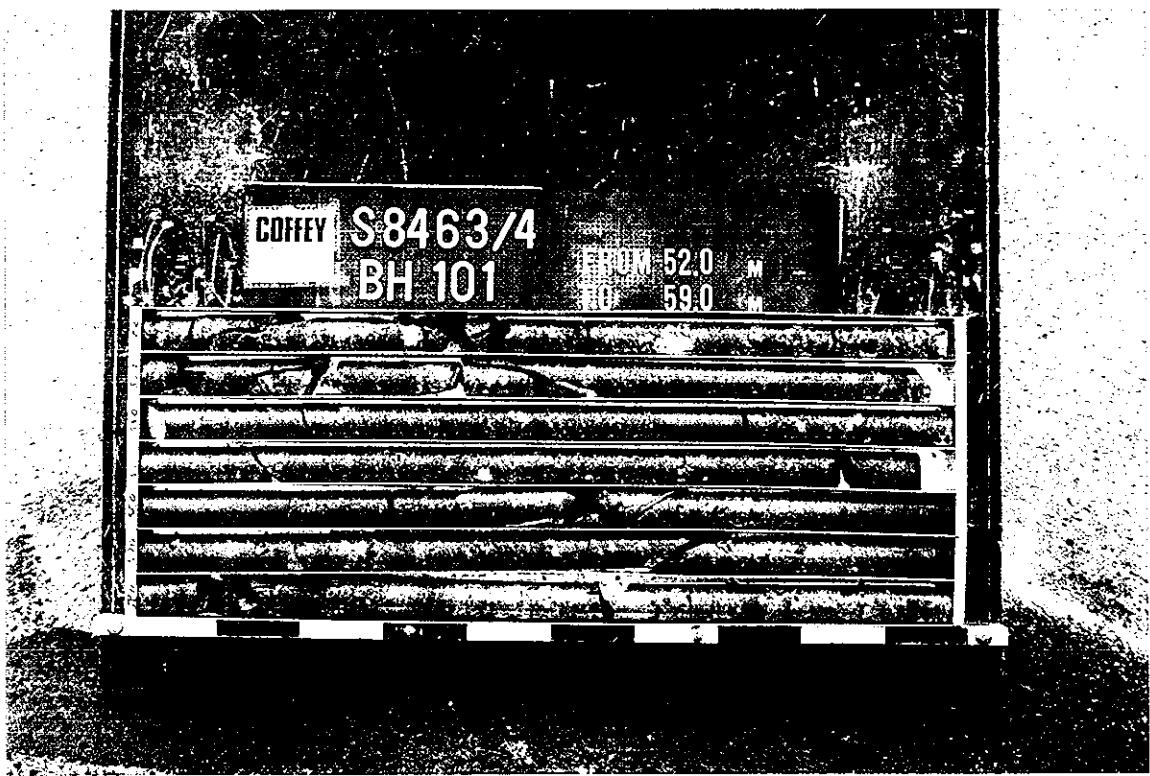
101

sheet 8 of 13

office job no: S8463/4

engineering log - cored borehole

client: principal: project: borehole location:	HORNSBY SHIRE COUNCIL OLD MANS VALLEY E 308513.88 N 1269889.05				hole commenced: hole completed: logged by: checked by:	14.11.89 30.11.89 SRM PLV	
drill model and mounting: barrel type and length:	PIONEER B40 TRUCK NQ 3.0m		slope: fluid:	-65 DEG WATER	R.L.Surface: bearing: datum:	102.9 m 260. AHD	
drilling information		rock substance			rock mass defects		
method class-lift water	core loss R.L. depth metres	graphic log core	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength Is(50) MPa	point load test Is(50) MPa	defect spacing mm
NQ			BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, clasts of coal, siltstone and sandstone	FR			3000 2000 1000
	59						
	49						
	58						
	50		BRECCIA: medium grained, light grey, indistinct bedding.	SW			
	57		BRECCIA: medium to coarse grained, dark grey, grey, indistinct bedding, large clasts of siltstone/sandstone	FR			
	51		BRECCIA: fine to medium grained, light grey, indistinct bedding.	SW			
	56		BRECCIA: medium to coarse grained, light grey, dark grey, thinly bedded, graded bedding and flows imbrication bedding dipping at 23deg DD.154deg	FR			
	52		BRECCIA: medium to coarse grained, grey, dark grey, indistinct bedding.	SW			
	55						
	53						
	54		BRECCIA: fine to coarse grained, light grey, grey, indistinct bedding.	FR			
	54		some fine grained boulders up to 100mm diameter.				
	53		BRECCIA: medium to coarse grained, grey, dark grey, indistinct bedding, some larger clasts possibly dolerite				
	55		BRECCIA: fine to medium grained, grey, indistinct bedding.				
	56		BRECCIA: medium to coarse grained, grey, dark grey, indistinct bedding, some larger clasts of dolerite				
D A 0.600.60							
General Defect Description: JT PL							
METHOD AS auger screwing AD auger drilling R roller/tricone W washbore NMLC core drilling NQ,HQ core drilling T T T T casing used barrel withdrawn	water level V V V V	water inflow V V V V	POINT LOAD TEST D -diametral A -axial GRAPHIC LOG/CORE LOSS * not measured Drilling Water partial loss complete loss	WEATHERING FR -fresh SW -slightly MW -moderately HW -highly EW -extremely	STRENGTH EL -extremely low VL -very low L -low M -medium H -high VH -very high EH -extremely high	DEFECTS JT -joint PT -parting SM -seam CL -clay RO -rough DC -decomposed PL -planar IR -irregular	



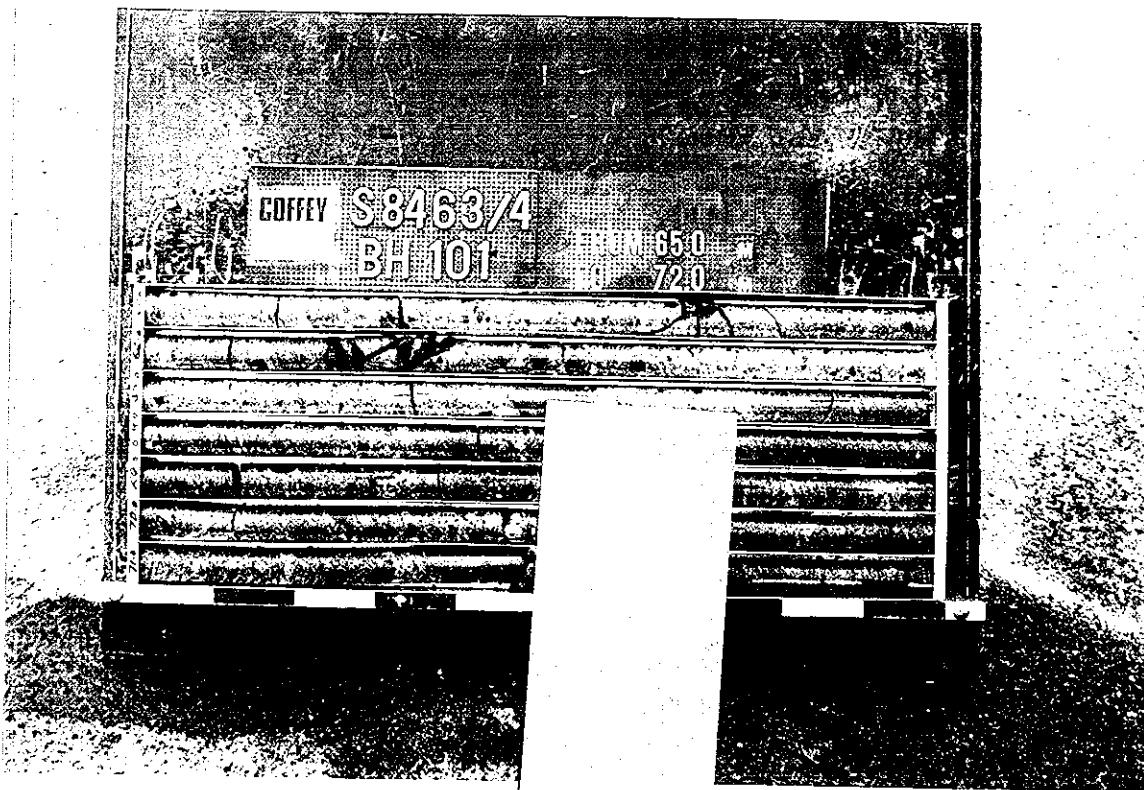
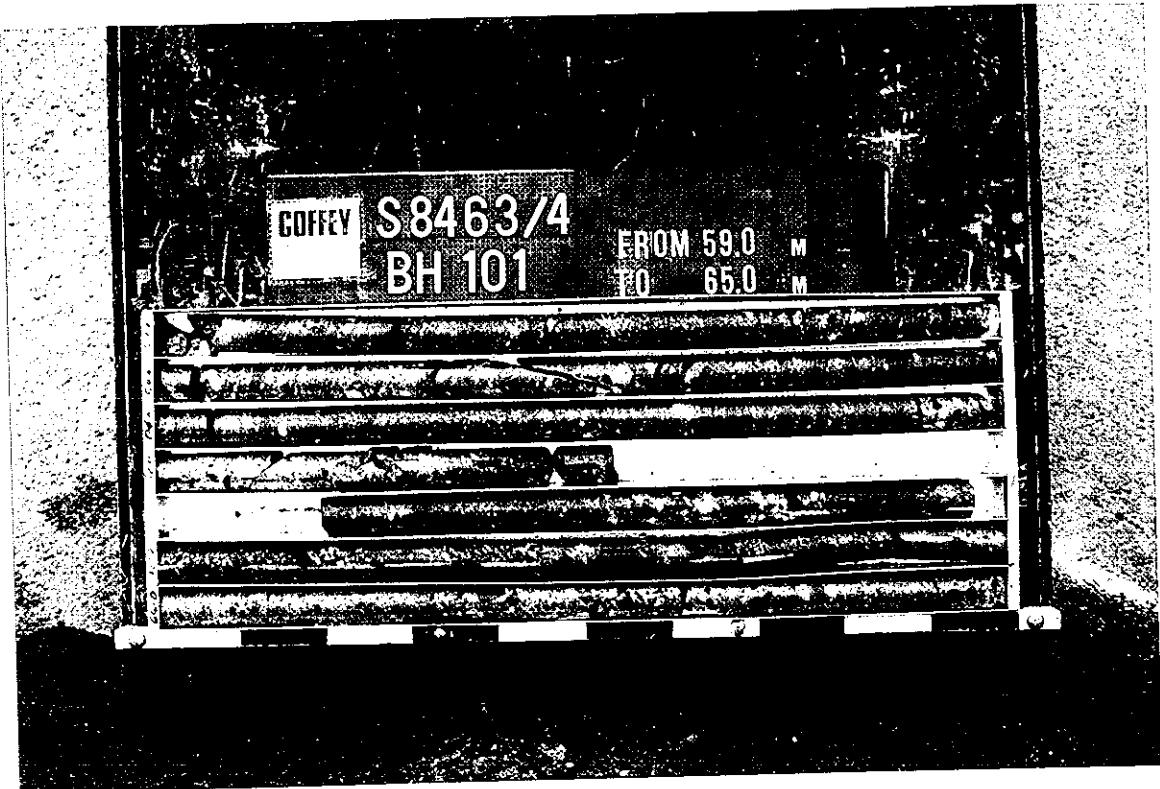
6000-7



borehole no: 101
sheet 9 of 13
office job no: S8463/4

engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	14.11.89			
principal:	OLD MANS VALLEY				hole completed:	30.11.89			
project:	E 308513.88 N 1269889.05				logged by:	SRM			
borehole location:	PIONEER B40 TRUCK	slope:	-6° DEG	R.L. Surface:	102.9	m	AHD		
drill model and mounting:	NO 3.0m	fluid:	WATER	bearing:	260°	column:			
drilling information		rock substance				rock mass defects			
method	core-bit: water	R.L. depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test: Is(50) MPa	defect spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NA	△	52	▼ □ △	BRECCIA: fine to medium grained, grey, indistinct bedding.	FR	M	3.5	300 300 300	JT PL calcite JT CU calcite 56.4 - 56.6m fractured layer associated with JT JT PL calcite 2mm thick
		57	▼ □ △	BRECCIA: medium to coarse grained, dark grey, grey, indistinct bedding, large clasts of siltstone/sandstone					calcite vein IR 1mm thick zone of IR calcite fissures <1mm thick 57.2 - 57.7m
		51	▼ □ △	BRECCIA: fine to medium grained, dark grey, grey, thinly bedded.					JT PL calcite JT IR RO CU
		58	▼ □ △	BRECCIA: medium to coarse grained, light grey, grey, thinly bedded, some imbrication					JT PL RO calcite 40deg DD.21deg JT PL calcite 76deg DD.16deg JT PL calcite 80deg DD.40deg JT PL calcite 78deg DD.94deg bedding 9deg DD.234deg
		50	▼ □ △	BRECCIA: fine to coarse grained, grey, dark grey, thinly bedded with graded bedding dipping at 9deg DD.234deg					JT CU calcite 72deg DD.144deg JT PL 78deg DD.156deg bedding 15deg DD.260deg
		59	▼ □ △	BRECCIA: medium to coarse grained, dark grey, light grey, indistinct bedding, clasts include coal, siltstone and sandstone					PT 21deg DD.201deg bedding 17deg DD.196deg
		49	▼ □ △	BRECCIA: fine to coarse grained, dark grey, grey, thinly bedded, dipping at 13deg DD.260deg					calcite veins <1mm thick 34deg DD.191deg calcite veins <1mm thick 31deg DD.120deg calcite veins <1mm thick 33deg DD.204deg calcite veins <1mm thick 37deg DD.184deg
		60	▼ □ △	BRECCIA: medium to coarse grained, light grey, dark grey, indistinct bedding, dipping at 12deg DD.189deg					JT PL RO 61deg DD.119deg
		48	▼ □ △	BRECCIA: fine to coarse grained, grey, dark grey, indistinct bedding, dipping at 20 deg DD. 199deg					JT PL RO calcite 89deg DD.39deg calcite veins <1mm thick 30deg DD.221deg
		61	▼ □ △	BRECCIA: medium to coarse grained, light grey, dark grey, indistinct bedding, dipping at 12deg DD.189deg					calcite veins <1mm thick 88deg DD.29deg calcite veins IR <1mm thick
		47	▼ □ △	BRECCIA: fine to coarse grained, light grey, grey, indistinct bedding, dipping at 12deg DD.189deg					calcite veins <1mm thick 32deg DD.17deg calcite veins <1mm thick 31deg DD.37deg calcite veins <1mm thick 67deg DD.209deg
		62	▼ □ △	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, dipping at 12deg DD.189deg					bedding plane 19deg DD.191deg calcite veins <1mm thick 62.2m - 62.2m
		46	▼ □ △	BRECCIA: fine to coarse grained, light grey, grey, indistinct bedding, dipping at 12deg DD.189deg					JT PL calcite 62deg DD.146deg JT PL calcite 80deg DD.74deg JT PL RO 46deg DD.272deg
		63	▼ □ △	BRECCIA: fine to coarse grained, grey, dark grey, indistinct bedding					calcite veins <1mm thick 32deg DD.17deg
		45	▼ □ △	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, apparent bedding at 12deg DD.189deg					calcite veins <1mm thick 31deg DD.312deg calcite veins <1mm thick 34deg DD.309deg calcite veins <1mm thick 72deg DD.49deg calcite veins <1mm thick 33deg DD.317deg
		64	▼ □ △						
General Defect Description:									
METHOD	AS auger screwing	▼ water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS			
AD	auger drilling	▼ water inflow	D -diametral	FR -fresh	EL -extremely low	JT -joint			
R	roller/tricone	* not measured	A -oxic!	VL -slightly	VL -very low	PT -parting			
W	washbore	Drilling Water	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam			
NMLC	core drilling	partial loss	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay			
NOHQ	core drilling	complete loss	no core recovered	EW -extremely	H -high	RO -rough			
T	casing used				VH -very high	DC -decomposed			
	barrel withdrawn				EH -extremely high	PL -planar			
						IR -irregular			



BH 101-8

engineering log cored borehole

office job no: S5463/4

sheet 10 of 13

client:		HORNSBY SHIRE COUNCIL										Office Job No.: 30405-2	
principal:		OLD MANS VALLEY											
project:		€ 308513.88 N 1269889.05											
borehole location:		drill model and mounting:			PIONEER B40 TRUCK			slope:		-63	DEG	R.L Surface:	102.9
barrel type and length:		NQ 3.0m			fluid:			bearing:		260.		datum:	AHD
drilling information			rock substance				rock mass defects						
method	case-lift	water	R.L	depth metres	graphic log core loss	substance description	weathering	Est Strength	point load test Is(50) MPa	defect spacing mm	defect description	type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below	
NQ						rock type: grain characteristics colour, structure, minor components							
						BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding, apparent bedding at 12deg DD.186deg	FR				JT PL RO 81deg DD.213deg		
				-44	65	darker band 50mm thick					JT PL calcite 68deg DD.119deg		
				-43	66						PT calcite 12deg DD.180deg		
				-42	67	darker medium grained band 100mm thick	SW				JT IK RO Fe 78deg DD.131deg		
				-41	68		FR				PT PL Fe 18deg DD.136deg		
				-40	69	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding dipping at 10deg DD.2deg					fractured/decomposed layer 40mm thick		
				-39	70	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding					JT PL 62deg DD.144deg		
				-38	71	BRECCIA: fine to coarse grained. grey, light grey, very thinly bedded 29 to 32deg					JT PL 61deg DD.151deg		
						BRECCIA: fine to coarse grained. grey, dark grey, indistinct bedding.					JT PL 63deg DD.149deg		
											bedding 10deg DD.100deg		
											calcite vein <1mm thick 82deg DDD.124deg		
											JT PL calcite 15deg DD.297deg		
											bedding 29deg DD.352deg		
											calcite vein <1mm thick 87deg DD.201deg		
											calcite vein IR <1mm thick		
											calcite vein <1mm thick PL 30deg DD.234deg		
								D A					
								070 1.60					
											bedding planes 18deg DD.284deg		
											calcite vein <1mm thick 82deg DD.74deg		
											bedding planes 19deg DD.202deg		
											fissured zone calcite filled IR 70.1-70.3m		
											calcite vein <1mm thick 31deg DD.290deg		
											calcite vein <1mm thick 33deg DD.307deg		
											calcite vein <1mm thick 32deg DD.37deg		
											calcite vein <1mm thick 78deg DD.193deg		
											JT PL 18deg DD.198deg		

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	▽ = water level	D -diametral	FR -fresh	JT -joint
AD	auger drilling	▽ = water inflow	A -axial	VL -very low	PT -parting
R	roller/tricone	* = not measured	GRAPHIC LOG/CORE LOSS	L -low	SM -seam
W	washbore	Drilling Water	core recovered (hatching indicates material)	MW -moderately	CL -clay
NMLC	core drilling	partial loss	no core recovered	HW -highly	RO -rough
NQ,HQ	core drilling			VH -very high	DC -decomposed
[]	casing used			EH -extremely	PL -planar
	barrel withdrawn	▽ = complete loss		EH -extremely high	IR -irregular



134107-9



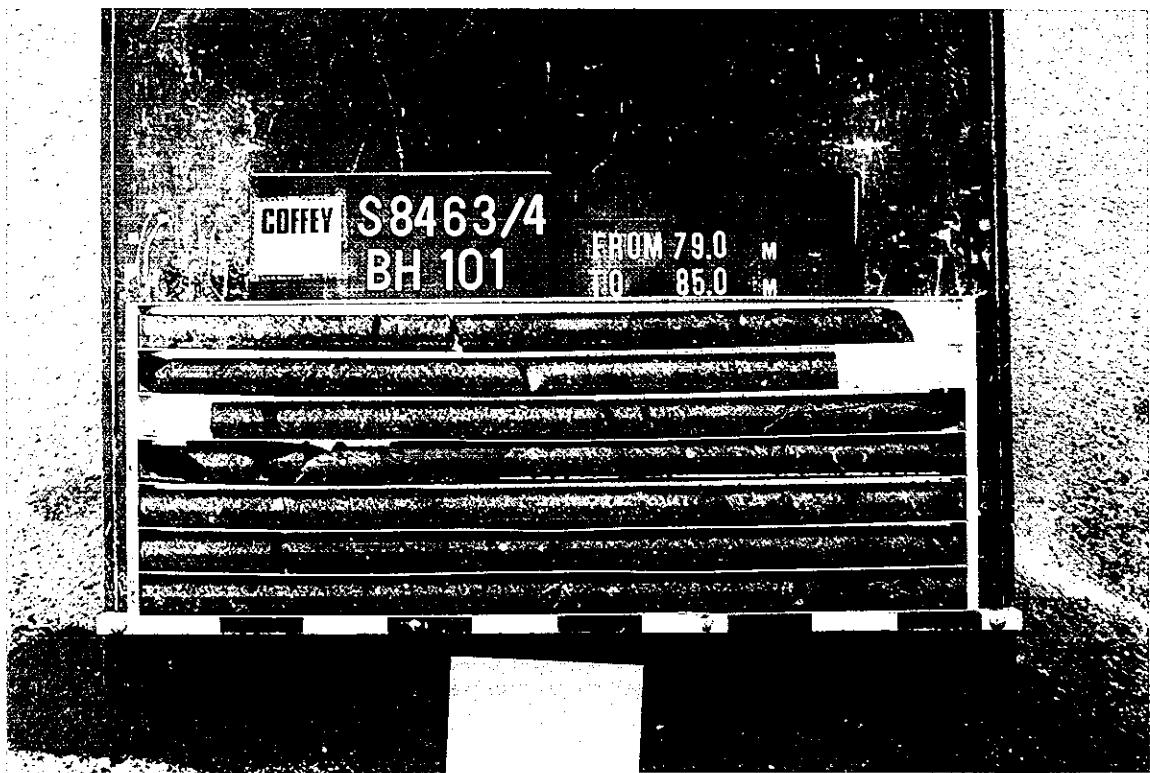
borehole no:
101
sheet 11 of 13

engineering log cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	14.11.89			
principal:					hole completed:	30.11.89			
project:	OLD MANS VALLEY				logged by:	SRM			
borehole location:	E 306513.88 N 1269889.08				checked by:	PLY			
drill model and mounting:	PIONEER B40 TRUCK		slope:	-05 DEG	R.L.Surface:	102.9	m		
barrel type and length:	NQ 3.0m		fluid:	WATER	bearing:	260.	datum: AHD		
drilling information	rock substance				rock mass defects				
method	core-lift	depth metres	Graphic log core loss	substance description	weathering	Est. Strength	point load test (Is(50)) MPa	defect spacing mm	defect description
water	R.L.			rock type: grain characteristics colour, structure, minor components				mm	type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ		37		BRECCIA: fine to coarse grained, dark grey, grey, indistinct bedding.	FR			300	JT PL RO 44deg DD.169deg
		73						300	JT PL RO 81deg DD.151deg
		36						300	JT PL RO 85deg DD.176deg
		74						300	calcite vein IR <1mm thick
		35						300	calcite vein 73deg DD.52deg
		75						300	calcite vein <1mm thick 76deg DD.59deg
		34		BRECCIA: medium to coarse grained, light grey, grey, bedding dipping at approx 12deg DD. 234deg				300	
		76						300	calcite vein <1mm thick 75deg DD.62deg
		33		BRECCIA: coarse grained, light grey, grey, indistinct bedding, at about 14deg DD. 260deg				300	broken zone 42mm thick 12deg DD.234deg
		77		BRECCIA: fine to coarse grained, dark grey, grey, indistinct bedding.				300	some IP calcite fissures
		78		BRECCIA: coarse grained, grey, light grey, indistinct bedding.				300	calcite vein 2mm thick 73deg DD.54deg
		32		BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding.				300	JT PL calcite vein 1mm thick 74deg DD.57deg
		79		BRECCIA: fine to coarse grained, grey, dark grey, indistinct bedding.				300	calcite vein <1mm thick 74deg DD.57deg
		31		BRECCIA: medium to coarse grained, grey, indistinct bedding.				300	calcite fissures IR <1mm thick
		80		BRECCIA: medium to coarse grained, dark grey, grey, indistinct bedding.				300	calcite vein IR <1mm thick

General Defect Description:
JT PL RO

METHOD	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	A -axial	SW -slightly	VL -very low	PT -parting
R roller/lithcone	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W washbore	* not measured	HW -highly	M -medium	CL -clay
NMLC core drilling	Drilling Water	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	partial loss		VH -very high	DC -decomposed
	complete loss		EH -extremely high	PL -planar
TII casing used				IR -irregular
barrel withdrawn				



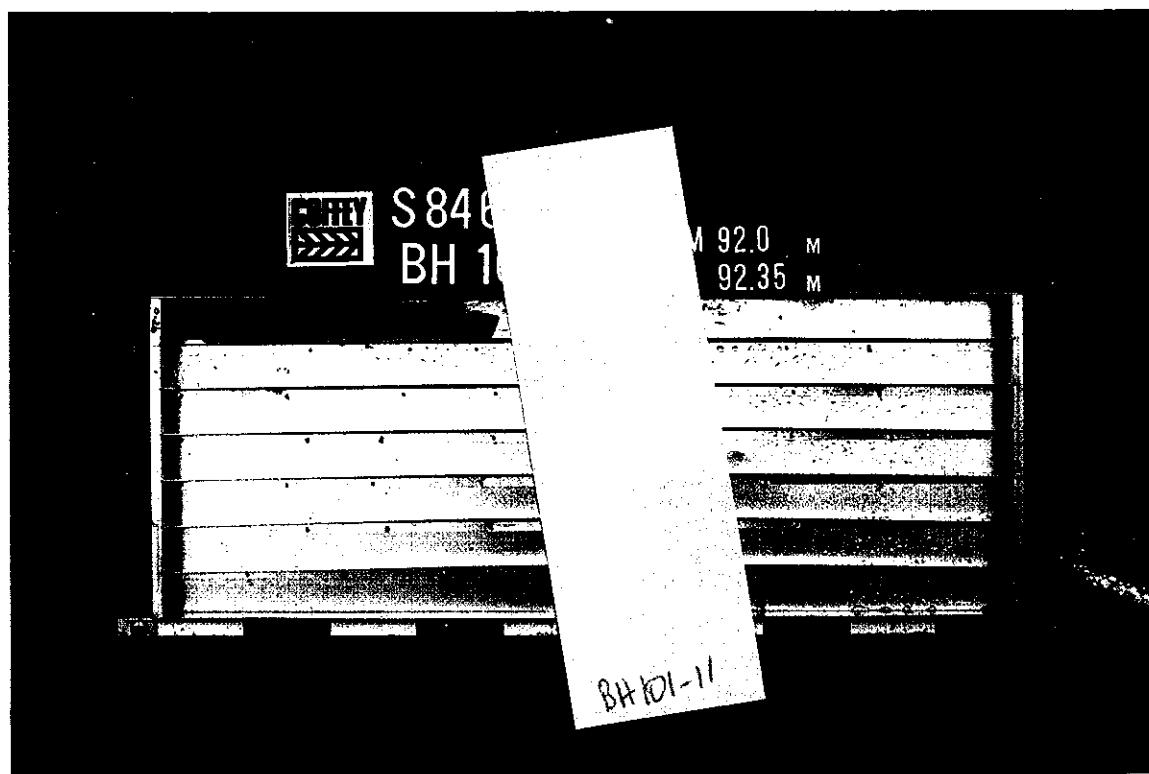
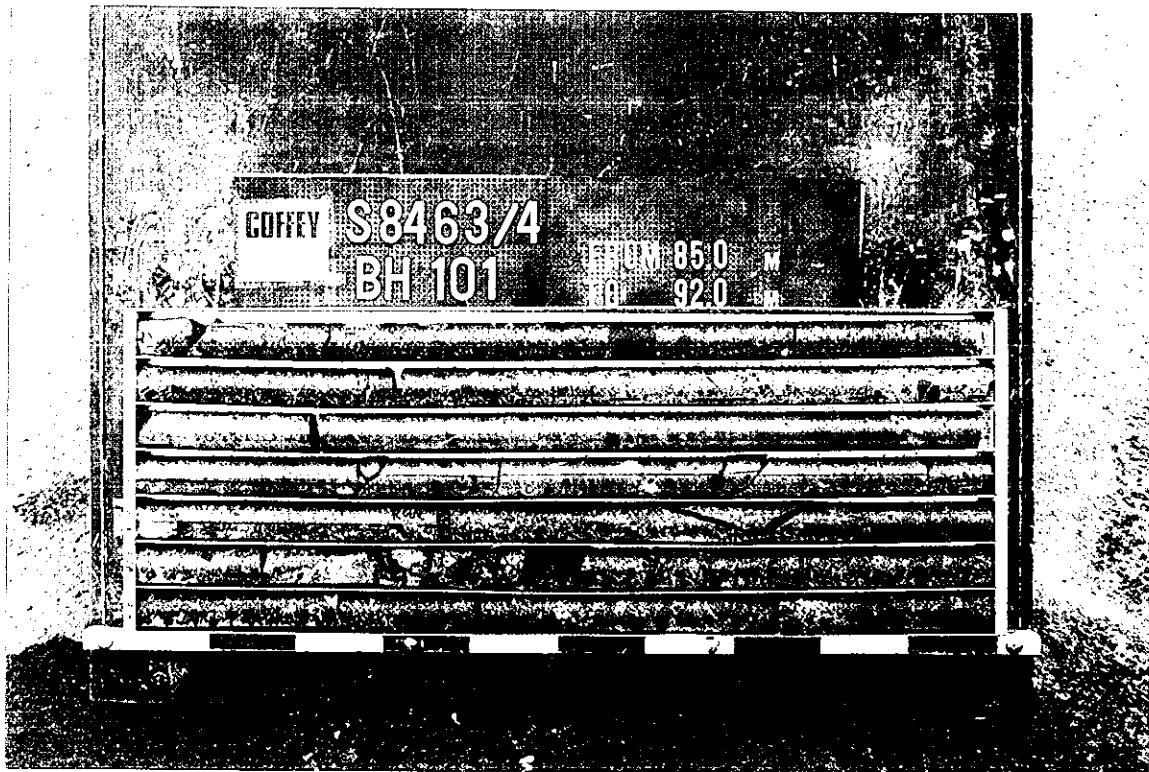
BH101-12

engineering log cored borehole

HORNSBY SHIRE COUNCIL								hole commenced: 14.11.89 hole completed: 30.11.89 logged by: SRM checked by: PLV			
OLD MANS VALLEY E 308513.86 N 1269889.03											
drill model and mounting: PIONEER B40 TRUCK				slope: -65 DEG		R.L.Surface: 102.9 m					
barrel type and length: HQ 3.0m				dip: WATER		bearing: 260.		datum: AHD			
drilling information		rock substance				rock mass defects					
method	case-lift	R.L. metres	depth metres	Graphic log core loss	substance description	weathering	est Strength	point load test Is(50) MPa	defect spacing mm	defect type	defect description
					rock type: grain characteristics colour, structure, minor components						type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ		-30	80	▼: ▲: △: ▽: ▾:	BRECCIA: fine to coarse grained, light grey, grey, very thin bedded.	FR					calcite vein IR <1mm thick
		-30	81	▼: ▲: △: ▽: ▾:	BRECCIA: medium to coarse grained light grey, grey, indistinct bedding.	FR					calcite vein IR <1mm thick J1 PL calcite 2mm thick
		-29	82	▼: ▲: △: ▽: ▾:	BRECCIA: fine to coarse grained, light grey, grey, thin bedded.	FR					J1 IR calcite 2mm thick
		-29	82	▼: ▲: △: ▽: ▾:	BRECCIA: medium to coarse grained, light grey, grey, indistinct bedding.	FR					J1 PL smooth calcite broken zone 100mm thick 13deg DD.21deg J1 PL smooth calcite 83deg DD.64deg
		-28	83	▼: ▲: △: ▽: ▾:	BRECCIA: fine to coarse grained, grey.	FR					calcite vein 2mm thick 80deg DD.106deg J1 PL RU calcite 74deg DD.154deg calcite vein IR
		-27	84	▼: ▲: △: ▽: ▾:	DOLERITE: fine grained, grey, massive.	FR					calcite vein PL 81deg DD.184deg
		-27	84	▼: ▲: △: ▽: ▾:	BRECCIA: fine to coarse grained, dark grey, grey, indistinct bedding.	FR					calcite vein IR <1mm thick
		-26	85	▼: ▲: △: ▽: ▾:	Coal clast 100mm diameter	FR					PL calcite vein 2mm 88deg DD.82deg
		-25	86	▼: ▲: △: ▽: ▾:		FR					calcite filled IR fissured zone in coal clast
		-25	86	▼: ▲: △: ▽: ▾:		FR					broken zone 5mm thick 13deg DD.221deg
		-24	87	▼: ▲: △: ▽: ▾:	BRECCIA: medium to coarse grained, light grey, indistinct bedding.	FR					calcite vein <1mm thick 60deg DD.7deg J1 PL PO 43deg DD.109deg
		-24	87	▼: ▲: △: ▽: ▾:	BRECCIA: fine to coarse grained, light grey, indistinct bedding.	FR					

General Defect Description:
JT PL RO

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	- water level	D -diametral	FR -fresh	J1 -joint
AD	auger drilling		A -axial	VL -very low	PT -parting
R	roller/tricone	▼ water inflow		L -low	SM -seam
W	washbore	*		M -medium	CL -clay
NMLC	core drilling	not measured		H -high	RO -rough
NQ,HQ	core drilling	Drilling Water	core recovered (hatching indicates material)	VH -very high	DC -decomposed
	casing used	△ partial loss		EH -extremely high	PL -planar
	barrel withdrawn	▲ complete loss	no core recovered		IR -irregular



engineering log cored borehole

client: HORNBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308513.88 N 1269880.0

hole commenced: 14.11.89
 hole completed: 30.11.89
 logged by: SRM
 checked by: BIV

drill model and mounting: PIONEER B40 TRUCK slope: -55 DEG k L Surface: 102.9 m
 barrel type and length: NO. 30m fluid: WATER bearing: 260. datum: AHD

barrier type and length: **NG 3.0m** HOW: **WATER** BRIDGING: **NO**

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	▽ = water level	D -diametral	FR -fresh	J1 -joint
AD	auger drilling		A -axial	SW -slightly	PT -parting
R	roller/tricone	▽▽ water inflow		MW -moderately	SM -seam
W	washbore	*		HW -highly	CL -clay
NMLC	core drilling	not measured	core recovered (hatching indicates material)	EW -extremely	RO -rough
NQ,HQ	core drilling	Drilling Water			DC -decomposed
	casing used	△△ partial loss	no core recovered	EL -extremely low	PL -planar
	barrel withdrawn	△△△ complete loss		VL -very low	IR -irregular
				L -low	
				M -medium	
				H -high	
				VH -very high	
				EH -extremely high	



borehole no:

102

sheet 1 of 12

office job no: S8463.3

hole commenced: 4.12.89

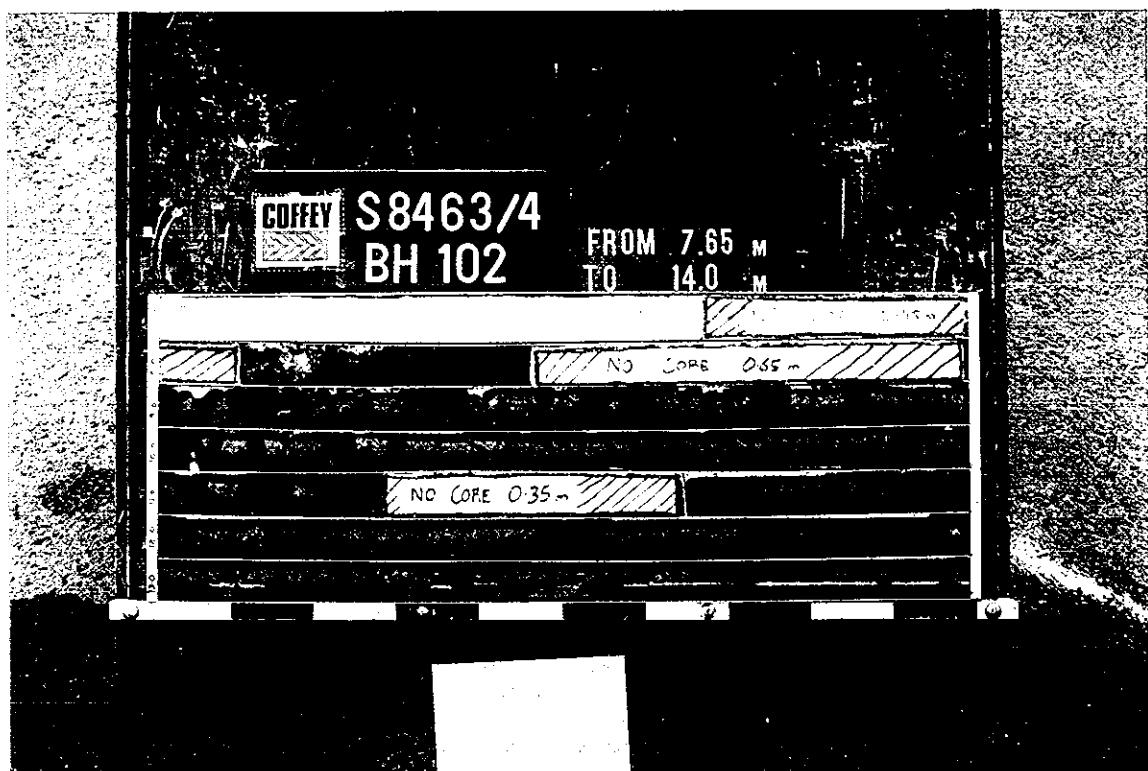
hole completed: 4.12.89

logged by: SRM

checked by: PLV

engineering log - borehole

client: HORNSBY SHIRE COUNCIL							hole commenced: 4.12.89				
principal:							hole completed: 4.12.89				
project: OLD MANS VALLEY							logged by: SRM				
borehole location: E308518.10 N1269869.83							checked by: PLV				
drill model and mounting: PIONEER B40			slope: -65 DEG			R.L. Surface: 103.1		datum: AHD			
hole diameter: 76mm			bearing: 80deg								
method	penetration 1 2 3	support water	notes samples, test,etc	R.L. depth metres	graphic log	classification symbol	material soil type: plasticity or particle characteristics colour, secondary and minor components	moisture condition	consistency/ density index/c consistency index/c meter	structure and additional observations	
R		C		- 103		CL	FILL: Clay medium plasticity, red brown Gravel and Sand fine to coarse grained	M	70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290 300 310 320 330 340 350 360 370 380 390 400 410 420 430 440 450 460 470 480 490 500 510 520 530 540 550 560 570 580 590 600 610 620 630 640 650 660 670 680 690 700 710 720 730 740 750 760 770 780 790 800 810 820 830 840 850 860 870 880 890 900 910 920 930 940 950 960		FILL~ contains breccia boulders
				- 102		CL	GRAVELLY CLAY: medium plasticity, yellow brown Gravel and Sand fine to coarse grained			RESIDUAL?	
				- 101							
				- 100							
				- 99							
				- 98							
				- 97							
				- 96							
Commenced coring at 7.65m											
METHOD		SUPPORT		NOTES samples and tests			CLASSIFICATION SYMBOLS AND SOIL DESCRIPTION		CONSISTENCY/DENSITY INDEX		
AS	auger screwing*	C	casing	U50	undisturbed sample 50 mm diameter		SYMBOLS AND SOIL DESCRIPTION		VS	very soft	
AD	auger drilling*	M	mud	D	disturbed sample		based on unified classification system		S	soft	
R	roller/tricone	PENETRATION 1 2 3	no resistance ranging to refusal	N	standard penetration test:				F	firm	
W	washbore			N*	SPT + sample recovered			S1	stiff		
CT	cable tool			Nc	SPT with solid cone			VSt	very stiff		
HA	hand auger			V	vane shear			H	hard		
DT	diatube			P	pressumeter			Fb	friable		
*bit shown by suffix				Bs	bulk sample			VL	very loose		
B	blank bit			R	refusal			L	loose		
V	V bit							MD	medium dense		
T	TC bit							D	dense		
e.g.	ADT							VD	very dense		



S8463/4
BH 102

engineering log - cored borehole

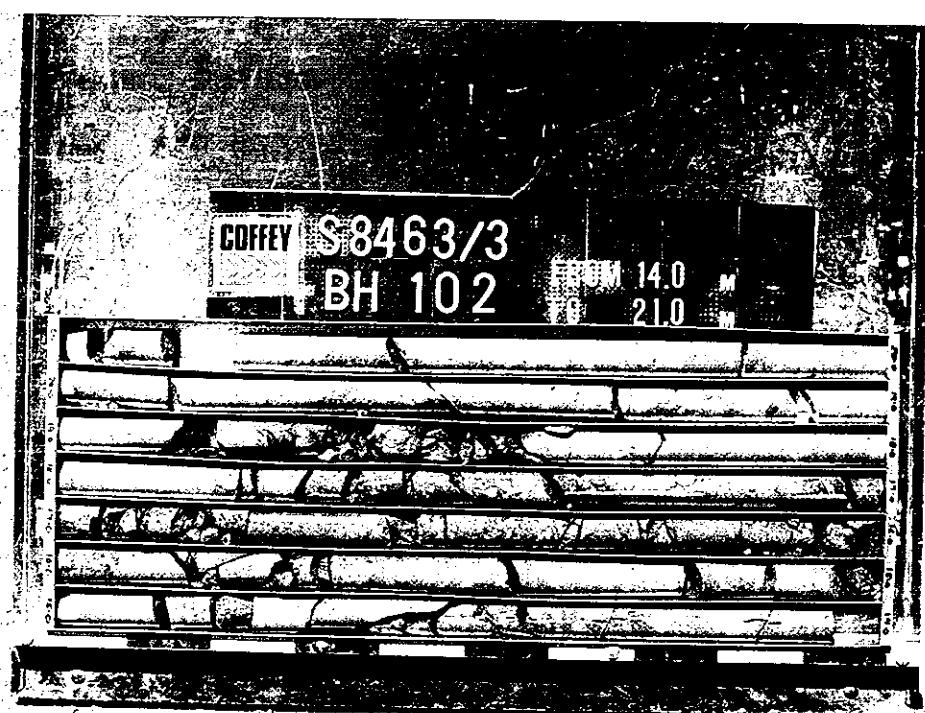
office job no: S8463/4

102

sheet 2 of 13

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD	auger drilling	A -axial	SW -slightly	VL -very low	PT -parting
R	roller/tricone		MW -moderately	L -low	SM -seam
W	washbore	*	HW -highly	M -medium	CL -clay
NMLC	core drilling	Drilling Water		H -high	RO -rough
NQ,HQ	core drilling			VH -very high	DC -decomposed
	casing used	partial loss	EW -extremely	EH -extremely high	PL -planar
	barrel withdrawn	complete loss			IR -irregular
		core recovered (hatching indicates material)			
		no core recovered			



BH102-2
BH102-3

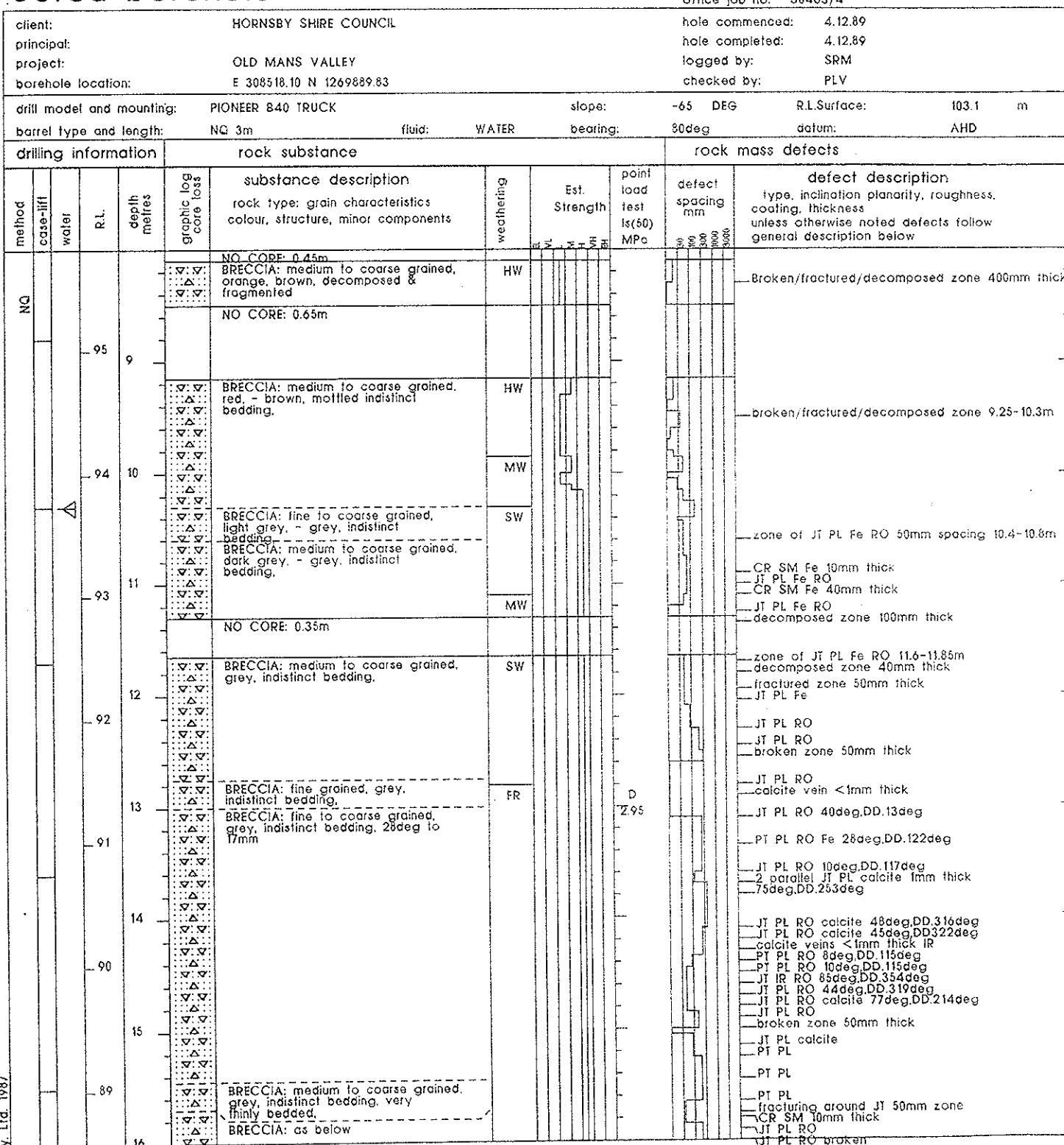


borehole no:

102

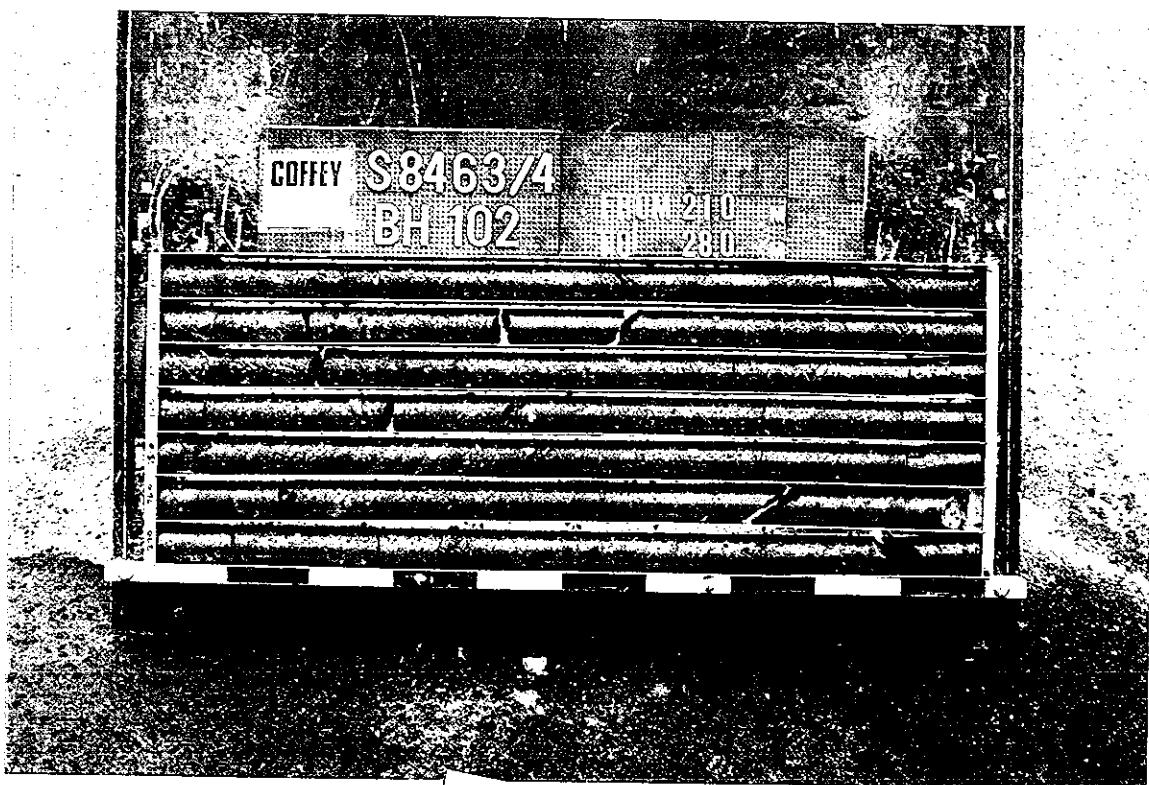
sheet 3 of 13

engineering log - cored borehole

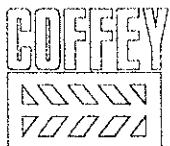


General Defect Description:

METHOD	WATER LEVEL	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	*	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W washbore	not measured	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay
NMLC core drilling	Drilling Water	no core recovered	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	partial loss			VH -very high	DC -decomposed
casing used	complete loss			EH -extremely high	PL -planar
barrel withdrawn					IR -irregular

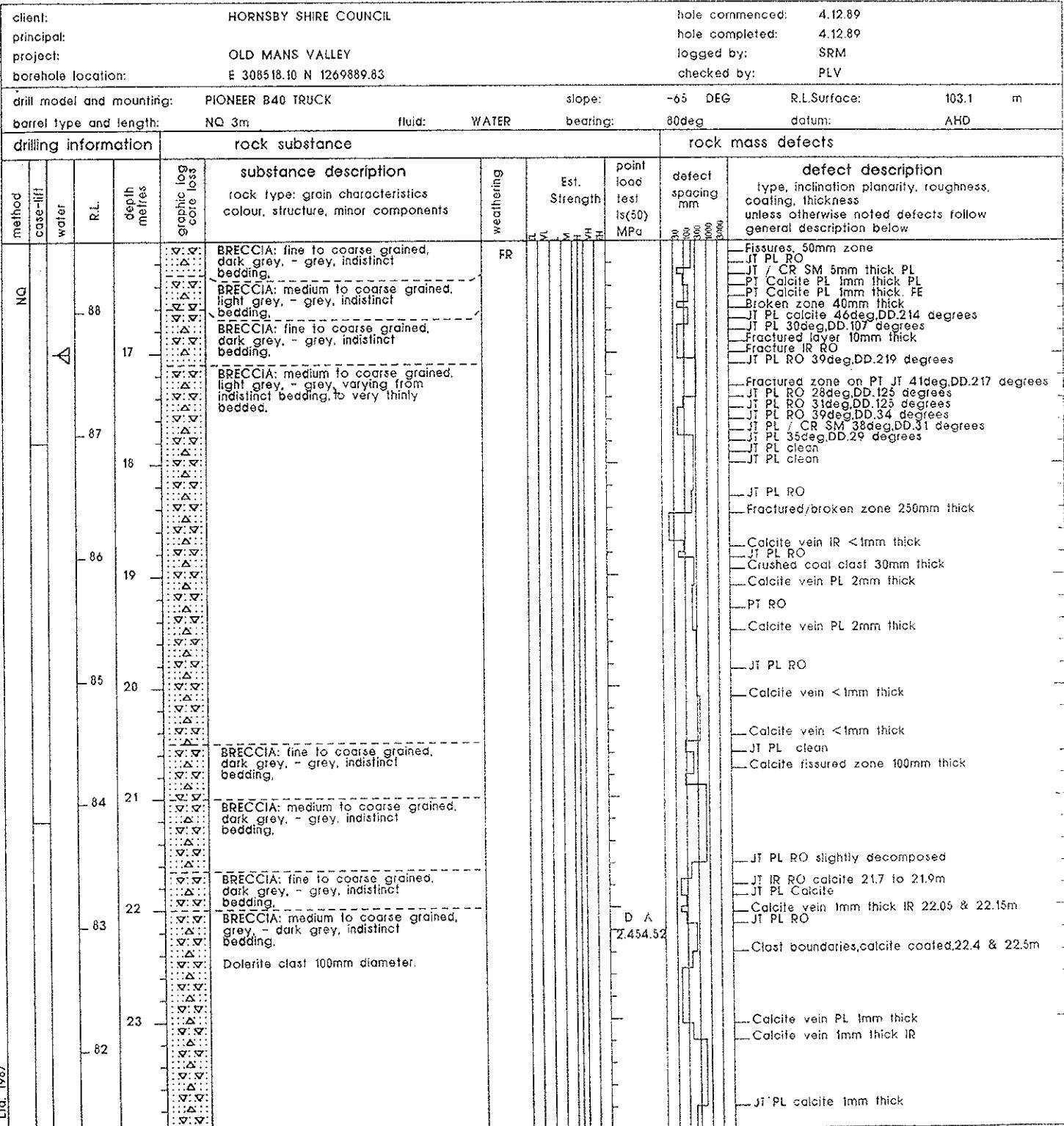


BH102-3



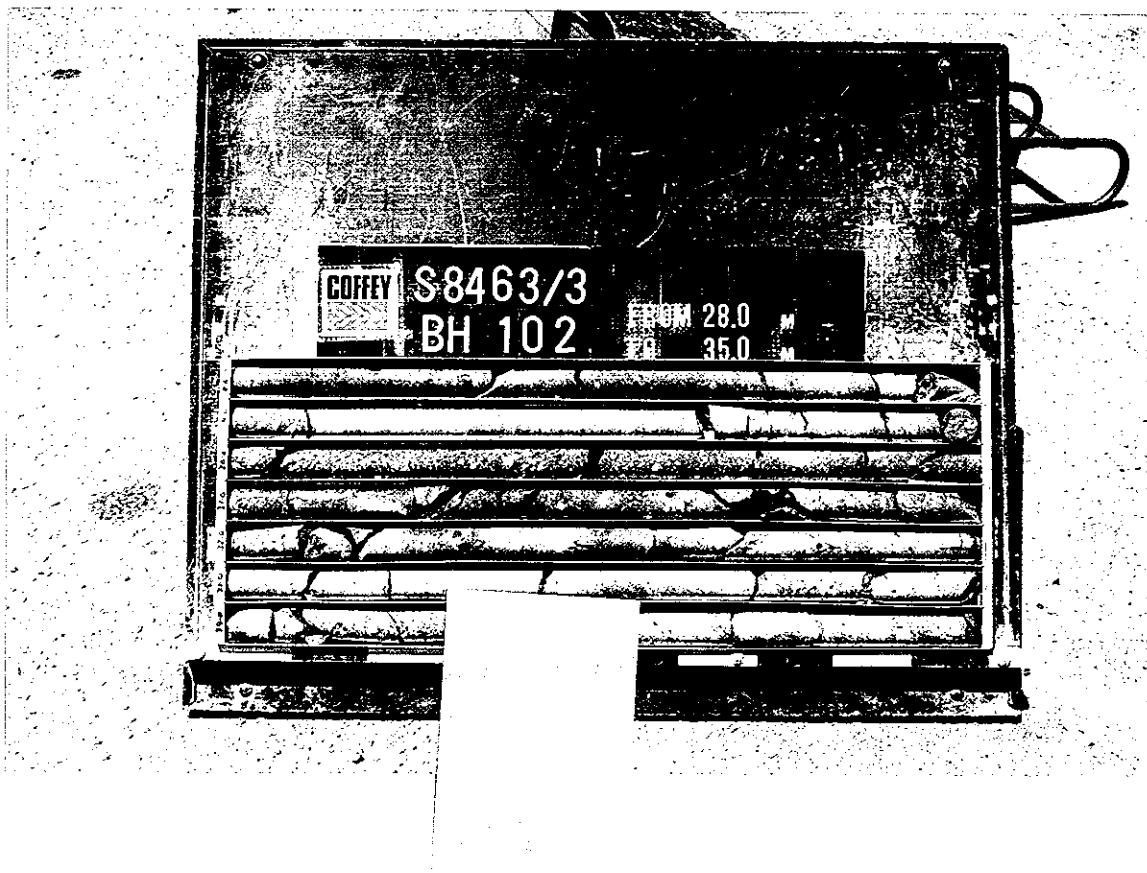
borehole no:
102
sheet 4 of 13
office job no: S8463/4

engineering log - cored borehole

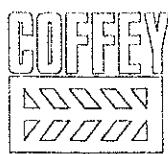


General Defect Description:

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	V water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	V water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	*	not measured	MW -moderately	L -low	SM -seam
W washbore		Drilling Water	HW -highly	M -medium	CL -clay
NMLC core drilling			EW -extremely	H -high	RO -rough
NQ,HQ core drilling		core recovered (hatching indicates material)		VH -very high	DC -decomposed
casing used	partial loss	no core recovered		EH -extremely high	PL -planar
barrel withdrawn	complete loss				IR -irregular



| BH102-4 |



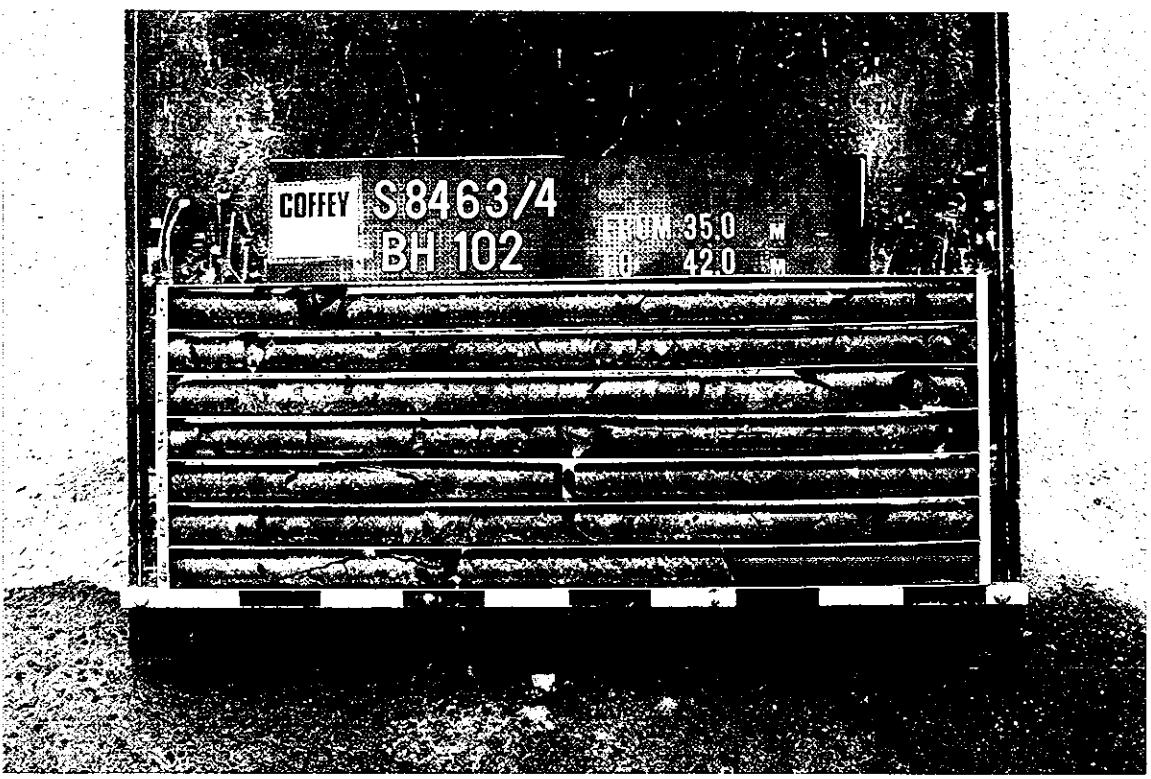
borehole no:

102

sheet 5 of 13

engineering log cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	4.12.89		
principal:					hole completed:	4.12.89		
project:	OLD MANS VALLEY				logged by:	SRM		
borehole location:	E 308518.10 N 1269889.83				checked by:	PLV		
drill model and mounting:	PIONEER B40 TRUCK	slope:	-65 DEG	R.L.Surface:	103.1	m		
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	80deg	datum:	AHD	
drilling information	rock substance			rock mass defects				
method	core-lift	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test Is(50) MPa	defect spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ	water	R.L. depth metres		FR				
		81	BRECCIA: medium to coarse grained, grey, - dark grey, indistinct bedding.					JT PL calcite 42deg, DD.257 degrees Calcite fissures <1mm thick Calcite vein 1mm thick 40deg, DD.137 degrees JT PL RO 66deg, DD.239 degrees PT PL clean 27deg, DD.4 degrees JT PL IR calcite
		25	BRECCIA: fine to coarse grained, dark grey, - grey, varying from indistinct bedding, to very thinly bedded, dipping 24deg DD 114deg					PT PL calcite 25deg, DD.21 degrees
		80						JT PL RO calcite 60deg, DD.284 degrees
		26						
		79	BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.					JT PL RO calcite, pyrite 67deg, DD.349deg
		27	BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding.					JT PL RO calcite 78deg, DD.239 degrees JT PL RO calcite 60deg, DD.264 degrees JT PL RO calcite
		78						JT PL RO 40deg, DD.41 degrees
		28						JT PL calcite 32deg, DD.80 degrees Calcite vein IR RO 2mm thick
		77						JT PL calcite 47deg, DD.162 degrees JT PL calcite, pyrite 21deg, DD.36 degrees Calcite vein 2mm thick 44deg, DD.152 degrees JT PL RO 73deg, DD.152 degrees JT PL calcite 15deg, DD.95 degrees Fissured zone with calcite 29.1 to 29.4m
		29						
		76						Broken zone 40mm wide Joints (3) 50mm spacings, calcite
		30						JT PL calcite JT PL RO calcite
		75						JT PL RO
		31						Calcite veins, <1mm thick IR JT PL calcite JT PL calcite
		32	BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.					JT PL RO calcite JT PL calcite, 31.3 and 31.35m JT IR RO FE 31.6 to 31.8m Coal clast 60mm thick JT PL FE CR 8mm thick JT PL calcite
General Defect Description:								
METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS			
AS	auger screwing	D -diametral	FR -fresh	EL -extremely low	JT -joint			
AD	auger drilling	A -axial	SW -slightly	VL -very low	PT -parting			
R	roller/tricone	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam			
W	washbore	* not measured	HW -highly	M -medium	CL -clay			
NMLC	core drilling	Drilling Water	EW -extremely	H -high	RO -rough			
NQ,HQ	core drilling	partial loss		VH -very high	DC -decomposed			
	casing used	complete loss		EH -extremely high	PL -planar			
	barrel withdrawn				IR -irregular			



BH102-S

engineering log - cored borehole

client: HORNBSY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308518 10 N 1269889 A3

hole commenced: 4.12.89
 hole completed: 4.12.89
 logged by: SRM

drill model and mounting: PIONEER B40 TRUCK slope: -65 DEG R.L.Surface: 103.1 m
 barrel type and length: NQ 3m fluid: WATER bearing: 80deg datum: AHD

drilling information | rock substance | rock mass classification

drilling information rock substance rock mass defects

method	core-lift	R.L.	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test: Is(50) MPa	defect spacing mm	defect description	
										type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below	
			-74		BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.	FR	Fractured	2.5	300	JT PL FE	
			-33		BRECCIA: fine to coarse grained, light grey, - dark grey, very thinly bedded, indistinct bedding.				300	JT PL FE	
			-73						300	JT IR RO	
			-34		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding, very thinly bedded.				300	JT PL RO 80deg,DD.46 degrees	
			-72						300	JT PL RO 47deg,DD.344 degrees	
			-35						300	JT IR RO	
			-71						300	JT PL calcite	
			-36						300	JT PL RO calcite	
			-70						300	JT PL	
			-37						300	JT PL	Broken zone 50mm thick
			-69		BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.				300	JT PL calcite	
			-38		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding.				300	JT IR RO	
			-68						300	JT PL calcite	
			-39						300	JT PL	
			-67						300	JT IR RO calcite	
			-40						300	JT IR RO	
									300	Broken zone ass., with JT	
									300	JT PL 64deg,DD.324 degrees	
									300	JT IR calcite RO	
									300	JT PL calcite 3mm thick	
									300	Calcite fissures <1mm thick	

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS		
AS	auger screwing		water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD	auger drilling		water inflow	A -axial	SW -slightly	VL -very low	PT -porous
R	roller/tricone	*	not measured		MW -moderately	L -low	SM -seam
W	washbore		Drilling Water		HW -highly	M -medium	CL -clay
NMLC	core drilling				VH -very high	RO -rough	
NQ,HQ	core drilling			no core recovered	EW -extremely	DC -decomposed	
	casing used		partial loss		EH -extremely high	PL -planar	
	barrel withdrawn		complete loss			IR -irregular	
GRAPHIC LOG/CORE LOSS							
			core recovered (hatching indicates material)				
			no core recovered				



borehole no:

102

sheet 0 of 13

engineering log - cored borehole

client: principal: project: borehole location:	HORNSBY SHIRE COUNCIL OLD MANS VALLEY E 308518.10 N 1269889.83							hole commenced: 4.12.89 hole completed: 4.12.89 logged by: SRM checked by: PLV	
drill model and mounting: barrel type and length:	PIONEER B40 TRUCK NQ 3m							slope: -65 DEG R.L.Surface: 103.1 m fluid: WATER bearing: 80deg datum: AHD	
drilling information		rock substance					rock mass defects		
method	core-lift	water	R.L.	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test Is(50) MPa
NQ			-74			BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.	FR		
				33		BRECCIA: fine to coarse grained, light grey, - dark grey, very thinly bedded, indistinct bedding.			
			-73						
				34		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding, very thinly bedded.			
			-72						
				35					
			-71						
				36					
			-70						
				37					
			-69			BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.			
				38		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding.			
			-68						
				39					
			-67						
				40					

General Defect Description:

METHOD	AS	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	coring screwing		D -diametral	FR -fresh	EL -extremely low	JT -joint
AD	coring drilling		A -axial	SW -slightly	VL -very low	PT -porting
R	roller/tricone		GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W	washbore	*	core recovered (hatching indicates material)	RW -highly	M -medium	CL -clay
NMLC	core drilling	Drilling Water	no core recovered	EW -extremely	H -high	RO -rough
NQ,HQ	core drilling	partial loss			VH -very high	DC -decomposed
	casing used	complete loss			SH -extremely high	PL -planar
	barrel withdrawn					IR -irregular

COFFEY S8463/3
BH 102

FROM 42.0
TO 49.0

S8462 - 6

engineering log - cored borehole

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308518.10 N 1269889.83

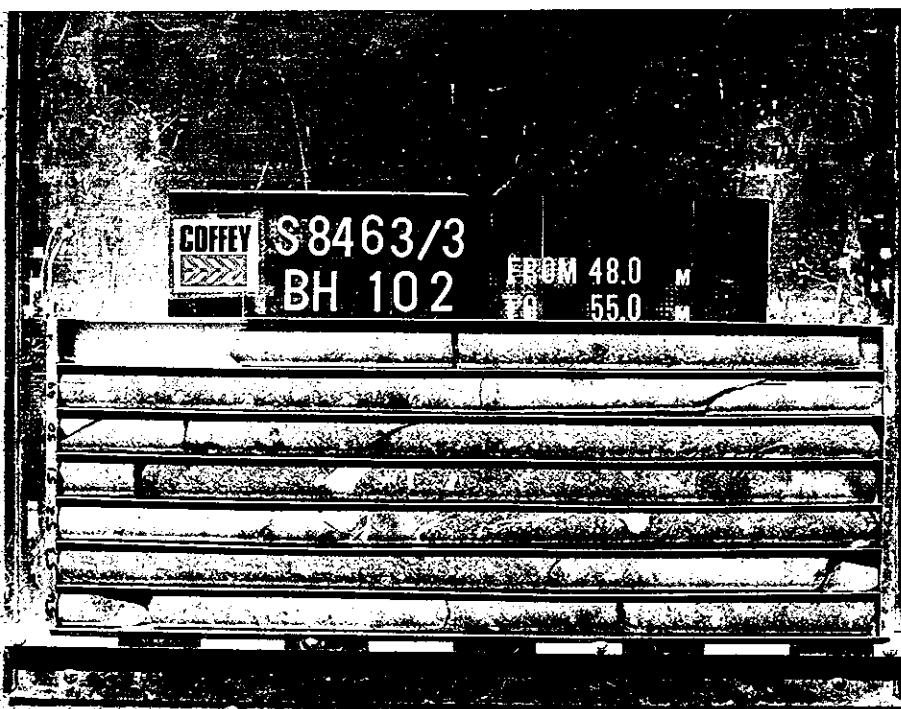
hole commenced: 4.12.89

drill model and mounting: PIONEER B40 TRUCK slope: -65 DEG R.L.Surface: 103.1 m
 borehole type and length: NQ 3m fluid: WATER bearing: 80deg datum: AHD

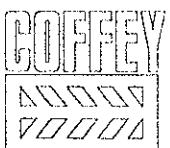
drilling information rock substance rock mass defects

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing		water level	D -diametral	JT -joint
AD	auger drilling		water inflow	A -axial	PT -parting
R	roller/tricone		not measured	GRAPHIC LOG/CORE LOSS	SM -seam
W	washbore	*	Drilling Water		CL -clay
NMLC	core drilling		partial loss	core recovered (hatching indicates material)	RO -rough
NQ,HQ	core drilling				DC -decomposed
	casing used			no core recovered	PL -planar
	barrel withdrawn			EW -extremely	IR -irregular
				VH -very high	
				EH -extremely high	



BH102-7



borehole no:
102
sheet 8 of 13
office job no: S8463/4

engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	4.12.89					
principal:					hole completed:	4.12.89					
project:	OLD MANS VALLEY				logged by:	SRM					
borehole location:	E 308518.10 N 1269889.83				checked by:	PLV					
drill model and mounting:	PIONEER B40 TRUCK		slope:	-65 DEG	R.L.Surface:	103.1	m				
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	80deg	datum:	AHD				
drilling information	rock substance				rock mass defects						
method	core-lift	water	R.L.	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test Is(50) MPa	defect spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ							FR			300 300 300	
				59		BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding.					JT PL RO calcite 56deg, DD.272 degrees
				49							JT PL RO 49deg, DD.269 degrees
				58		BRECCIA: medium to coarse grained, light grey, - grey, indistinct bedding.					JT PL calcite
				50		BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding.					JT PL RO calcite
				57							JT PL RO calcite
				51							Calcite vein 1mm thick
				56							Zone of calcite fissures to 2mm thick 50.75 to 50.95m
				52							JT PL RO calcite
				55							Calcite vein <1mm thick
				53							JT PL RO
				54							JT PL RO calcite
				54		Coarse grained band 250mm thick					JT PL RO
				55							JT PL RO
				53							JT PL RO
				56							JT PL RO calcite
											JT PL RO calcite

General Defect Description:

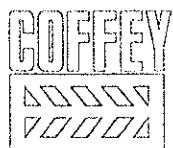
METHOD	AS	auger screwing	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AD	AD	auger drilling	=	D -diametral A -axial	FR -fresh	EL -extremely low	JT -joint
R	R	roller/tricone	▽	water inflow	SW -slightly	VL -very low	PT -parting
W	W	washbore	*	not measured	MW -moderately	L -low	SM -seam
NMLC	NMLC	core drilling	Drilling Water	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay
NQ,HQ	NQ,HQ	core drilling	partial loss	no core recovered	EW -extremely	H -high	RO -rough
		casing used	complete loss			VH -very high	DC -decomposed
		barrel withdrawn				EH -extremely high	PL -planar
							IR -irregular

COFFEY

S8463/3
BH 102

FROM 55.0
TO 62.0

BH 102-8



borehole no: 102
sheet 9 of 13
office job no: S8463/4

engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL					hole commenced:	4.12.89				
principal:						hole completed:	4.12.89				
project:	OLD MANS VALLEY					logged by:	SRM				
borehole location:	E 308518.10 N 1269889.83					checked by:	PLV				
drill model and mounting:	PIONEER 840 TRUCK			slope:	-65 DEG	R.L.Surface:	103.1	m			
barrel type and length:	NQ 3m		fluid:	WATER	bearing:	80deg	datum:	AHD			
drilling information	rock substance					rock mass defects					
method	core-lift	water	R.L.	depth metres	graphic log loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test (kg)	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ							FR		3.172.64	30 100 300 500 800 1000	
				52		BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding.					JT PL RO calcite
				57							JT PL RO
				51							JT curved RO calcite
				58							JT PL calcite
				50							calcite vein <1mm thick
				59							JT IR RO
				49							Broken zone 40mm thick
				60							Fractured zone with JT PL
				48							Fractured zone 30mm thick
				61							Fractured zone 58.55 to 58.70m
				47		BRECCIA: fine to coarse grained, light grey, - grey, indistinct bedding.					Calcite vein 1mm thick
				62							Broken zone 58.8 to 59.0m
				46		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding.					Crushed and fractured zone 250mm thick
				63							Crushed and fractured zone 200mm thick
				64							JT PL calcite
											JT PL calcite
											Calcite vein 1mm thick
											JT PL RO calcite 56deg, DD.80 degrees
											JT PL calcite 78deg, DD.394 degrees
											JT PL 47deg, DD.339 degrees
											JT PL 43deg, DD.339 degrees
											Calcite vein 74deg, DD.269 degrees
											Calcite vein 78deg, DD.274 degrees
											Calcite vein / JT 65deg, DD.80 degrees
											JT PL RO calcite 74deg, DD.322 degrees
											Calcite vein <1mm thick
											JT PL RO 88deg, DD.319 degrees
											JT PL RO 89deg, DD.326 degrees
											JT PL RO calcite 43deg, DD.322 degrees
											Calcite vein 2mm thick 46deg, DD.319 degrees
											Calcite vein 1mm thick 47deg, DD.324 degrees
											JT PL RO calcite 30deg, DD.25 degrees

General Defect Description:

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	water level	D -diametral A -axial	FR -fresh	EL -extremely low	J1 -joint
AD auger drilling	water inflow	GRAPHIC LOG/CORE LOSS	SW -slightly	VL -very low	P1 -parting
R roller/tricone	* not measured	core recovered (hatching indicates material)	MW -moderately	L -low	SM -seam
W washbore	Drilling Water	no core recovered	HW -highly	M -medium	CL -clay
NMLC core drilling	partial loss		EW -extremely	H -high	RO -rough
NQ,HQ core drilling	complete loss			VH -very high	DC -decomposed
casing used				EH -extremely high	PL -planar
barrel withdrawn					IR -irregular

COFFEE

S8463/3
BH 102

FROM 62.0 M
TO 69.0 M

BH 102 - 9

engineering log cored borehole

client: HORNBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308518.10 N 1269889.83

hole commenced: 4.12.89
 hole completed: 4.12.89
 logged by: SRM
 checked by: BLV

drill model and mounting: PIONEER B40 TRUCK slope: -65 DEG R.L.Surface: 103.1 m
 barrel type and length: NO. 3m fluid: WATER bearing: 80deg datum: AHD

drilling information rock substance rock mass defects

Drilling Information		Rock Substance		Rock Mass Rating						
Method	Core-Lift water	R.L. metres	Graphic Log core loss	Substance Description		Weathering	Est. Strength	Point load test (Is(50)) MPa	Defect spacing mm	Defect Description
NQ		45	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷	BRECCIA; fine to coarse grained, light grey, - grey, indistinct bedding.		FR	II	4.674.36	300 300 300	JT PL RO 42deg,DD,14 degrees JT PL RO 38deg,DD,21 degrees JT PL RO 38deg,DD,21 degrees JT PL RO 84deg,DD,262 degrees
		65	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷	BRECCIA; fine to coarse grained, grey, - dark grey, very thinly bedded, dipping 16 degrees						JT PL RO calcite 41deg,DD,332 degrees
		44	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							Calcite vein 1mm thick 42deg,DD,319 degrees
		66	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷							Calcite vein 3mm thick 30deg,DD,314 degrees
		43	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							Calcite vein <1mm thick 30deg,DD,326 degrees
		67	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷	BRECCIA; fine to coarse grained, light grey, - dark grey, indistinct bedding.						JT PL RO
		42	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL RO calcite
		68	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷							Calcite fissures <1mm thick SP
		41	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL calcite
		69	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷	BRECCIA; fine to coarse grained, dark grey, indistinct bedding.						JT PL calcite (2 parallel)
		40	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL calcite
		70	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL calcite
		39	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL calcite
		71	▼ ▲ ▽ △ ▷ ▵ ▶ ▴ ▽ △ ▷	BRECCIA; fine to coarse grained, light grey, indistinct bedding.			D A	4.674.36		calcite vein PL <1mm thick
		38	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL calcite
		72	△ ▽ ▲ ▷ ▵ ▶ ▴ ▽ △ ▷							JT PL RO
										Calcite vein PL <1mm thick
										JT PL
										Calcite vein <1mm thick PL
										JT PL RO
										JT PL RO calcite

General Defect Description:

METHOD		water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS		water level	D -diametral	FR -fresh	EL -extremely low	J1 -joint
AD			A -axial	SW -slightly	VL -very low	PT -pitting
R				MW -moderately	L -low	SM -seam
W				HW -highly	M -medium	CL -clay
NMLC	core drilling	*	not measured	EW -extremely	H -high	RO -rough
-NO.HO	core drilling		Drilling Water		VH -very high	DC -decomposed
	casing used				EH -extremely high	PL -planar
	barrel withdrawn					IR -irregular
			core recovered (hatching indicates material)			
			no core recovered			



S8463/3
BH 102

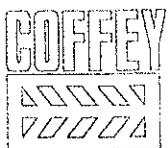
FROM 69.0 M
TO 76.0 M



S8463/3
BH 102

FROM 76.0 M
TO 83.0 M

BH 102 - 10



borehole no:
102
sheet 11 of 13

office job no: S8463/4

hole commenced: 4.12.89
hole completed: 4.12.89
logged by: SRM
checked by: PLV

engineering log cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	4.12.89
principal:					hole completed:	4.12.89
project:	OLD MANS VALLEY				logged by:	SRM
borehole location:	E 308518.10 N 1269889.83				checked by:	PLV
drill model and mounting:	PIONEER B40 TRUCK				slope:	-65 DEG
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	80deg	R.L.Surface: 103.1 m datum: AHD
drilling information	rock substance				rock mass defects	
method	core-lift	water	R.L.	depth metres	graphic log core loss	substance description
						rock type: grain characteristics colour, structure, minor components
						weathering
						Est. Strength
						point load test is(50) MPa
						defect spacing mm
						defect description
						type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ				73		BRECCIA: fine to coarse grained, light grey, indistinct bedding.
						FR
						JT PL calcite
						JI PL RO calcite
						JI PL RO calcite
						Calcite fissures IR <1mm thick
				74		BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding, thinly bedded.
				75		
				76		
				77		
				78		BRECCIA: medium to coarse grained, light grey, indistinct bedding.
				79		BRECCIA: fine to coarse grained, grey, - dark grey, indistinct bedding, to very thinly bedded.
				80		

General Defect Description:

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	V	D -diametral A -axial	FR -fresh	EL -extremely low	JF -joint
AD auger drilling	V		SW -slightly	VL -very low	PI -parting
R roller/tricone	V		MW -moderately	L -low	SM -seam
W washbore	*		HV -highly	M -medium	CL -clay
NMLC core drilling	Drilling Water	core recovered (hatching indicates material)	EW -extremely	H -high	RO -rough
NO,HQ core drilling		no core recovered		VH -very high	DC -decomposed
casing used	partial loss			EH -extremely high	PL -planar
barrel withdrawn	complete loss				IR -irregular



BH102 - 1



borehole no:

102

sheet 12 of 13

engineering log - cored borehole

Office job no: S8463/4

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308518.10 N 1269889.83

hole commenced:	4.12.89
hole completed:	4.12.89
logged by:	SRM
checked by:	PLV

drill model and mounting: PIONEER B40 TRUCK slope: -65 DEG R.L.Surface: 103.1 m
 barrel type and length: NQ 3m fluid: WATER bearing: 80deg datum: AHD

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS	
AS	auger screwing		water level	D -diametral	EL -extremely low	JT -joint
AD	auger drilling		water inflow	A -axial	VL -very low	PT -parting
R	roller/Iricon		not measured	GRAPHIC LOG/CORE LOSS	L -low	SM -seam
W	washbore	*	Drilling Water		MW -moderately	CL -clay
NMLC	core drilling		partial loss		HW -highly	RO -rough
NQ,HQ	core drilling		complete loss	no core recovered	EW -extremely	DC -decomposed
	casing used barrel withdrawn				PL -planar	
					IR -irregular	



8463/3
BH 102

engineering log - cored borehole

office job no: S8463/4

102

sheet 13 of 13

hole commenced: 4.12.89

hole completed: 4.12.89

logged by: SRM

checked by: PLV

-65 DEG R.L.Surface

80deg datum: AHD

rock mass defects

detect description

defect defect description
spacing type, inclination, planarity, roughness,
min coating, thickness
unless otherwise noted, defects follow

client:	HORNSBY SHIRE COUNCIL					hole commenced:	4.12.89		
principal:	OLD MANS VALLEY					hole completed:	4.12.89		
project:	E 308518.10 N 1269889.83					logged by:	SRM		
borehole location:						checked by:	PLV		
drill model and mounting:	PIONEER B40 TRUCK		slope:	-65 DEG	R.L.Surface:	103.1	m		
borehole type and length:	NQ 3m	fluid:	WATER	bearing:	80deg	datum:	AHD		
drilling information		rock substance			rock mass defects				
method	case-lift	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test: Is(50) MPa	defect spacing mm	defect description type, inclination, planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ		23		BRECCIA: fine to coarse grained, dark grey, - grey, indistinct bedding, some dolerite clasts to 50mm diameter.	FR			100 200 300 400 500	JT PL calcite JT PL
		89							JT PL RO calcite JT PL calcite
		22							Calcite veins IR 3mm thick Calcite veins IR 3mm thick
		90							Calcite veins 1mm thick IR
		21							
		91							
		20							
		92							
		19							
		93							
		18							
		94							
		17							
		95							
		96							
		97							JT (2 parallel) PL 5mm spacings

General Defect Description: Vehicle 102 Terminated at 96.00 m

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD	auger drilling	A -axial	SW -slightly	VL -very low	PT -parting
R	roller/tricone		MW -moderately	L -low	SM -seam
W	washbore		HW -highly	H -high	CL -clay
NMLC	core drilling	* not measured	EW -extremely	VH -very high	RO -rough
NQ,HQ	core drilling	Drilling Water		EH -extremely high	DC -decomposed
	casing used	partial loss			PL -planar
	barrel withdrawn	complete loss			IR -irregular
		core recovered (hatching indicates material)			
		no core recovered			



office job no: S8463/3

borehole no:

103

sheet 1 of 13

engineering log - borehole

client: principal: project: borehole location:	HORNSBY SHIRE COUNCIL OLD MANS VALLEY E308469.08 N1269764.16				hole commenced: hole completed: logged by: checked by:	14.12.89 20.12.89 SRM PLV
drill model and mounting:	B40 TRUCK				slope: bearing:	-65 DEG 142deg
hole diameter:	76mm				R.L Surface: datum:	112.6 m AHD
method 1 2 3	penetration support	water	notes samples, test,etc	R.L. depth metres	graphic log classification symbol	material soil type: plasticity or particle characteristics colour, secondary and minor components
R	C			112	GP	FILL: Gravel fine to coarse grained light grey. Sand fine to coarse grained Clay medium plasticity.
				111	CL	GRAVELLY CLAY: medium plasticity, red brown. Gravel, fine to coarse grained, some fine to coarse sand
				110		
				109		
				108		
				107		
				106		Commenced coring at 6.2m
				105		
				104		
				103		
				102		
				101		
				100		
				99		
				98		
				97		
				96		
				95		
				94		
				93		
				92		
				91		
				90		
				89		
				88		
				87		
				86		
				85		
				84		
				83		
				82		
				81		
				80		
				79		
				78		
				77		
				76		
				75		
				74		
				73		
				72		
				71		
				70		
				69		
				68		
				67		
				66		
				65		
				64		
				63		
				62		
				61		
				60		
				59		
				58		
				57		
				56		
				55		
				54		
				53		
				52		
				51		
				50		
				49		
				48		
				47		
				46		
				45		
				44		
				43		
				42		
				41		
				40		
				39		
				38		
				37		
				36		
				35		
				34		
				33		
				32		
				31		
				30		
				29		
				28		
				27		
				26		
				25		
				24		
				23		
				22		
				21		
				20		
				19		
				18		
				17		
				16		
				15		
				14		
				13		
				12		
				11		
				10		
				9		
				8		
				7		
				6		
				5		
				4		
				3		
				2		
				1		
				0		
				A		
METHOD	SUPPORT	NOTES	samples and tests	CLASSIFICATION SYMBOLS AND SOIL DESCRIPTION	CONSISTENCY/DENSITY INDEX	
AS auger screwing*	C casing	U50	undisturbed sample 50 mm diameter	based on unified classification system	VS very soft	
AD auger drilling*	M mud	D disturbed sample	Moisture	S soft		
R roller/tricone	PENETRATION 1 2 3	N standard penetration test	D dry			
W washbore	no resistance ranging to refusal	N* SPT + sample recovered	M moist			
CT cable tool		Nc SPT with solid cone	W wet			
HA hand auger		V vane shear	Wp plastic limit			
DT diatube		P pressuremeter				
*bit shown by suffix		Bs bulk sample				
B blank bit		R refusal				
V V bit						
T TC bit						
e.g. ADT						
	WATER *					
	water level					
	water outflow					
	water inflow					



S8463/4
BH 103

FROM 6.2 M
TO 13.0 M

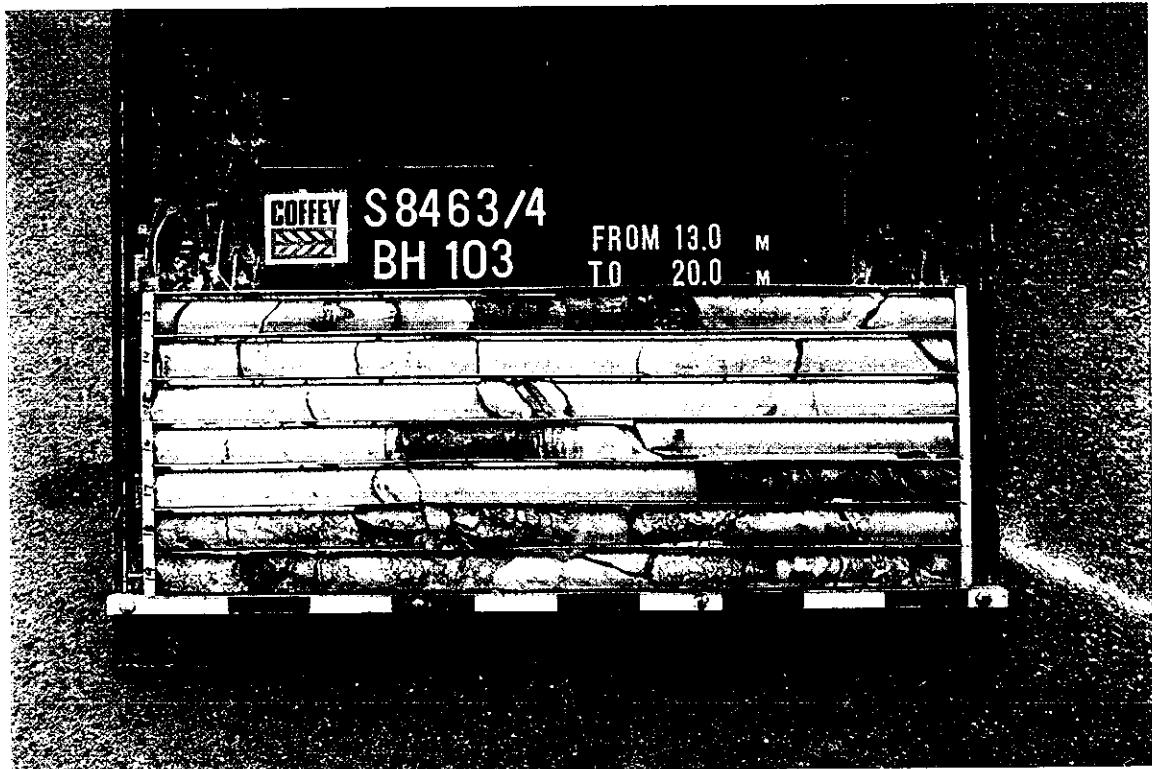
BHAC6 - 1



borehole no:
103
sheet 2 of 13
office job no: S8463/4

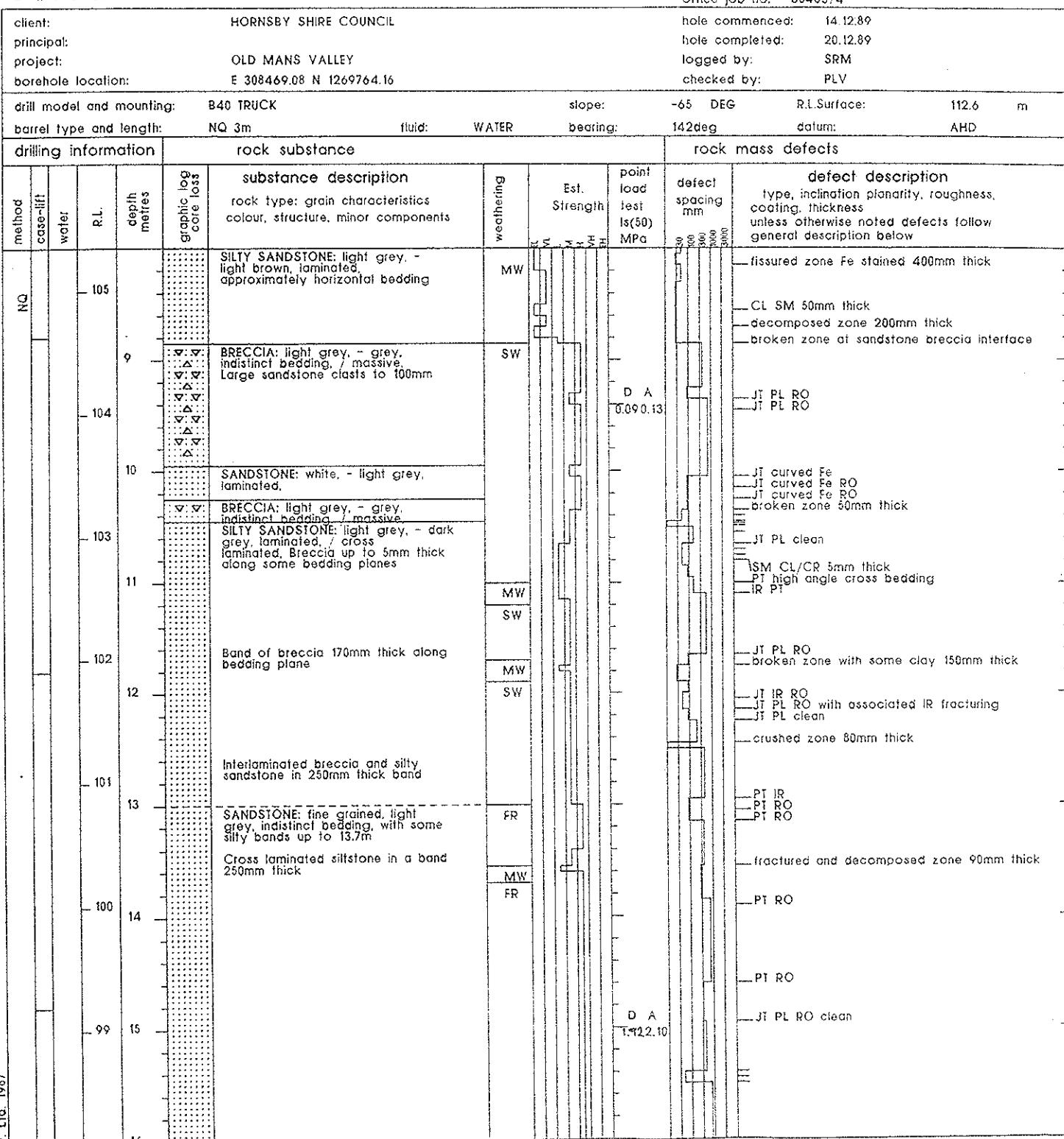
engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL					hole commenced:	14.12.89	
principal:						hole completed:	20.12.89	
project:	OLD MANS VALLEY					logged by:	SRM	
borehole location:	E 308469.08 N 1269764.16					checked by:	PLV	
drill model and mounting:	B40 TRUCK		slope:	-65 DEG	R.L.Surface:	112.6	m	
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	142deg	datum:	AHD	
drilling information	rock substance					rock mass defects		
method	core-lift	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength Is(50) MPa	point load test Is(50) MPa	defect spacing mm
	water	R.L.			S	X	NH	30 100 300 3000 (%)
		112	1					
		111	2					
		110	3					
		109	4					
		108	5					
		107	6					
		106	7					
Continued from non-core borehole								
NO CORE: 0.8m								
BRECCIA: fine grained, light grey. - brown, indistinct bedding.								
BRECCIA: fine grained, red, brown.								
NO CORE: 0.45m								
fissured zone 300mm thick EW / decomposed zone 250mm thick								
decomposed zone 150mm thick								
General Defect Description: Partings 0-10deg								
METHOD				POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS	
AS	auger screwing	▽	water level	D -diametral	FR -fresh	EL -extremely low	JT -joint	
AD	auger drilling	△	water inflow	A -axial	SW -slightly	VL -very low	PT -parting	
R	roller/tricone	* △	not measured	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam	
W	washbore	*	Drilling Water	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay	
NMLC	core drilling	△	partial loss	no core recovered	EW -extremely	H -high	RO -rough	
NQ,HQ	core drilling	△	complete loss			VH -very high	DC -decomposed	
II	casing used	△				EH -extremely high	PL -planar	
	barrel withdrawn						IR -irregular	



BH103-2

engineering log - cored borehole



General Defect Description:
Partings 0-10deg

METHOD	WATER LEVEL	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	V water level	D -diametral A -axial	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	V water inflow		SW -slightly	VL -very low	PT -parting
R roller/tricone	V water inflow		MW -moderately	L -low	SM -seam
W washbore	*		HW -highly	M -medium	CL -clay
NMLC core drilling	not measured	core recovered (hatching indicates material)	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	Drilling Water	no core recovered		VH -very high	DC -decomposed
casing used	partial loss			EH -extremely high	PL -planar
barrel withdrawn	complete loss				IR -irregular



BH 103 - 3



borehole no:

103

sheet 4 of 13

engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL			hole commenced:	14.12.89							
principal:				hole completed:	20.12.89							
project:	OLD MANS VALLEY			logged by:	SRM							
borehole location:	E 308469.08 N 1269764.16			checked by:	PLV							
drill model and mounting:	B40 TRUCK	slope:	-65 DEG	R.L.Surface:	112.6	m						
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	142deg	datum: AHD						
drilling information	rock substance				rock mass defects							
method	core-lift	water	R.L.	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test Is(50) MPa	defect spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below	
NQ			98		SANDSTONE: fine grained, light grey, indistinct bedding, with some silty bands up to 13.7m Breccia layer 150mm thick	SW			300 330 360 390			PT broken 5mm thick
			97	17		FR						JT PL
			96	18	SANDSTONE: fine grained, dark grey, - grey, laminated, laminated, / cross laminated, some carbonaceous material, including coal	SW						CR/CL SM 30mm thick cleats in coal with <5mm spacings broken zone 40mm thick fissured and broken zone 100mm thick
			95	19	BRECCIA: fine to coarse grained, light grey, dark grey, massive, clasts of sandstone and limestone(?) up to 100mm Sandstone 130mm thick							JT PL CL smear fissured zone around JT to 18.45
			94	20	Sandstone 120mm thick Sandstone 180mm thick Sandstone 120mm thick							PT on breccia sandstone contact JT CU PT PL broken zone 100mm thick
			93	21	SANDSTONE: fine to medium grained, grey, indistinct bedding, becoming silty sandstone at 20.9m BRECCIA: fine to coarse grained, light grey, - grey,							JT PL RO decomposed zone 50mm thick broken zone 100mm thick
			92	22	SANDY SILSTONE: fine grained, grey, - light grey, laminated, / cross laminated							JT PL decomposed zone of partings 100mm thick
			91	23								JT PL polished fissured zone 200mm thick
					SILTSTONE: fine grained, dark grey, laminated, carbonaceous with bands of coal							JT PL polished fractured zone 200mm thick fragmented zone 150mm thick
												fissured zone 23.35-23.55
												JT PL polished broken zone 23.7-23.9
												IT IR CL RO

General Defect Description:
Partings 0-5deg

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	▽ water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	▽ water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/Iriconic	* not measured	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W washbore	Drilling Water	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay
NMLC core drilling	partial loss	no core recovered	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	complete loss			VH -very high	DC -decomposed
casing used				EH -extremely high	PL -planar
barrel withdrawn					IR -irregular



S8463/4
BH 103

FROM 27.0 M
TO 34.0 M

NO CORE

BH103-4



borehole no:
103
sheet 5 of 13

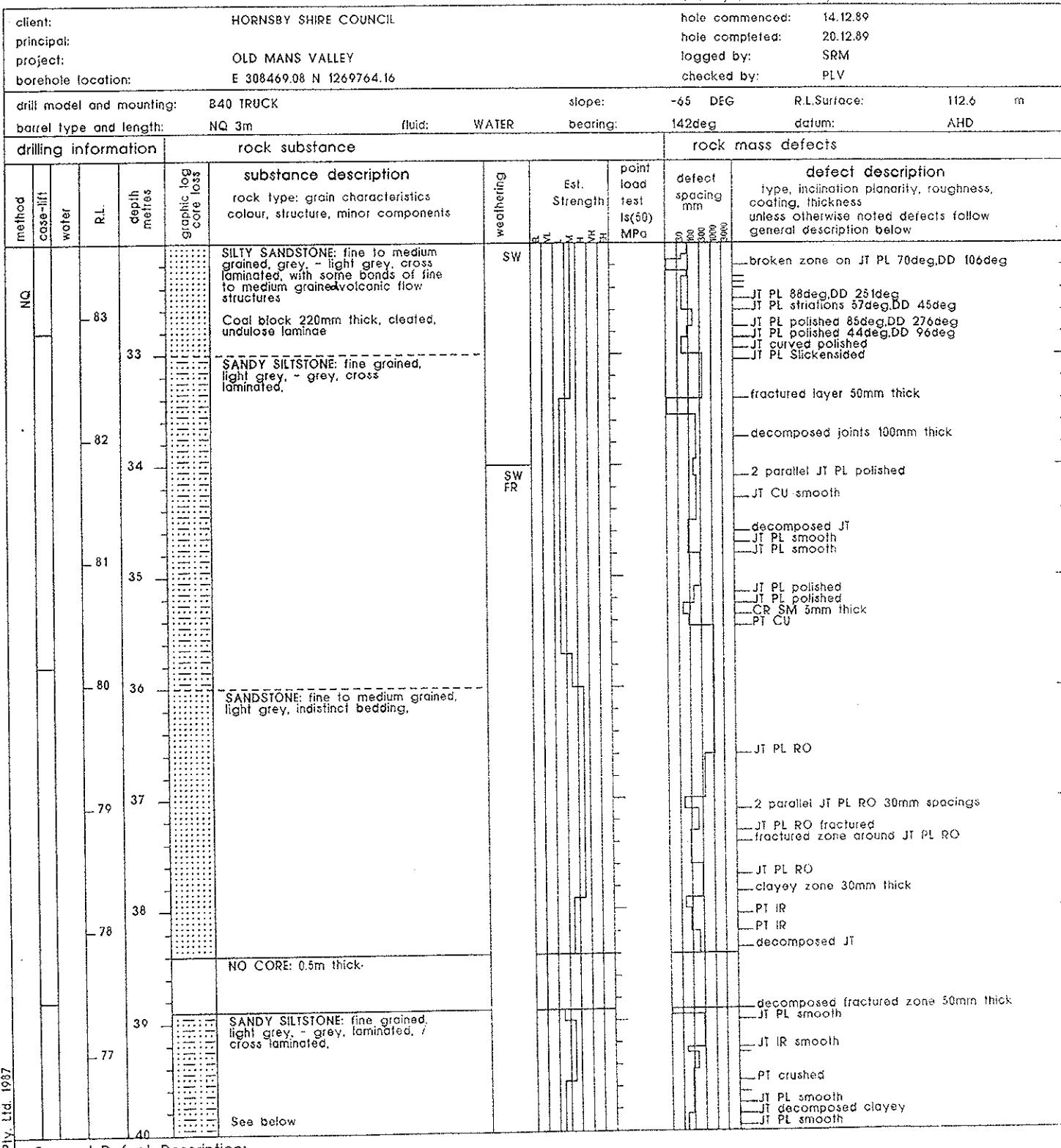
engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	14.12.89		
principal:					hole completed:	20.12.89		
project:	OLD MANS VALLEY				logged by:	SRM		
borehole location:	E 308469.08 N 1269764.16				checked by:	PLV		
drill model and mounting:	B40 TRUCK		slope:	-65 DEG	R.L.Surface:	112.6	m	
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	142deg	datum:	AHD	
drilling information		rock substance			rock mass defects			
method	casing-lift	depth metres	graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength Is(50) MPa	point load test spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
					SW		100 200 300 500 1000 3000	
	NQ			SILTSTONE: fine grained, dark grey, laminated, carbonaceous with bands of coal				broken layer 10mm thick JT PL polished fractured zone including coal cleats 100mm CL SM 10mm thick
				SILTY SANDSTONE: fine to medium grained, grey - light grey, cross laminated, with some bands of fine to medium grained volcanic flow structures 70mm thick band of breccia coal ply 200mm thick				JT PL smooth broken zone 50mm thick JT PL RO broken zone 50mm thick
		90	25					
		89	26					
		88	27					
		87	28					
		86	29					
		85	30					
		84	31					
					SW			
		83	32					
General Defect Description: Partings 0-5deg								
METHOD				POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS	
AS auger screwing	▽	water level	D -diametral	FR -fresh	EL -extremely low	JT -joint		
AD auger drilling	▽	water inflow	A -axial	VL -very low	PT -parting			
R roller/tricone	*	not measured	GRAPHIC LOG/CORE LOSS	L -low	SM -seam			
W washbore	Drilling Water	core recovered (hatching indicates material)	SW -slightly	M -medium	CL -clay			
NMLC core drilling	partial loss	no core recovered	MW -moderately	H -high	RO -rough			
NQ,HQ core drilling	complete loss		HW -highly	VH -very high	DC -decomposed			
casing used			EW -extremely	EH -extremely high	PL -planar			
barrel withdrawn					IR -irregular			



BH 103-5

engineering log - cored borehole





S 8463/4
BH 103

FROM 41.0 M
TO 48.0 M

8463/4
BH 103

engineering log - cored borehole

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308469.08 N 1269764.16

office job no: S8463/4

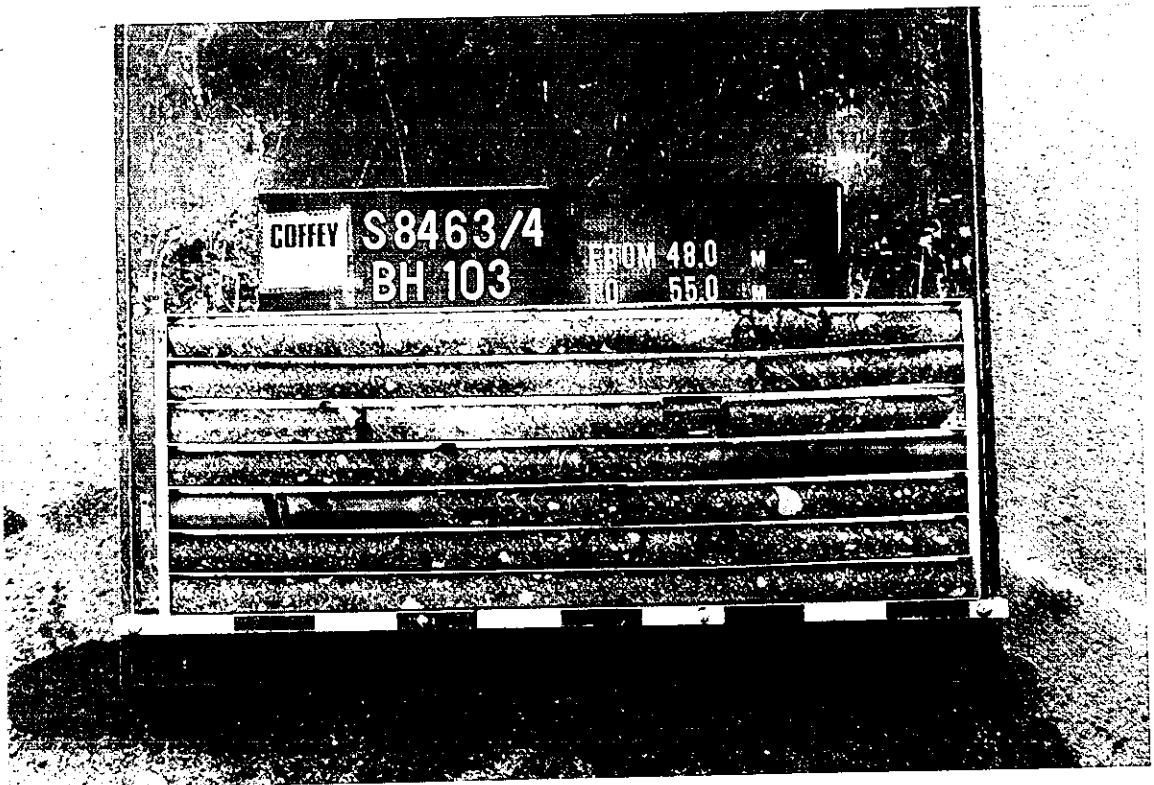
103

sheet 7 of 13

drill model and mounting: B40 TRUCK **slope:** -65 DEG **R.L.Surface:** 112.6 m
barrel type and length: NQ 3m **fluid:** WATER **bearing:** 142deg **datum:** AHD

General Defect Description:
Portings 0-5deg rough clean

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	water level	D -diametral	FR -fresh	JT -joint
AD	auger drilling		A -axial	SW -slightly	PT -parting
R	roller/Ilicone	water inflow		MW -moderately	SM -seam
W	washbore	*		HW -highly	CL -clay
NMLC	core drilling	not measured	core recovered (hatching indicates material)	VH -very high	RO -rough
NQ,HQ	core drilling	Drilling Water	no core recovered	EW -extremely	DC -decomposed
	casing used	partial loss		EH -extremely high	PL -planar
	barrel withdrawn	complete loss			IR -irregular



BH 103 - 2

engineering log - cored borehole

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308469.08 N 1269764.16

hole commenced: 14.12

hole commenced: 14.12.89
hole completed: 20.12.89
logged by: SRM
checked by: PLV

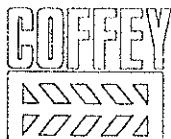
drill model and mounting: B40 TRUCK slope: -65 DEG R.L.Surface: 112.6 m
 barrel type and length: NO 3m fluid: WATER bearing: 142deg datum: AHD

General Defect Description:

METHOD		POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS	auger screwing	▽ water level	D -diametral	FR -fresh	JT -joint
AD	auger drilling	▽ water inflow	A -axial	SW -slightly	PT -parting
R	roller/tricone	* not measured		MW -moderately	SM -seam
W	washbore	Drilling Water	core recovered (hatching indicates material)	HW -highly	CL -clay
NMLC	core drilling	▽ partial loss	no core recovered	EW -extremely	RO -rough
NQ,HQ	core drilling	▽ complete loss			DC -decomposed
	casing used				PL -planar
	barrel withdrawn				IR -irregular

COFFEY S 8463/4
BH 103 FROM 55.0 M
 TO 62.0 M

BH 103 - 8



borehole no:

103

sheet 9 of 13

office job no: S8463/4

engineering log - cored borehole

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
borehole location: E 308469.08 N 1269764.16

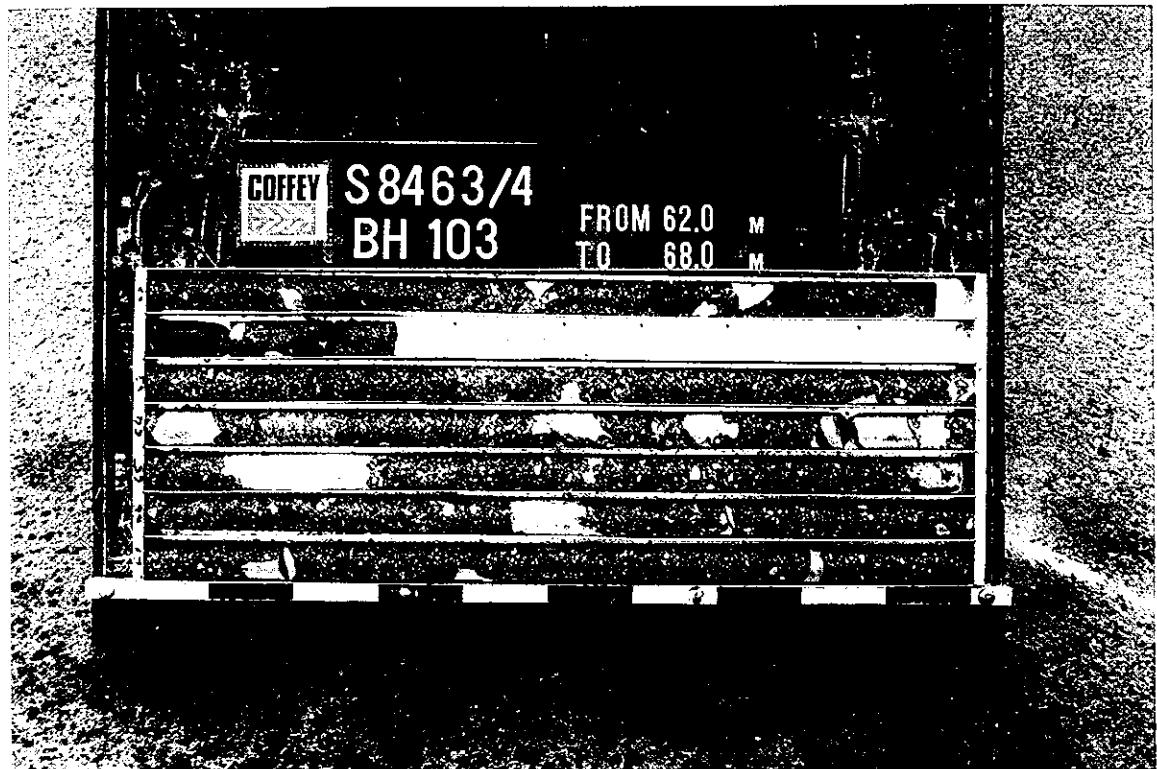
hole commenced: 14.12.89
hole completed: 20.12.89
logged by: SRM
checked by: PLV

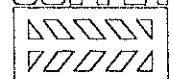
drill model and mounting: B40 TRUCK
barrel type and length: NQ 3m fluid: WATER bearing: 142deg R.L.Surface: 112.6 m datum: AHD

drilling information		rock substance				rock mass defects					
method	case-lift	water	R.L.	depth metres	graphic log core loss	substance description	weathering	Est. Strength	point load test ls(50) MPa	defect spacing mm	defect description
						rock type: grain characteristics colour, structure, minor components					type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
						BRECCIA: fine to coarse grained, dark grey, - grey massive, some clasts of fine sandstone up to 150mm across	FR	EL VL MW H VH EH	30 100 300 1000 3000		
	NQ			61							calcite filled fissures <1mm thick
				57							calcite vein PL <1mm thick
				60							calcite vein 1mm thick
				58							calcite vein 1mm thick IR
				59							calcite veins 2mm thick IR
				60							calcite veins 2mm thick IR
				58							calcite vein 4mm thick
				61							CR SM curved 3mm thick
				57							
				62							
				56							
				63							
				55							
				64							JT IR RO

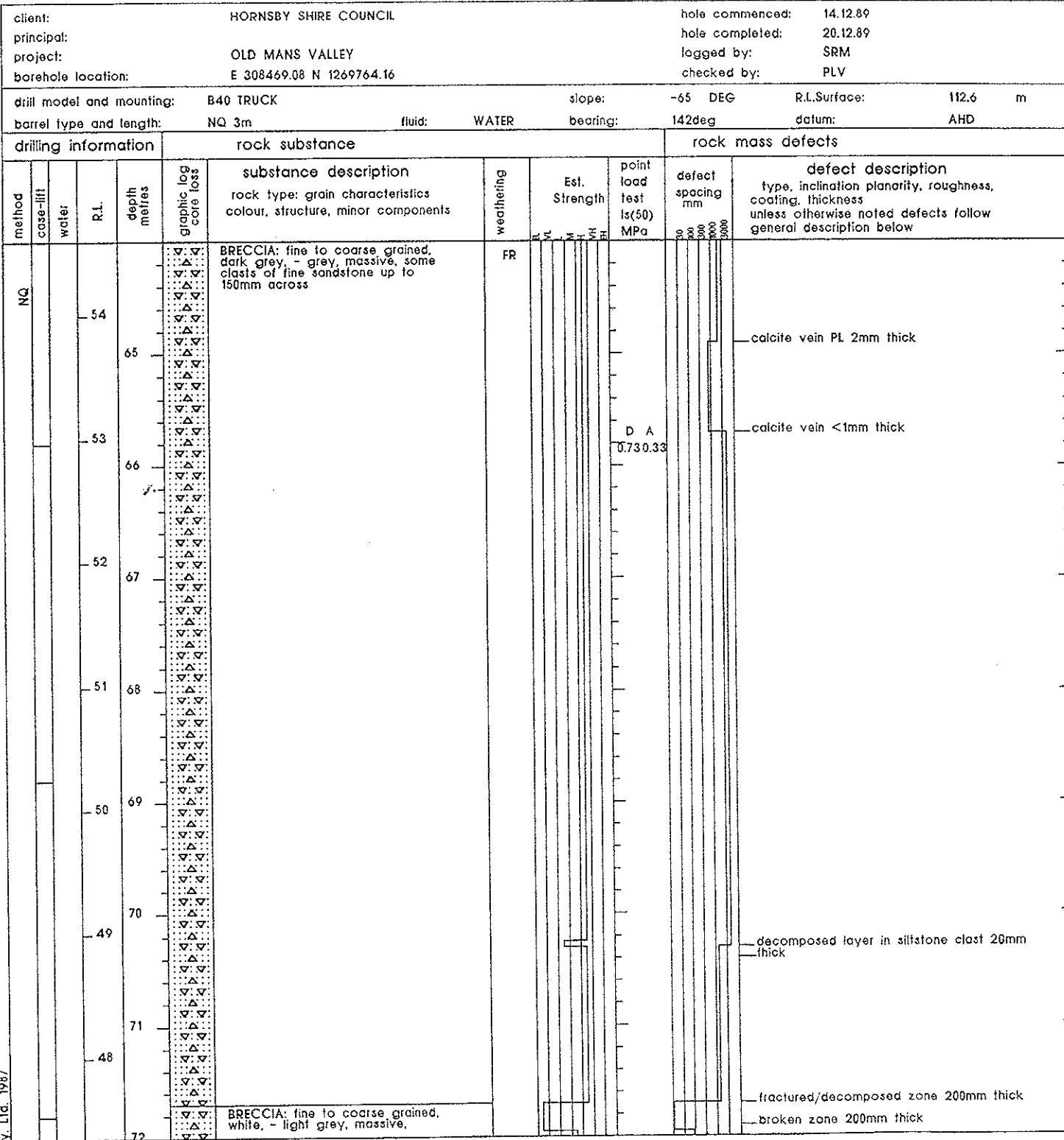
General Defect Description:

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	V water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	V water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	*	not measured	MW -moderately	L -low	SM -seam
W washbore	Drilling Water	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay
NMLC core drilling	partial loss	no core recovered	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	complete loss			VH -very high	DC -decomposed
I casing used				EH -extremely high	PL -planar
II barrel withdrawn					IR -irregular



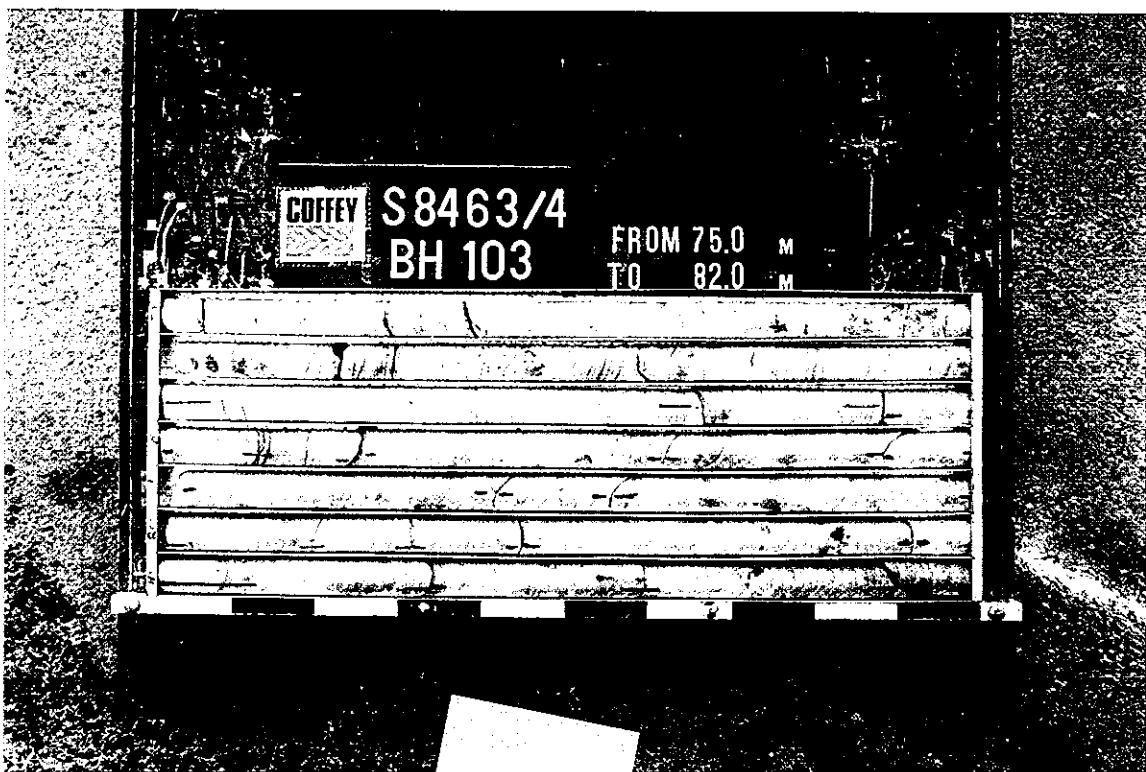


engineering log - cored borehole



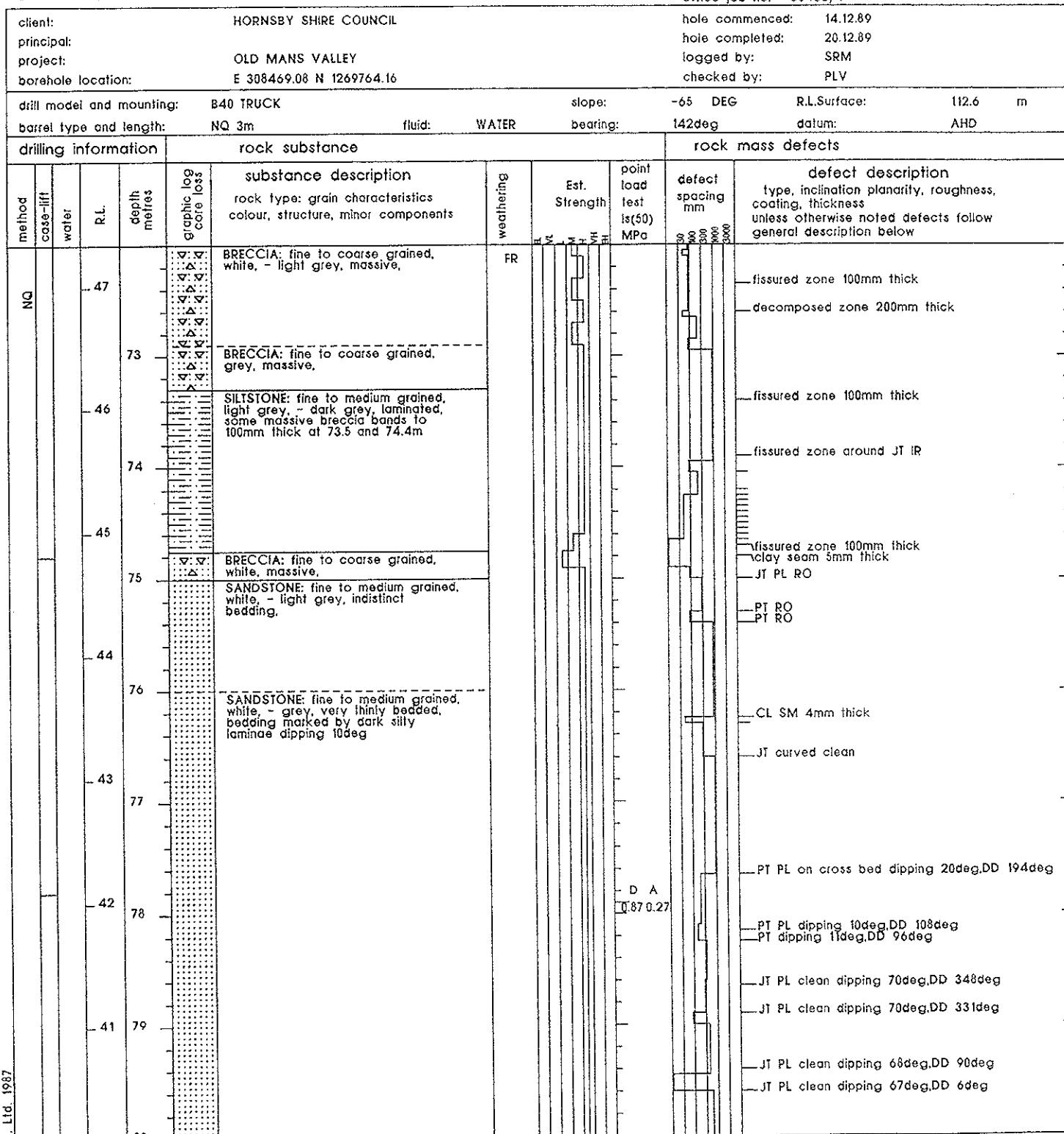
General Defect Description:

METHOD	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W washbore	* not measured	HW -highly	M -medium	CL -clay
NMLC core drilling	Drilling Water	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	partial loss		VH -very high	DC -decomposed
casing used	complete loss		EH -extremely high	PL -planar
barrel withdrawn				IR -irregular



Bit 103 - 10

engineering log - cored borehole

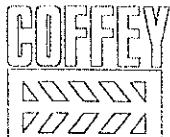


General Defect Description:
Partings 0-5deg, rough, clean

METHOD	WATER LEVEL	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	water level	D -diametral A -axial	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	water inflow	GRAPHIC LOG/CORE LOSS	SW -slightly	VL -very low	PT -parting
R roller/tricone	* not measured	core recovered (hatching indicates material)	MW -moderately	L -low	SM -seam
W washbore	Drilling Water	no core recovered	HW -highly	M -medium	CL -clay
NMLC core drilling	partial loss		EW -extremely	H -high	RO -rough
NQ,HQ core drilling	complete loss			VH -very high	DC -decomposed
casing used				EH -extremely high	PL -planar
barrel withdrawn					IR -irregular

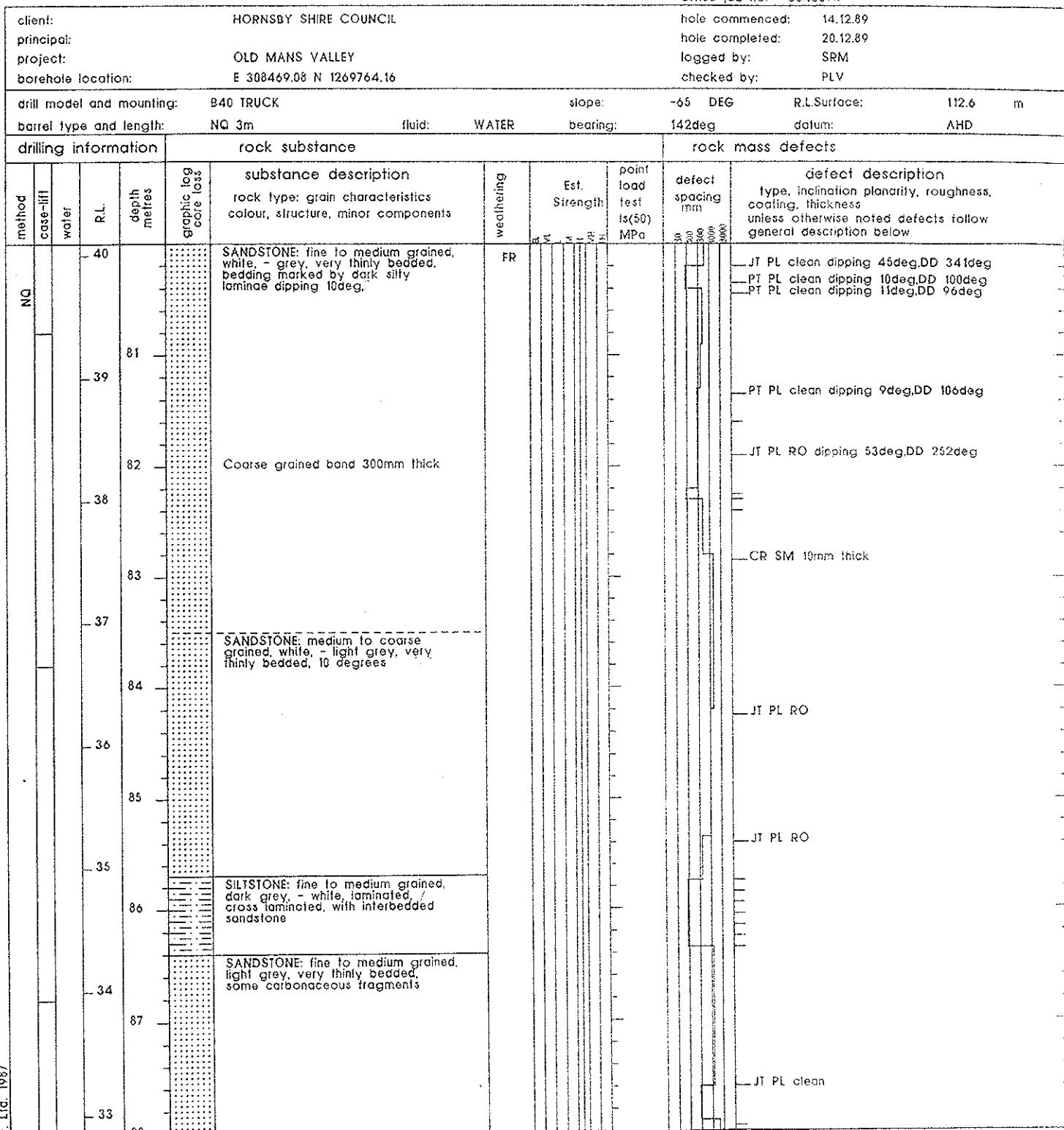


BH 103 - II



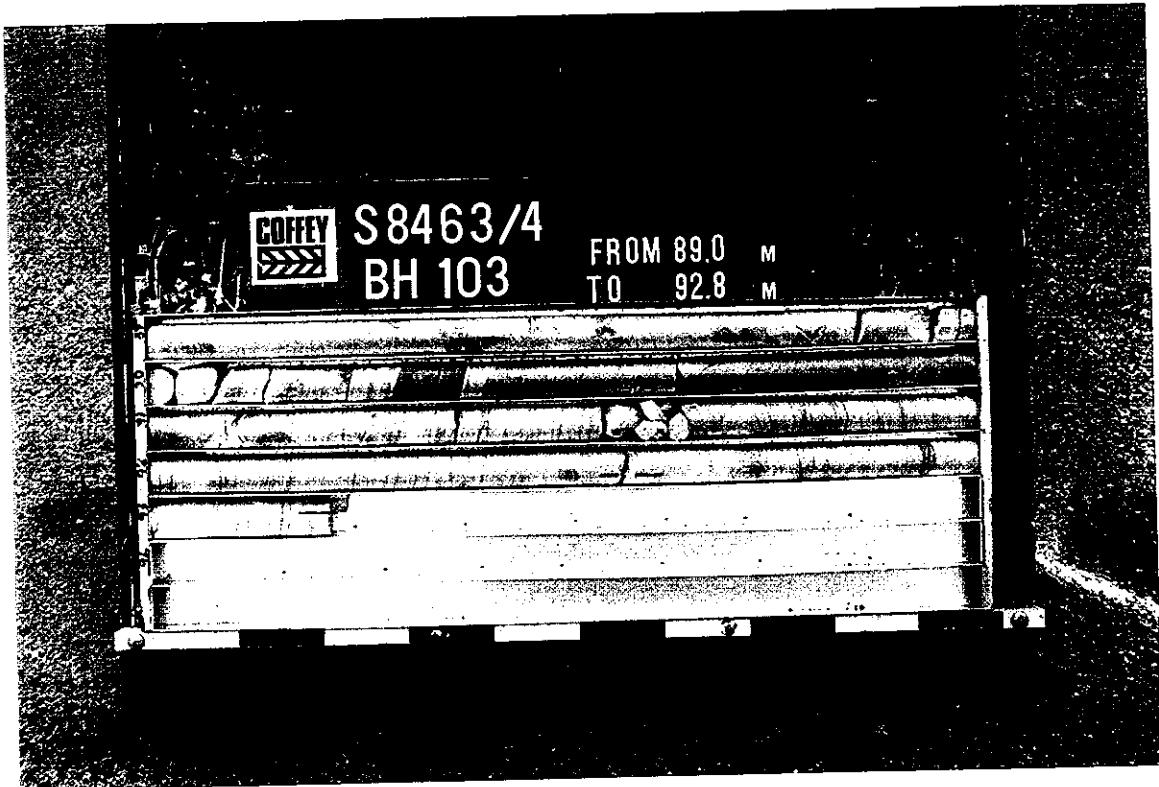
borehole no:
103
sheet 12 of 13

engineering log - cored borehole



General Defect Description:
Parting 0-5deg, planar, rough, clean

METHOD	AS	auger screwing		water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AD	AD	auger drilling		water inflow	D -diametral A -axial	FR -fresh	EL -extremely low	JT -joint
R	R	roller/tricone	*	not measured	GRAPHIC LOG/CORE LOSS	SW -slightly	VL -very low	PT -parting
W	W	washbore		Drilling Water		MW -moderately	L -low	SM -seam
NMLC	NMLC	core drilling		partial loss		HW -highly	M -medium	CL -clay
NQ,HQ	NQ,HQ	core drilling		complete loss	no core recovered	EW -extremely	H -high	RO -rough
T		casing used					VH -very high	DC -decomposed
		barrel withdrawn					EH -extremely high	PL -planar
								IR -irregular



BH103-12



borehole no:

103

sheet 13 of 13

office job no: S8463/4

engineering log - cored borehole

client:	HORNSBY SHIRE COUNCIL				hole commenced:	14.12.89					
principal:	OLD MANS VALLEY				hole completed:	20.12.89					
project:	E 308469.08 N 1269764.16				logged by:	SRM					
borehole location:					checked by:	PLV					
drill model and mounting:	B40 TRUCK		slope:	-66 DEG	R.L. Surface:	112.6 m					
barrel type and length:	NQ 3m	fluid:	WATER	bearing:	142deg	datum:	AHD				
drilling information		rock substance				rock mass defects					
method	case-lift	water	R.L.	depth metres	Graphic log core loss	substance description rock type: grain characteristics colour, structure, minor components	weathering	Est. Strength	point load test Is(50) MPa	defect spacing mm	defect description type, inclination planarity, roughness, coating, thickness unless otherwise noted defects follow general description below
NQ						SANDSTONE: fine to medium grained, light grey, very thinly bedded, some carbonaceous fragments	FR			30 60 100 200 500 1000	
				32	89						
				31	90						
				30	91						
				29	92						
				28	93	Borehole 103 Terminated at 92.80 m					
				27	94						
				26	95						
				25	96						

General Defect Description:
Partings 0-5deg, planar, rough, clean

METHOD	water level	POINT LOAD TEST	WEATHERING	STRENGTH	DEFECTS
AS auger screwing	▼ water level	D -diametral	FR -fresh	EL -extremely low	JT -joint
AD auger drilling	▼ water inflow	A -axial	SW -slightly	VL -very low	PT -parting
R roller/tricone	* not measured	GRAPHIC LOG/CORE LOSS	MW -moderately	L -low	SM -seam
W washbore	Drilling Water	core recovered (hatching indicates material)	HW -highly	M -medium	CL -clay
NMLC core drilling	partial loss	no core recovered	EW -extremely	H -high	RO -rough
NQ,HQ core drilling	complete loss			VH -very high	DC -decomposed
				EH -extremely high	PL -planar
					IR -irregular



APPENDIX B

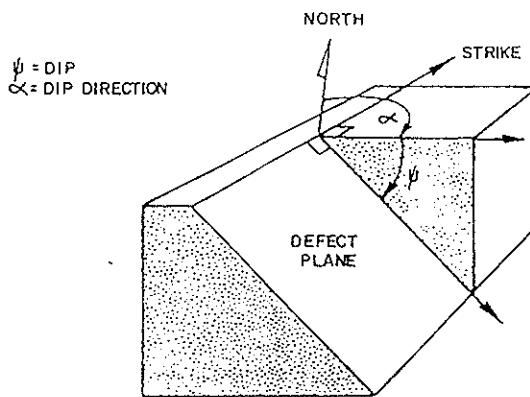
Coffey & Partners Pty. Ltd.

S8463/4-AD
3rd April, 1990

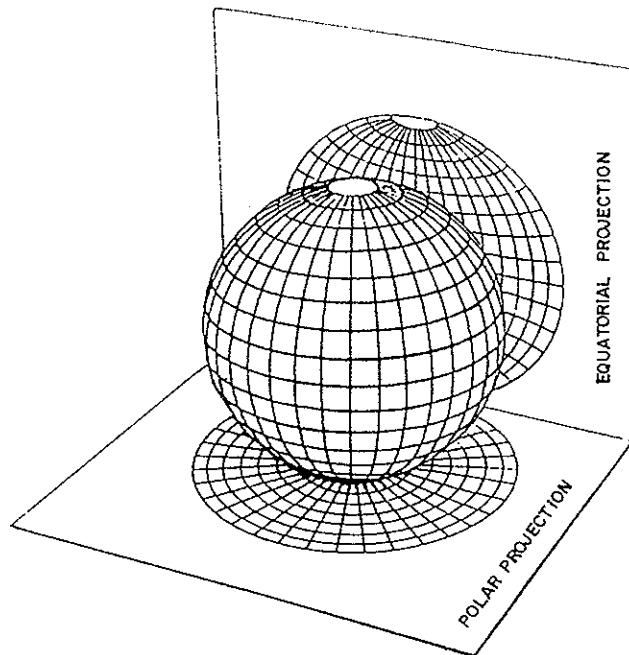


APPENDIX B

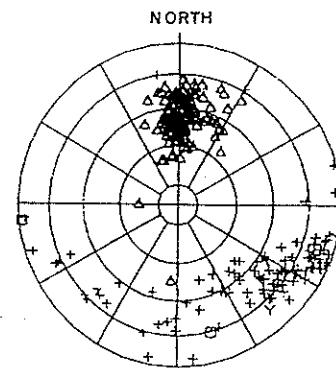
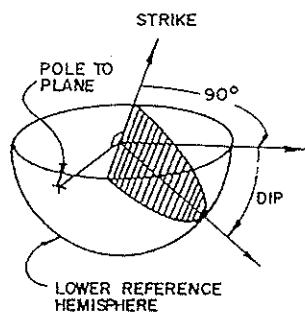
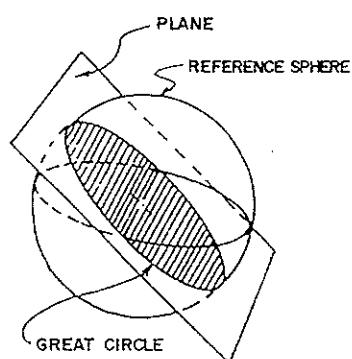
STEREOPHOTOGRAPHIC PROJECTIONS FOR ORIENTATED CORED BOREHOLES



DEFINITION OF GEOMETRICAL TERMS

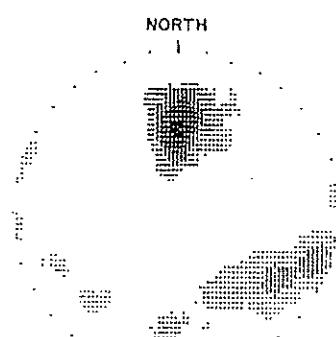
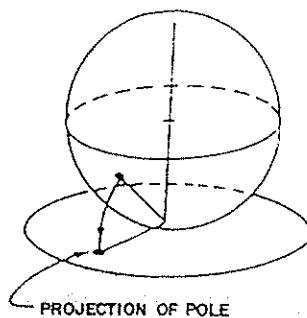


POLAR & EQUATORIAL PROJECTIONS



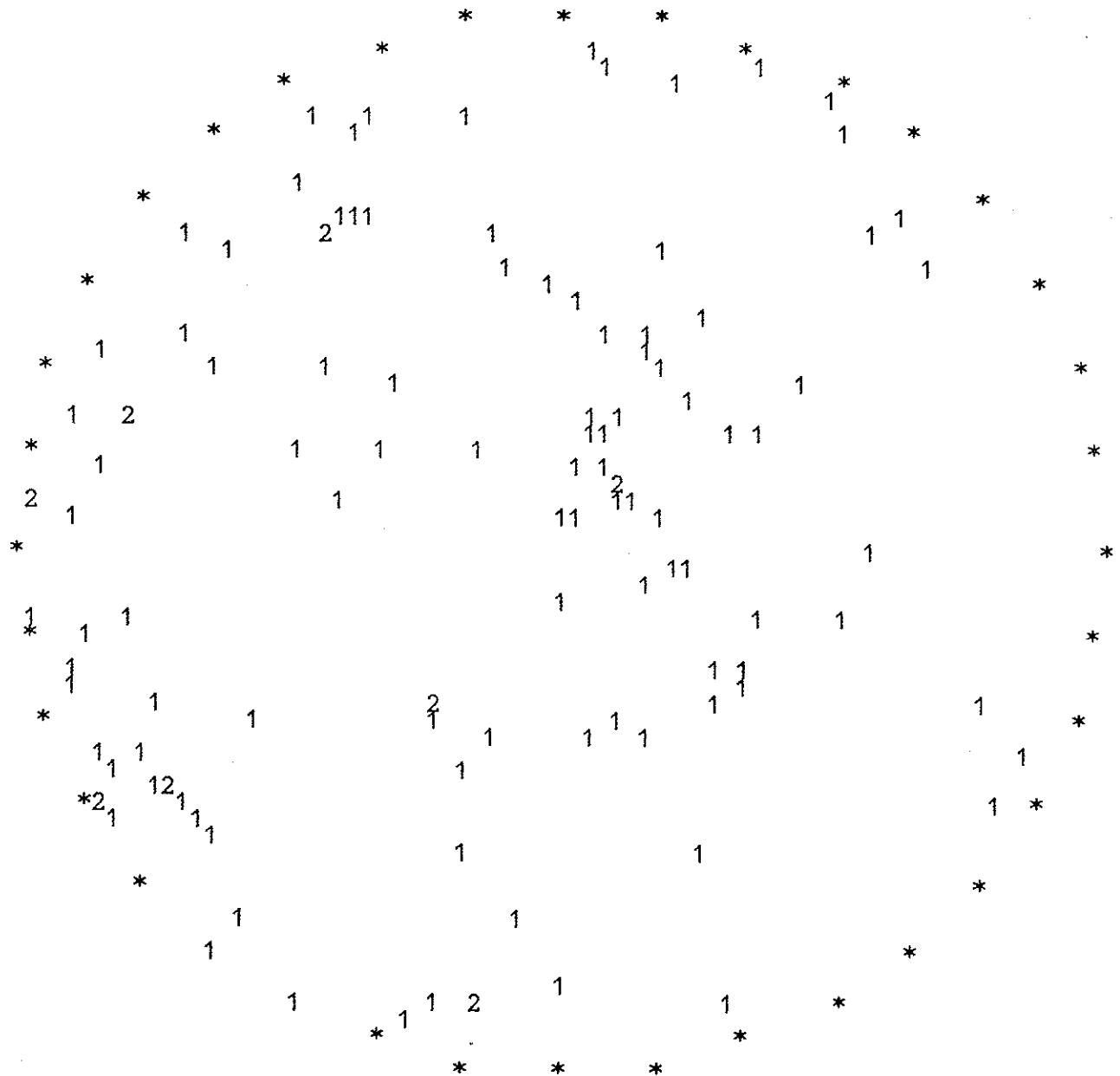
- + joint (JN)
- X fault (FL)
- △ bedding (BG)
- shear (SR)
- unconformity (UC)
- boundary (BD)
- cleavage (CV)
- contact (CN)
- gneissosity (GS)
- schistosity (SC)
- vein (VN)
- other

POLAR EQUAL-AREA STEREOGRAPHIC PROJECTION
DISPLAYING DEFECT TYPES



EQUATORIAL EQUAL-AREA STEREOGRAPHIC PROJECTION
OF ABOVE CONTOURED

Coffey & Partners Pty Ltd		Consulting Engineers in the geotechnical sciences	
drawn	PLV / LT	HORNSBY SHIRE COUNCIL OLD MANS VALLEY	COFFEY
approved		DEFINITION & PRESENTATION OF STRUCTURAL DEFECTS	FIGURE BI
date			job no S8463 / 4
scale	NOT TO SCALE		



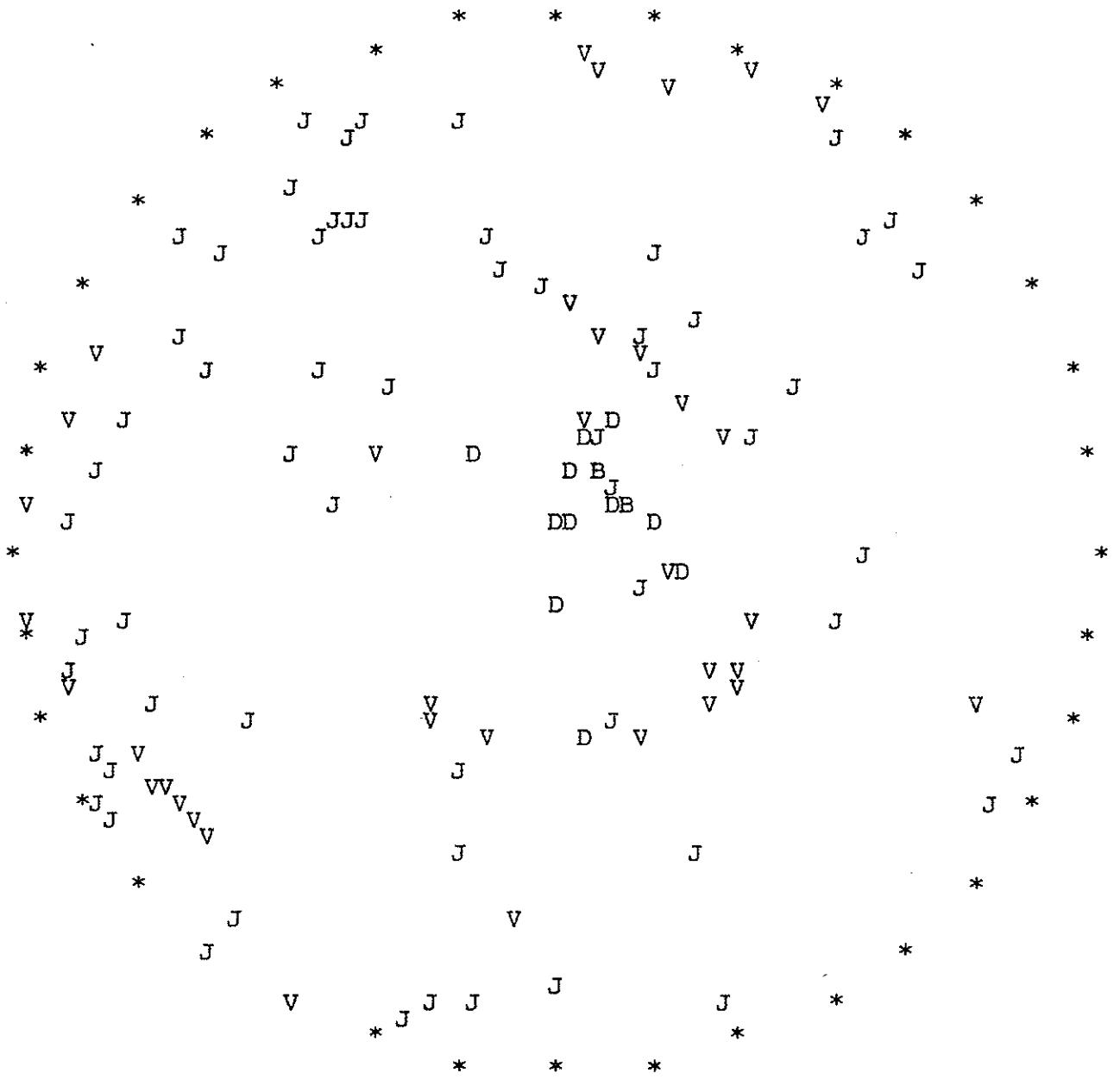
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 117

ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101
 SCATTER DIAGRAM - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 117
 ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

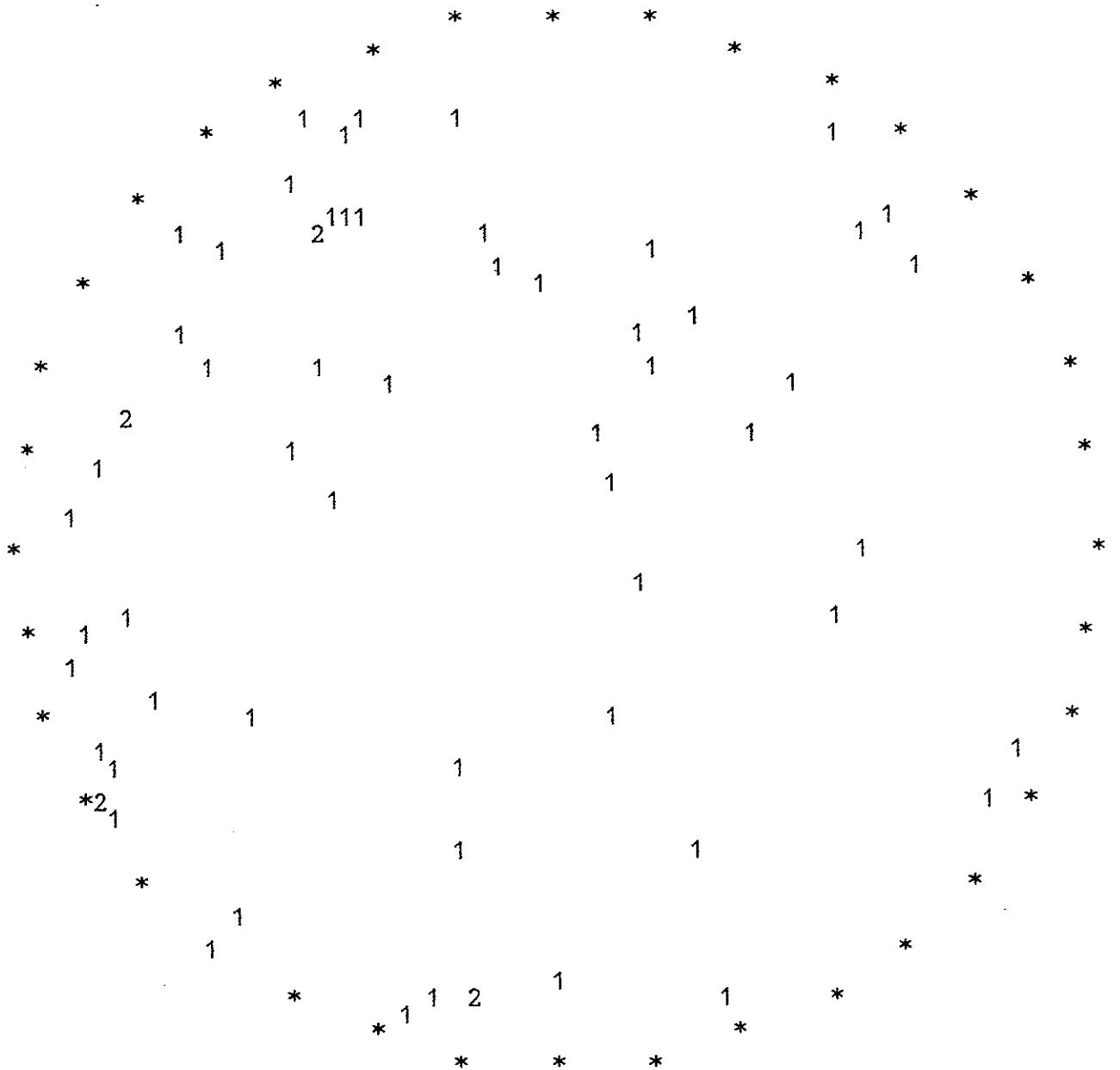
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 117

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	2%
'11'	<LT>	4%
'2'	<LT>	6%
'3'	<LT>	8%
'M'	MAX =	8.5



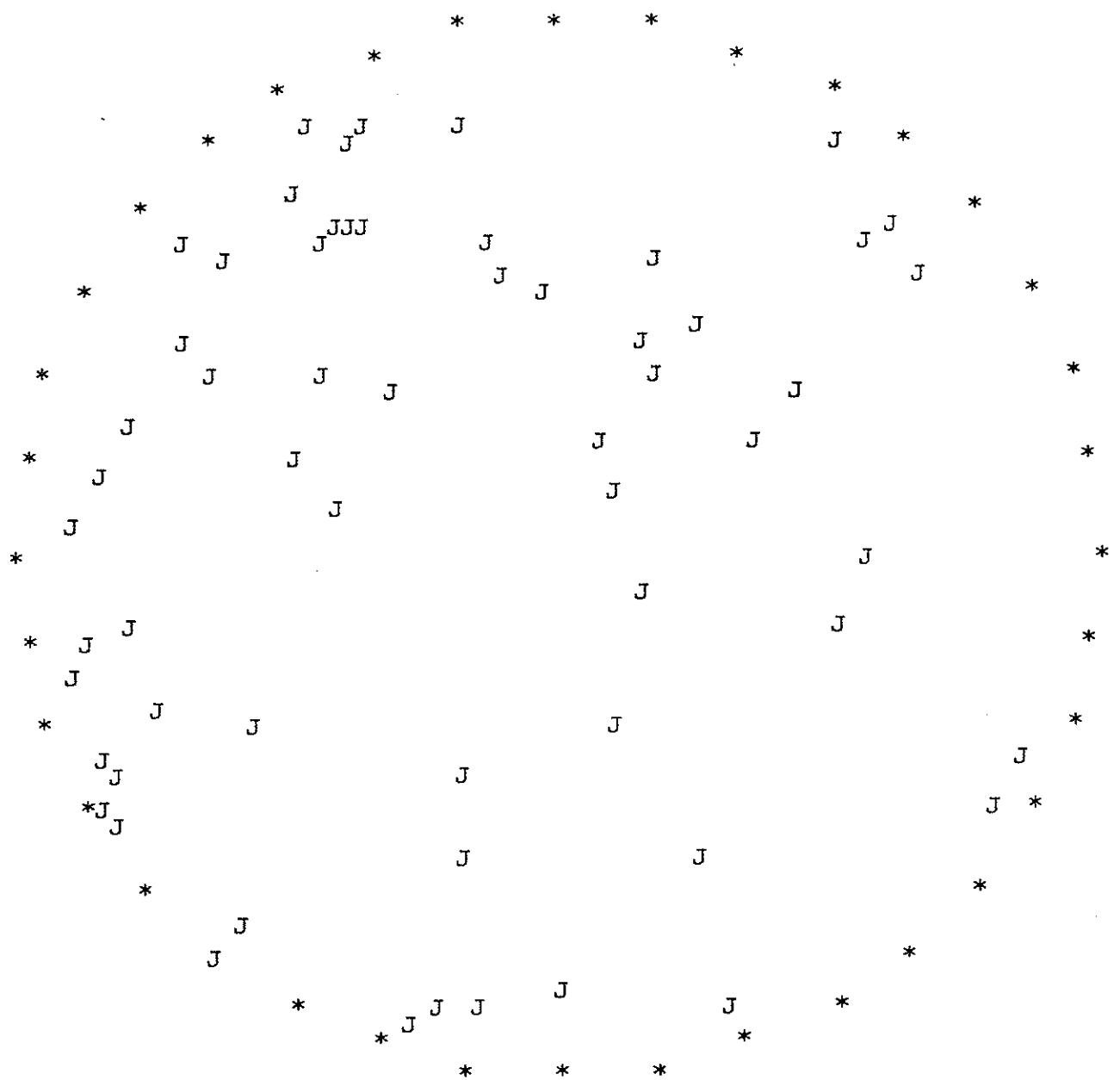
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 JOINTS

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 64

ROTATION ANGLES: 0 0 0



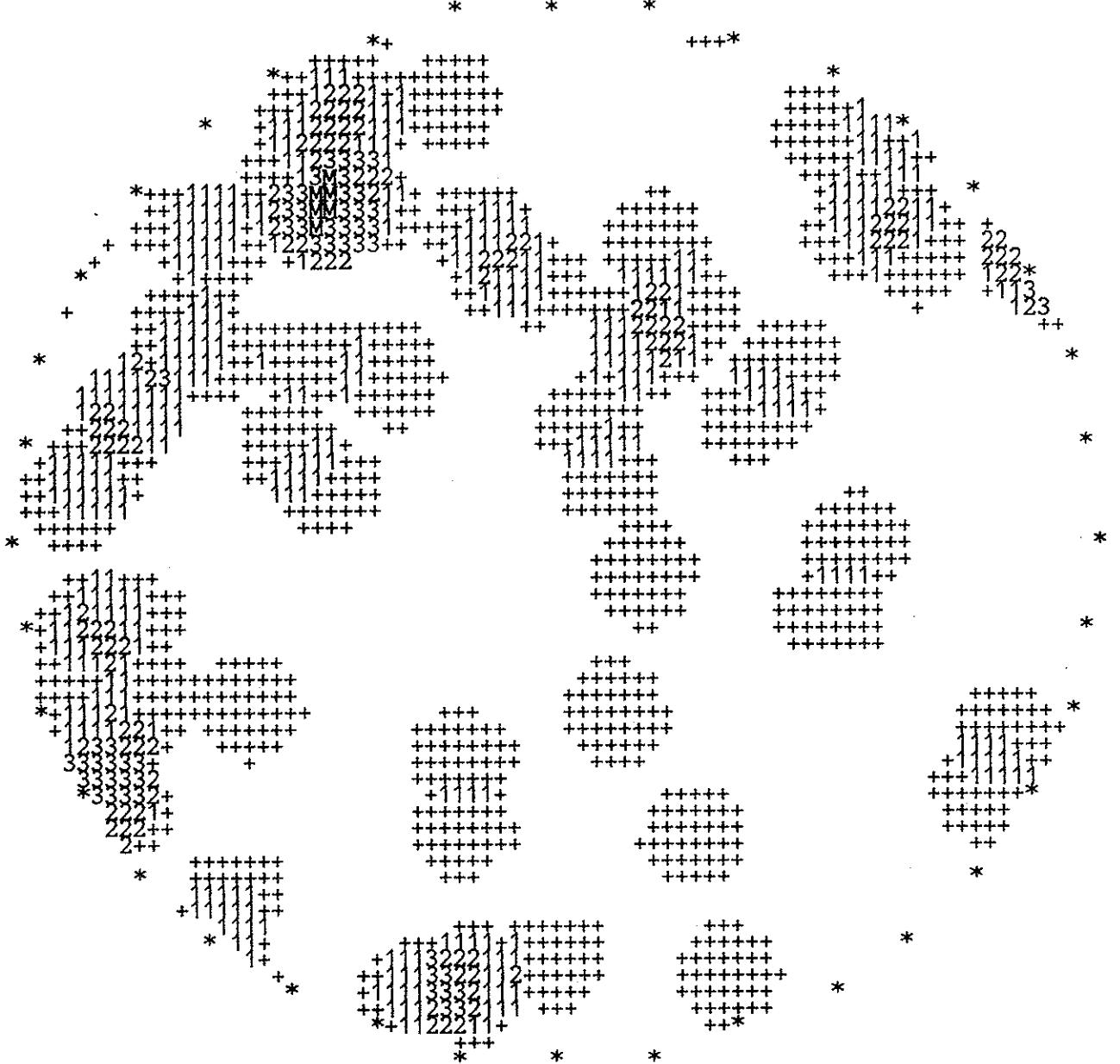
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 JOINTS

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 64

ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 JOINTS

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

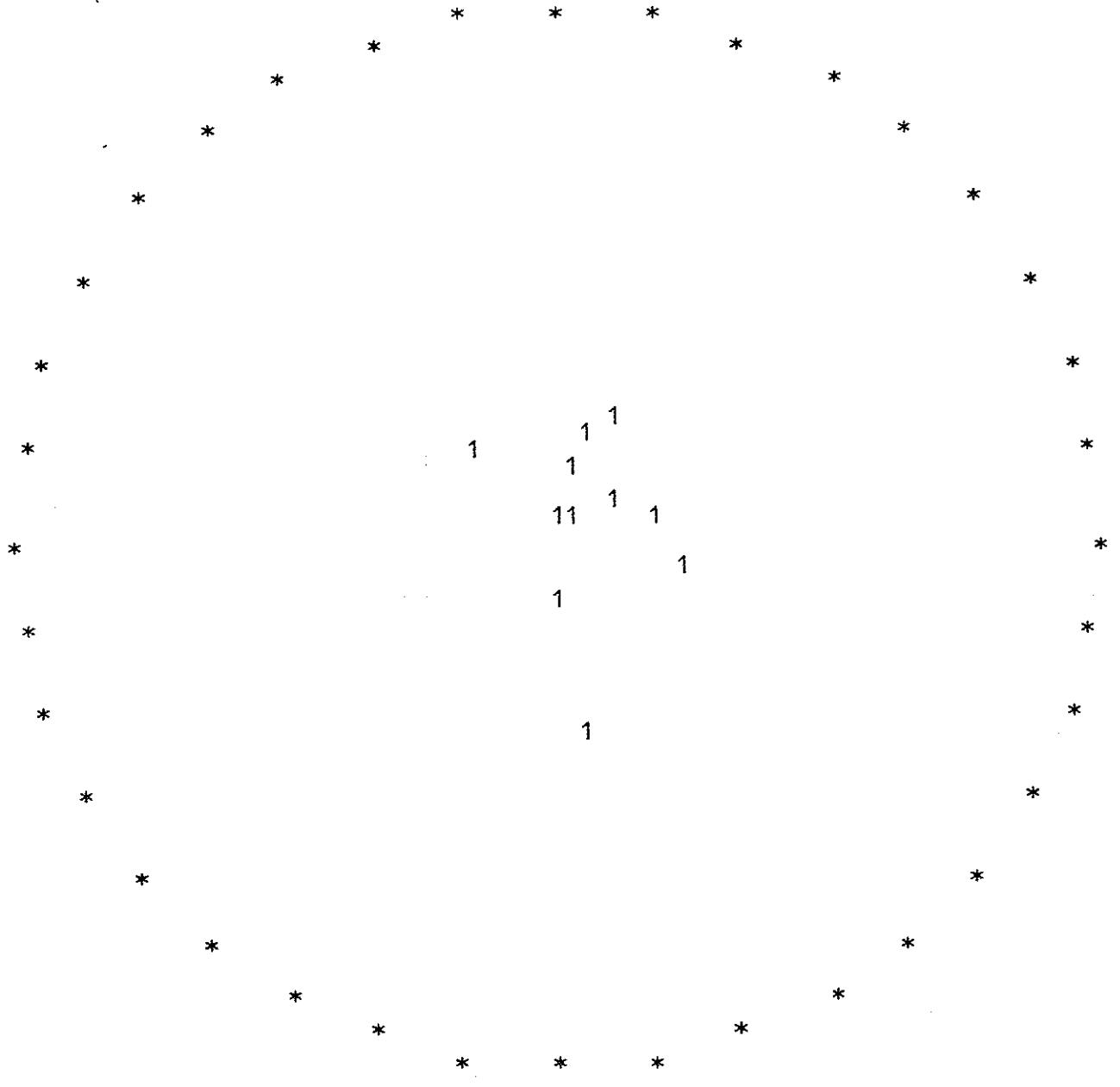
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 64

ROTATION ANGLES: 0 0 0

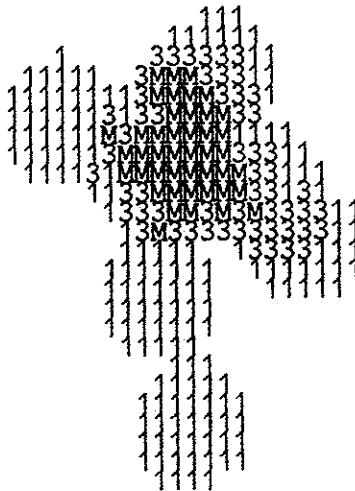
SHADING SYMBOLS

' 1'	<LT>	1%
'+'	<LT>	2%
'1'	<LT>	4%
'2'	<LT>	6%
'3'	<LT>	8%
'M'	MAX =	9.4



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 11
ROTATION ANGLES: 0 0 0

S8463/4 HORNBY SHIRE COUNCIL - BOREHOLE 101 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 11
ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 BEDDINGS

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

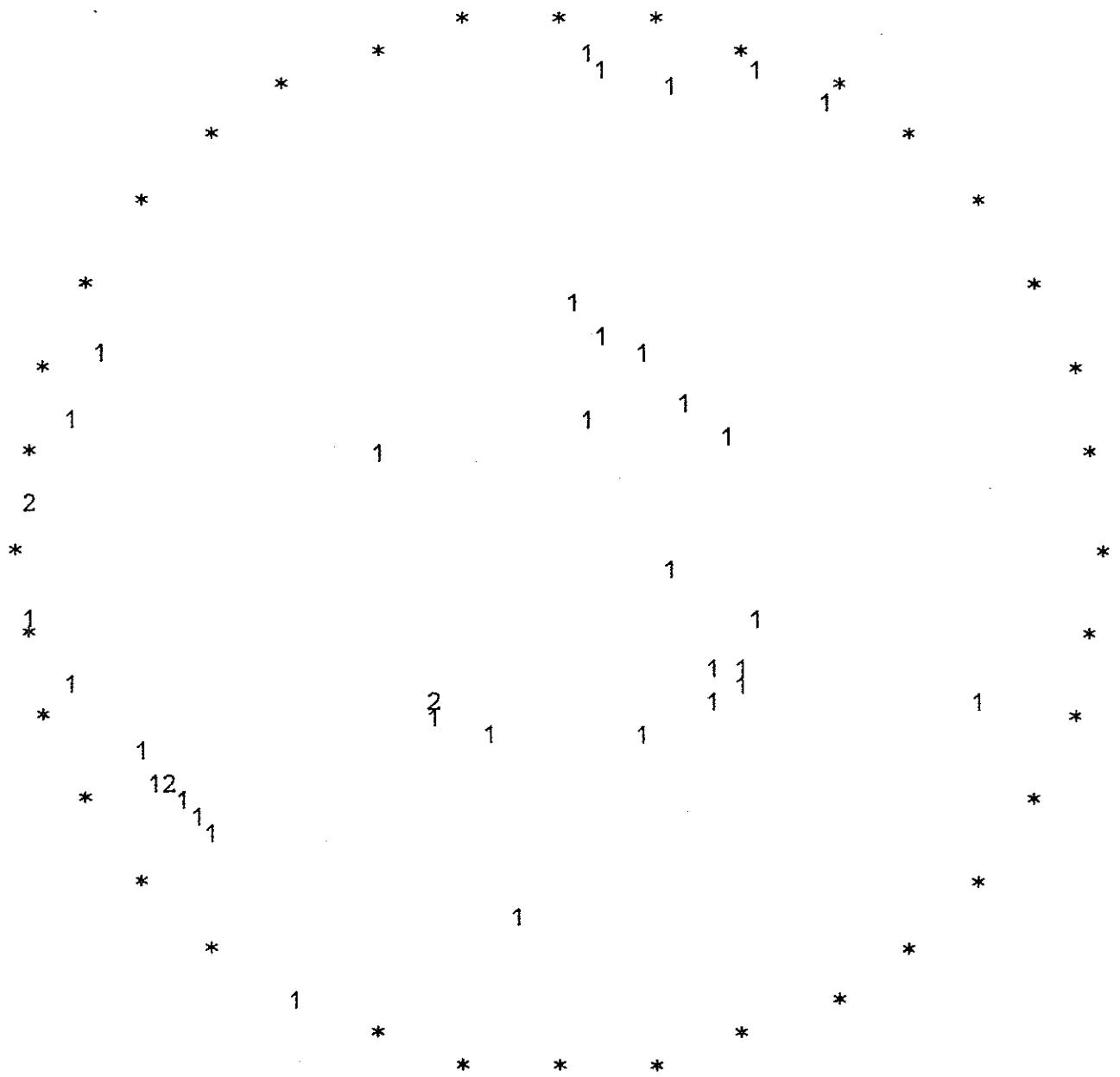
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 11

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	5%
'1+'	<LT>	10%
'2'	<LT>	15%
'3'	<LT>	20%
'M'	MAX =	45.5



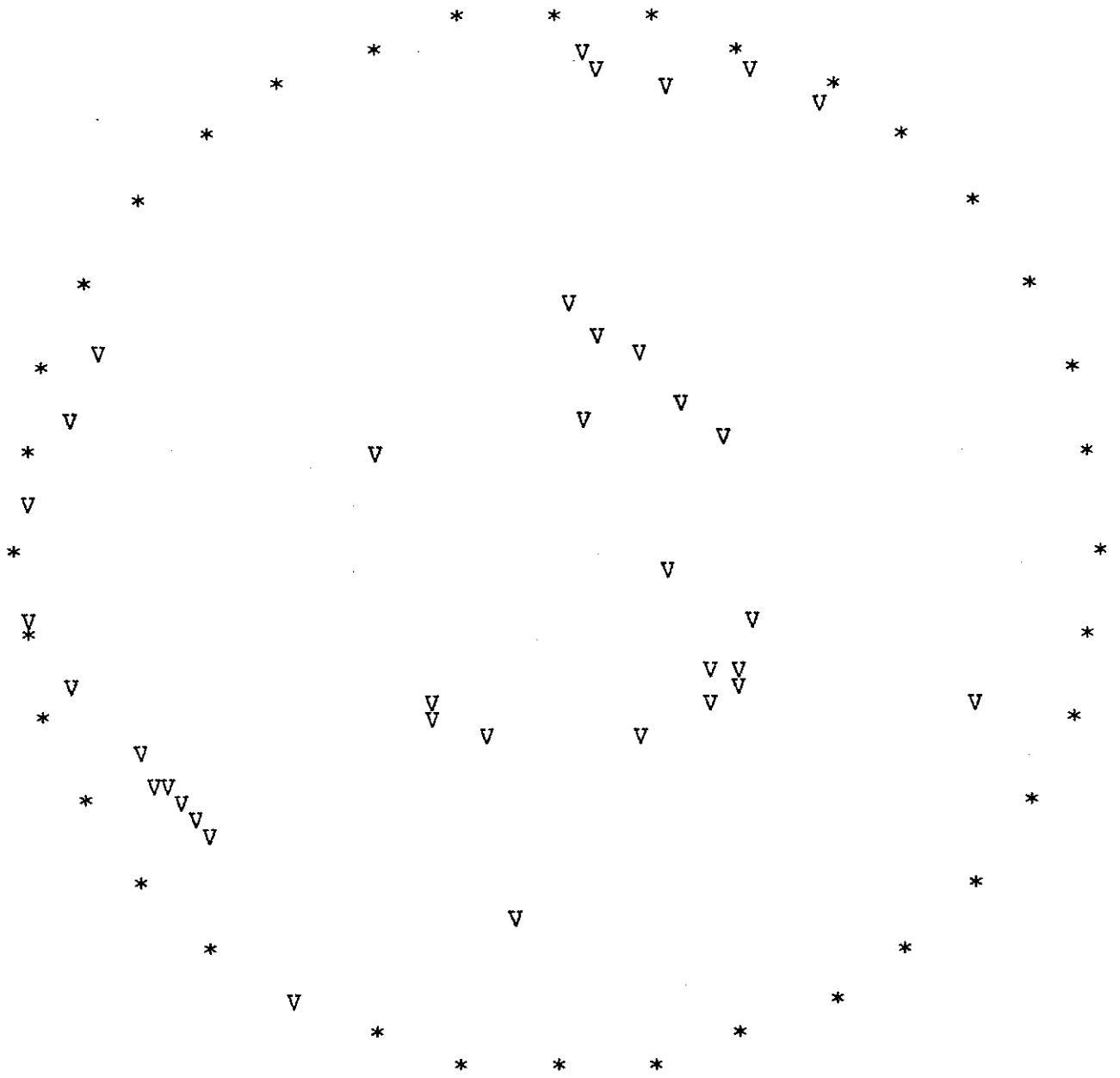
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 VEINS

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 39

ROTATION ANGLES: 0 0 0



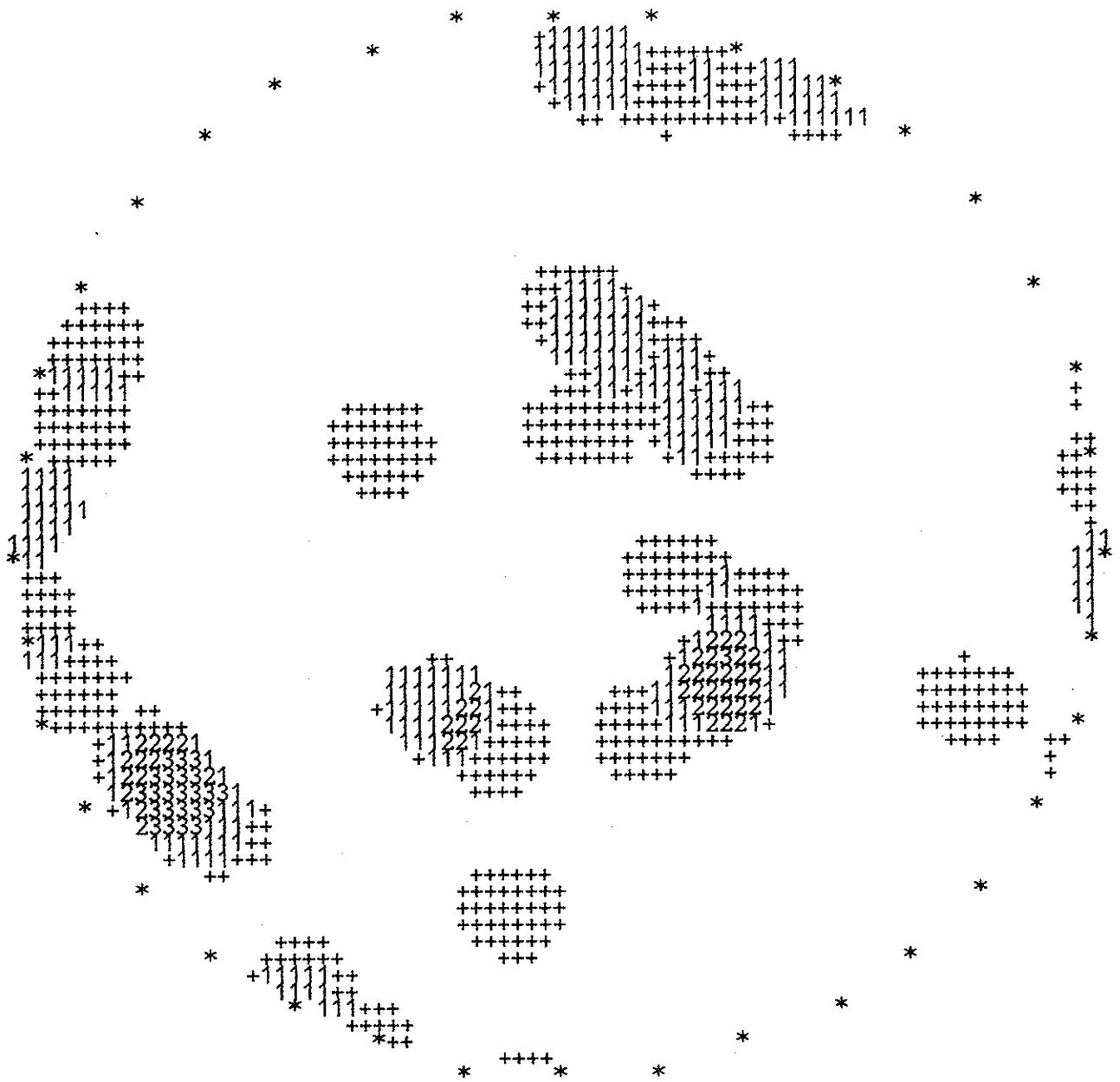
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 VEINS

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 39

ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 101 VEINS

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

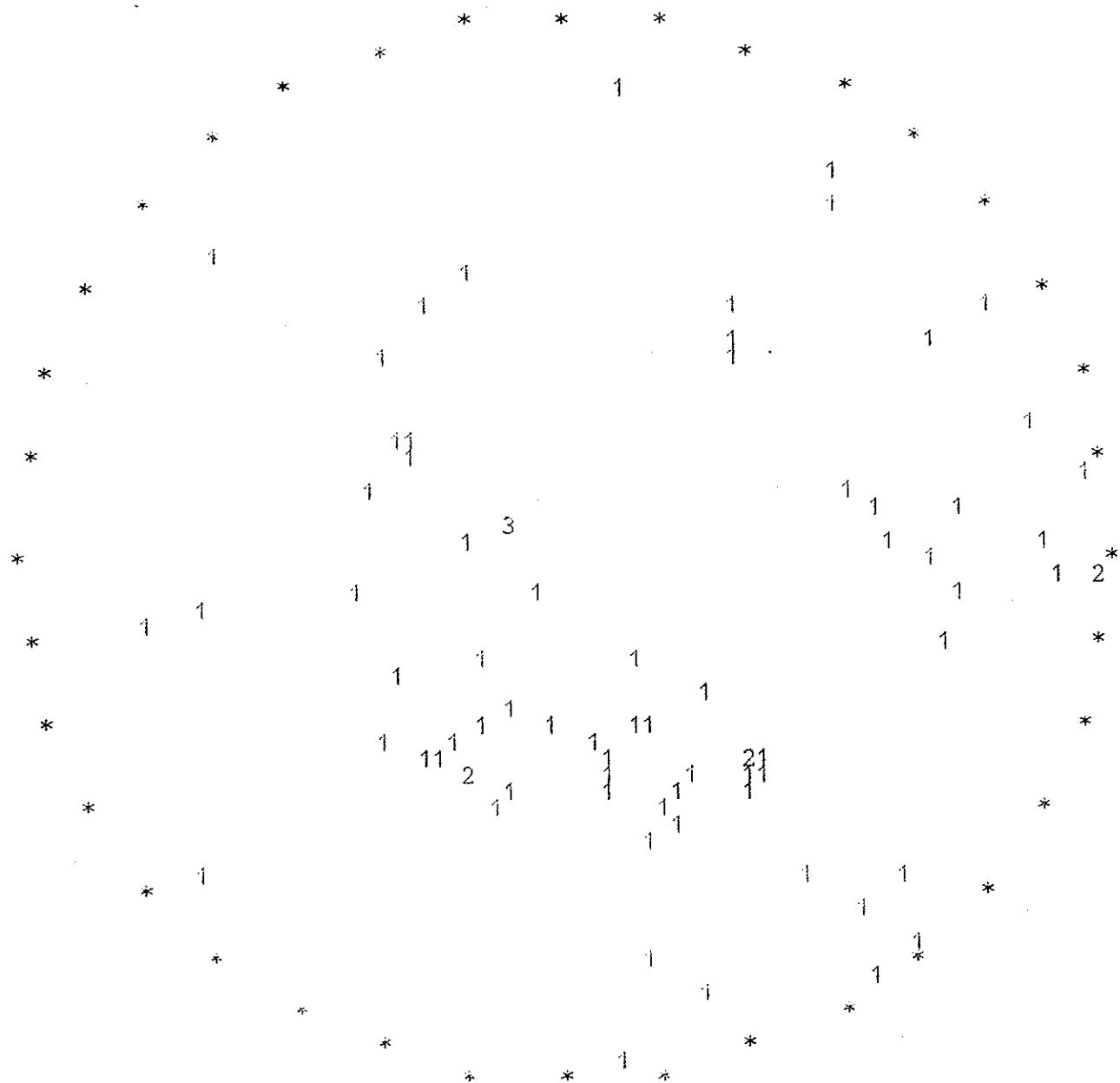
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 39

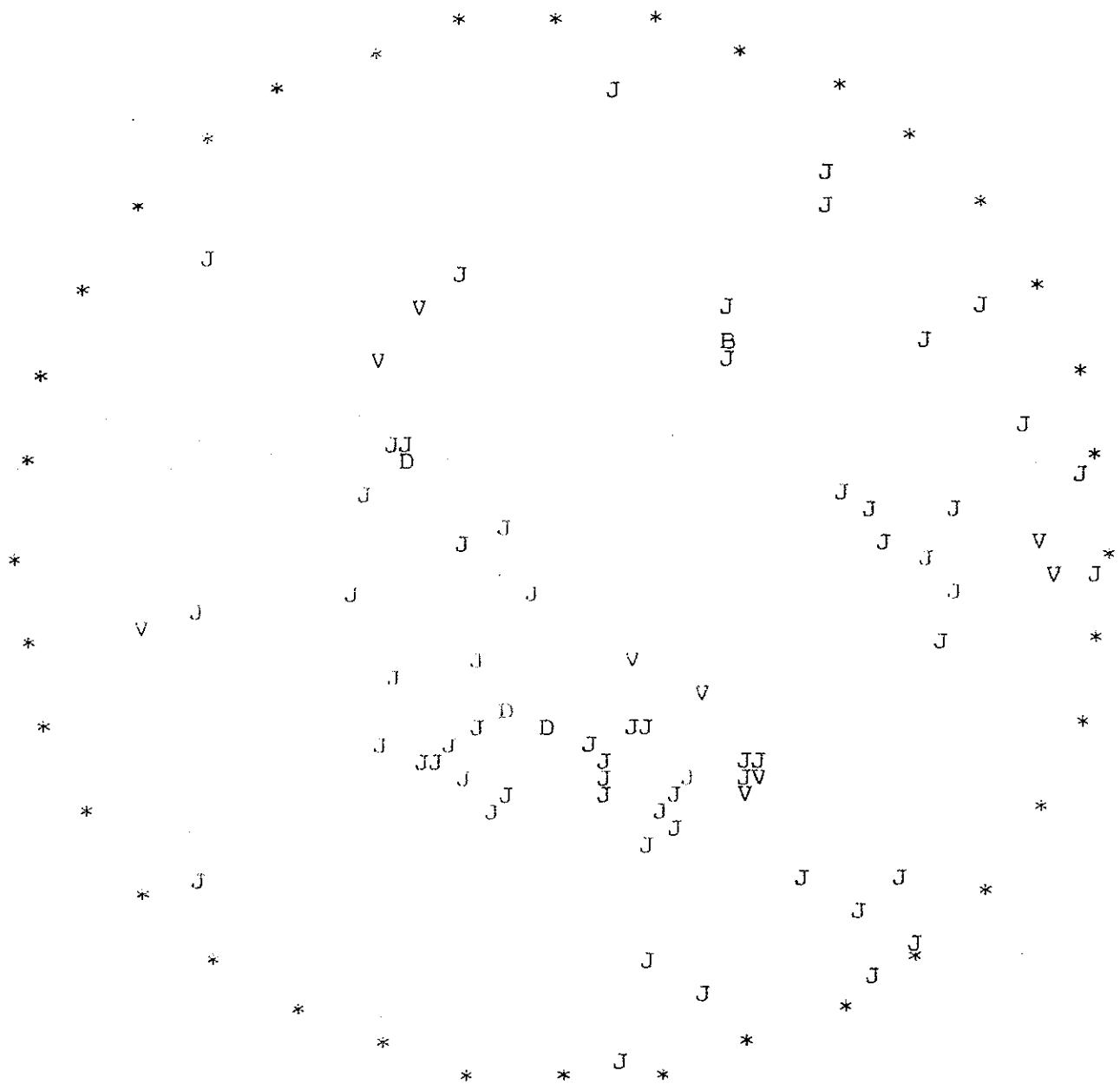
ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

' '	<LT>	1%
'+'	<LT>	4%
'1'	<LT>	8%
'2'	<LT>	12%
'3'	<LT>	16%
'M'	MAX	= 15.4



S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 78
ROTATION ANGLES: 0 0 0



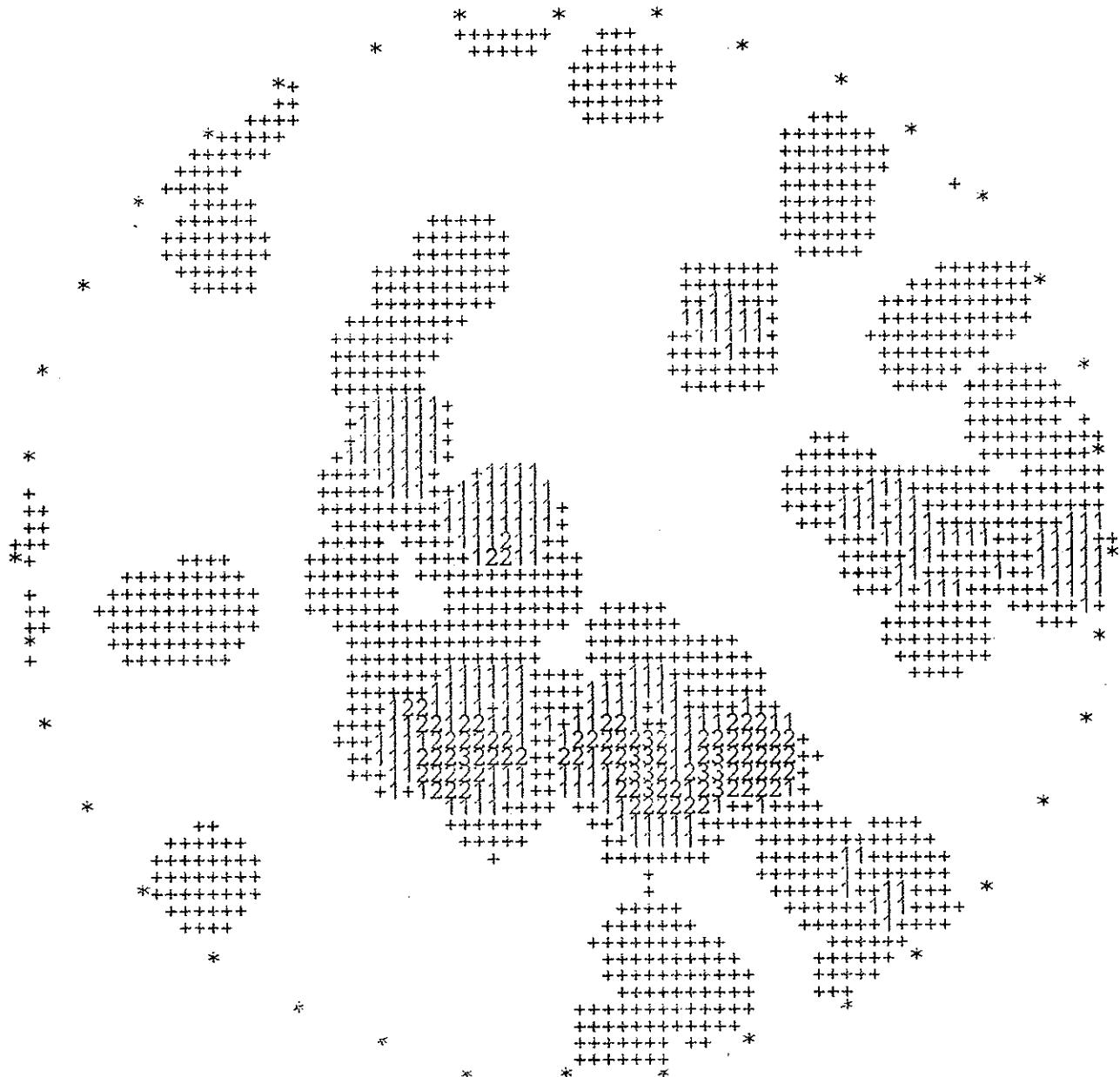
S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 78

ROTATION ANGLES: 0 0 0



S8463/4 HORNSEY SHIRE COUNCIL - BOREHOLE 102

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

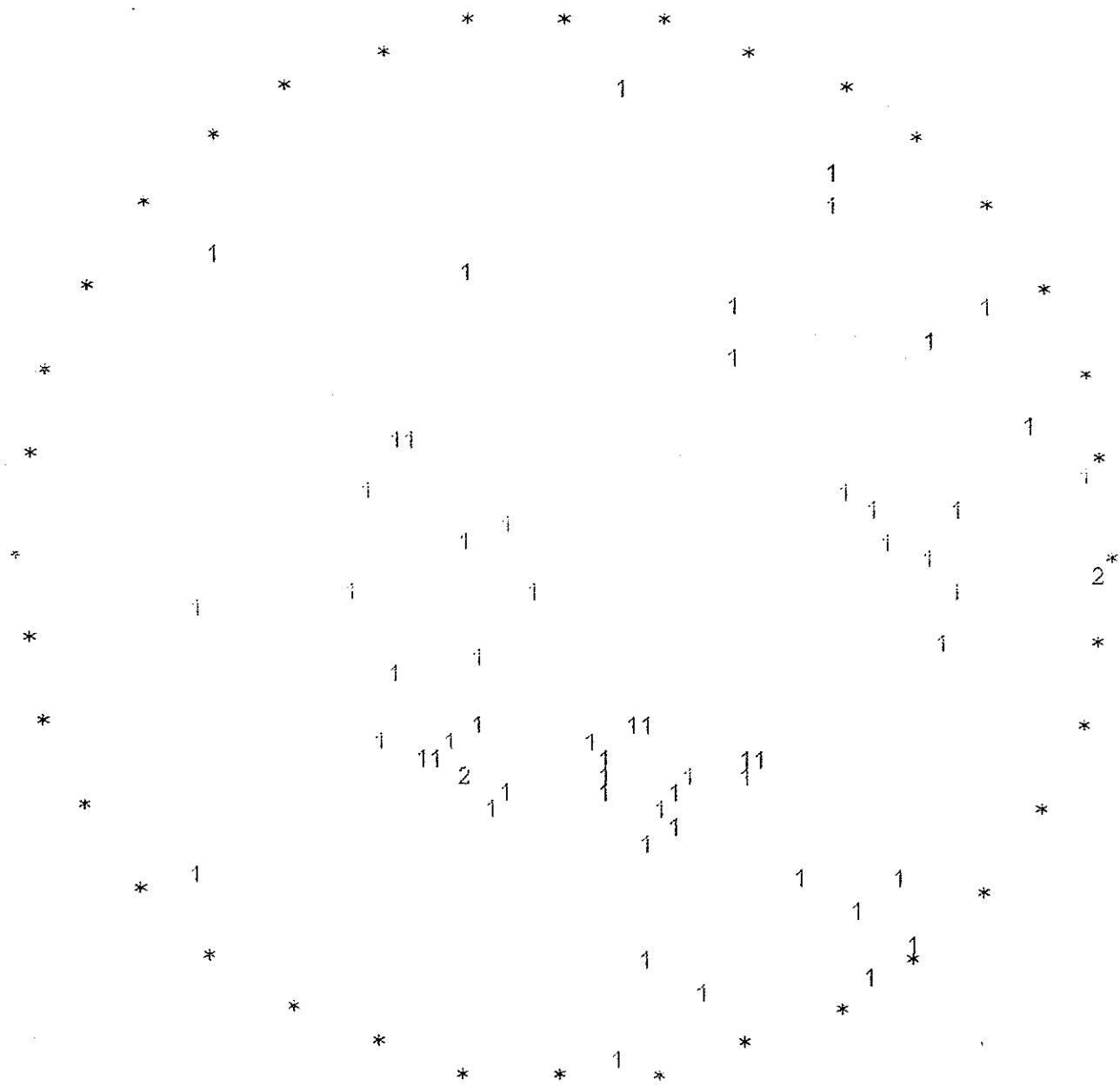
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 78

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	3%
'1'	<LT>	6%
'2'	<LT>	9%
'3'	<LT>	12%
'M'	MAX	= 11.5



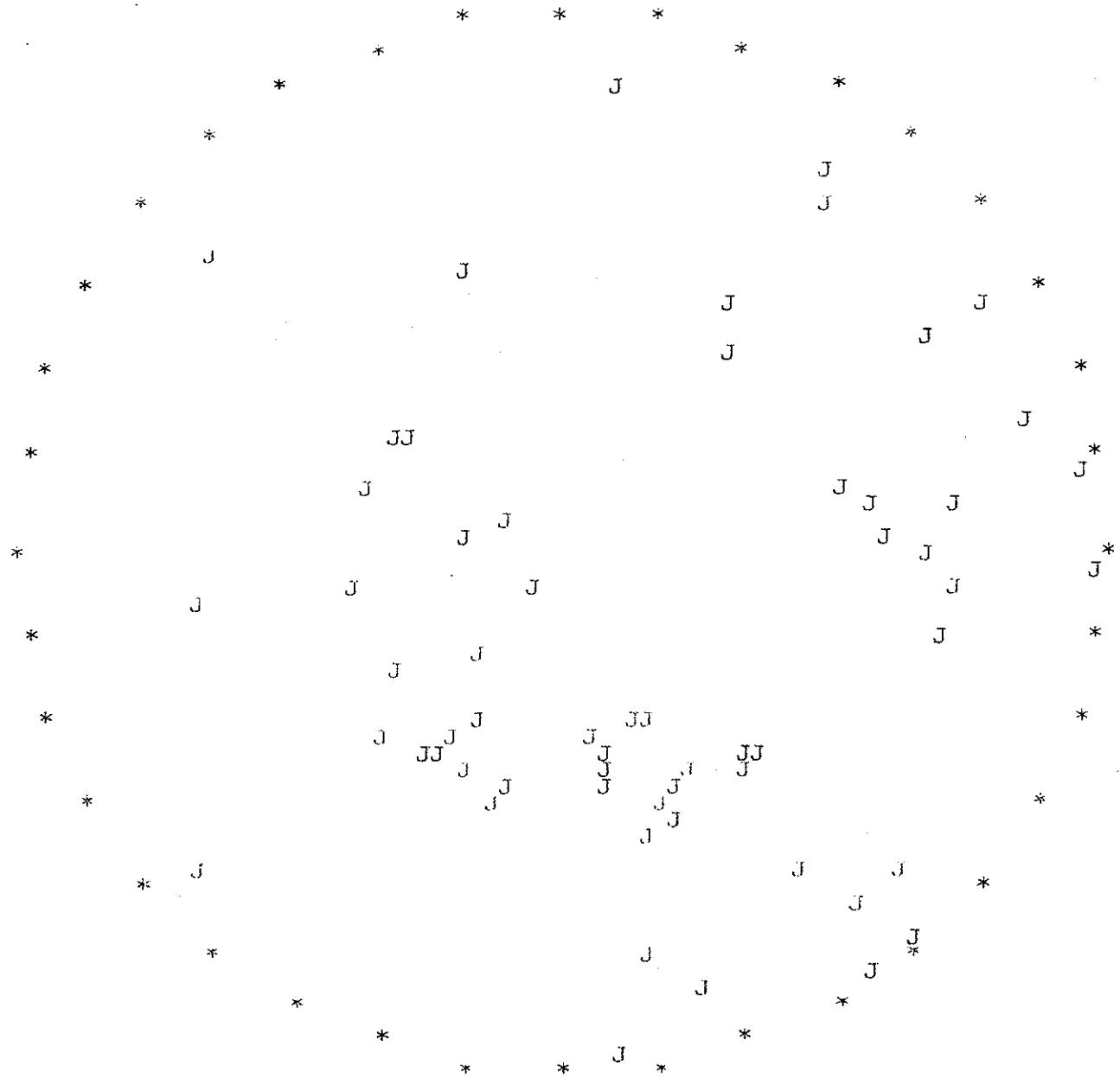
S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102 JOINTS

SCATTER DIAGRAM - POLES TO PLANES

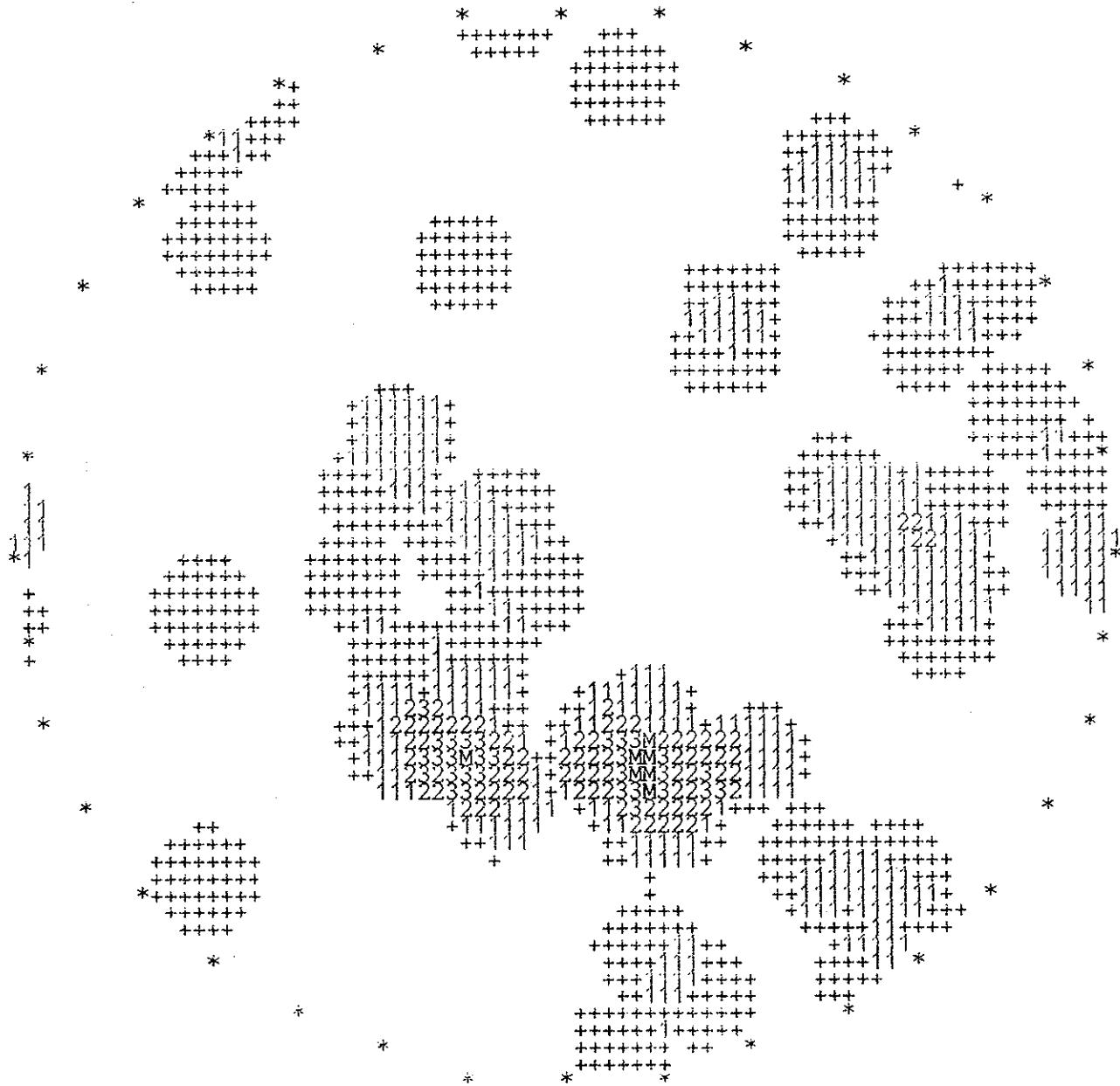
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 62

ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102 JOINTS
 SCATTER DIAGRAM - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 62
 ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 102 JOINTS
 SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 62
 ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	3%
'1'	<LT>	6%
'2'	<LT>	9%
'3'	<LT>	12%
'M'		MAX = 12.9

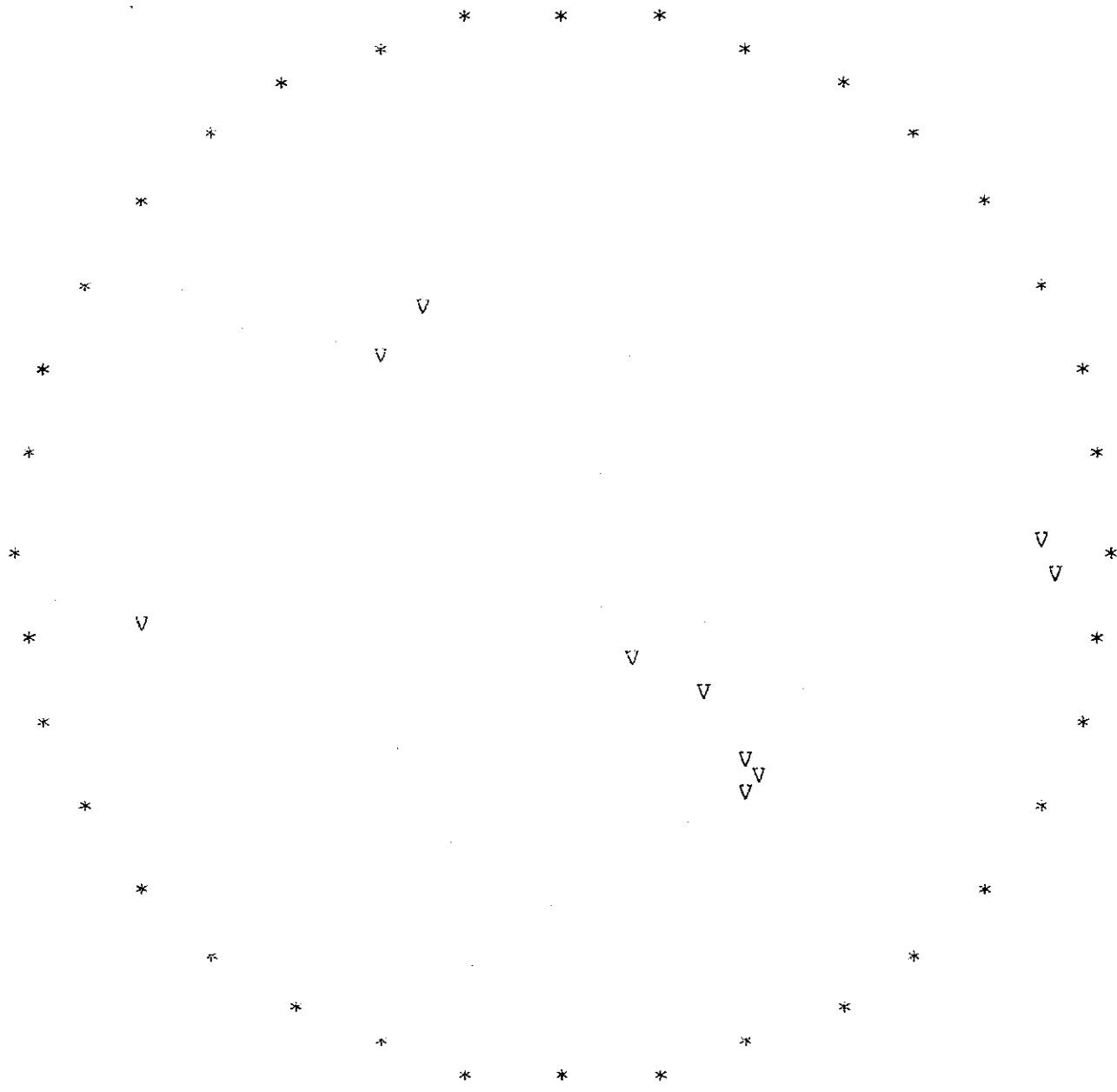
S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 5
ROTATION ANGLES: 0 0 0

S8463/4 HORNSBY SHIRE COUNCIL - BORROWHOLE 102 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 5
ROTATION ANGLES: 0 0 0

S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102 BEDDINGS
 SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 5
 ROTATION ANGLES: 0 0 0
 SHADING SYMBOLS

'	<LT>	1%
'+'	<LT>	5%
'1'	<LT>	10%
'2'	<LT>	15%
'3'	<LT>	20%
'M'	MAX	= 40.0

S8463/4 HORNSBY SHIRE COUNCIL -BOREHOLE 102 VEINS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 10
ROTATION ANGLES: 0 0 0



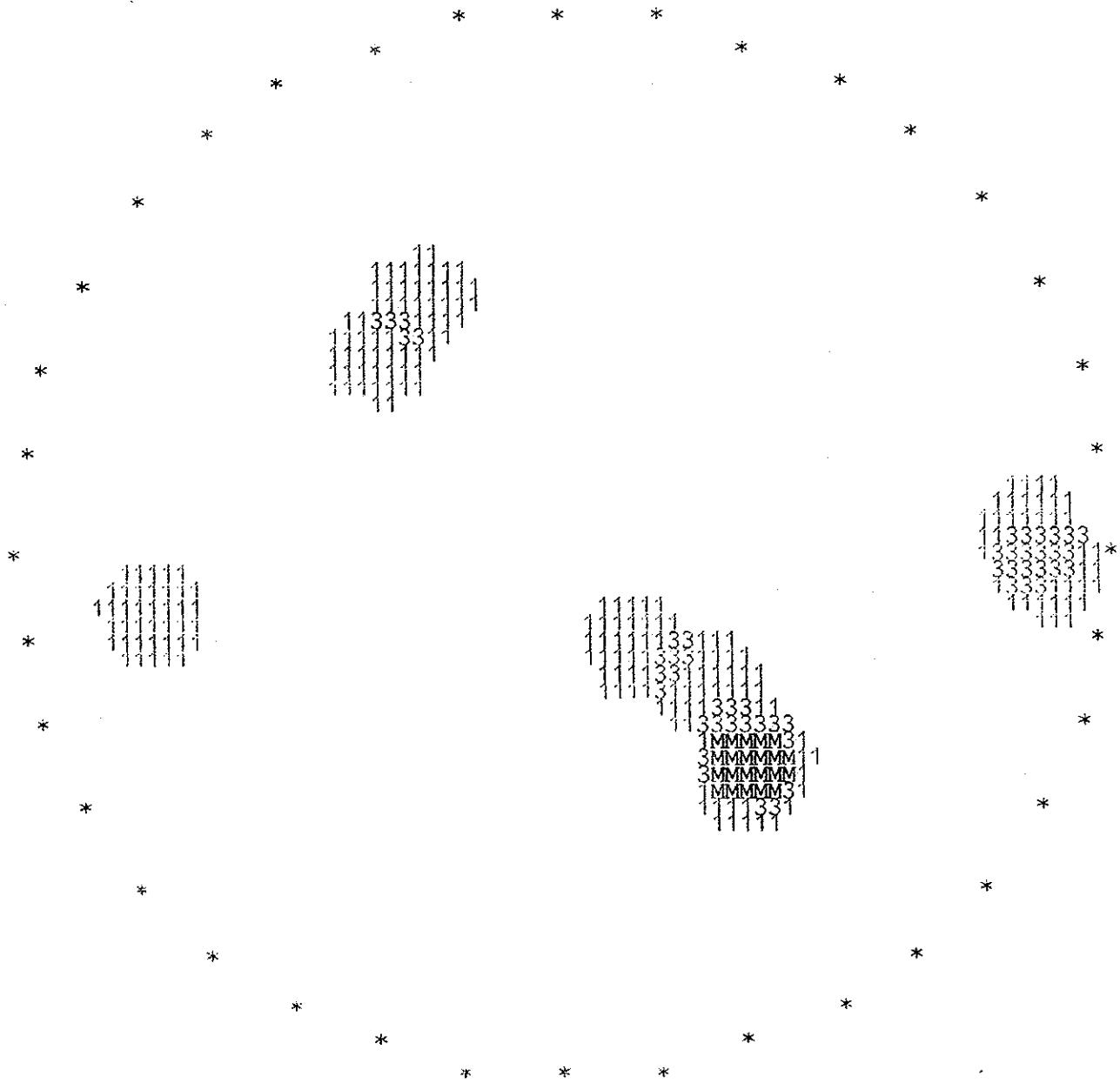
S8463/4 HORNSBY SHIRE COUNCIL - BOREHOLE 102 VEINS

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 10

ROTATION ANGLES: 0 0 0

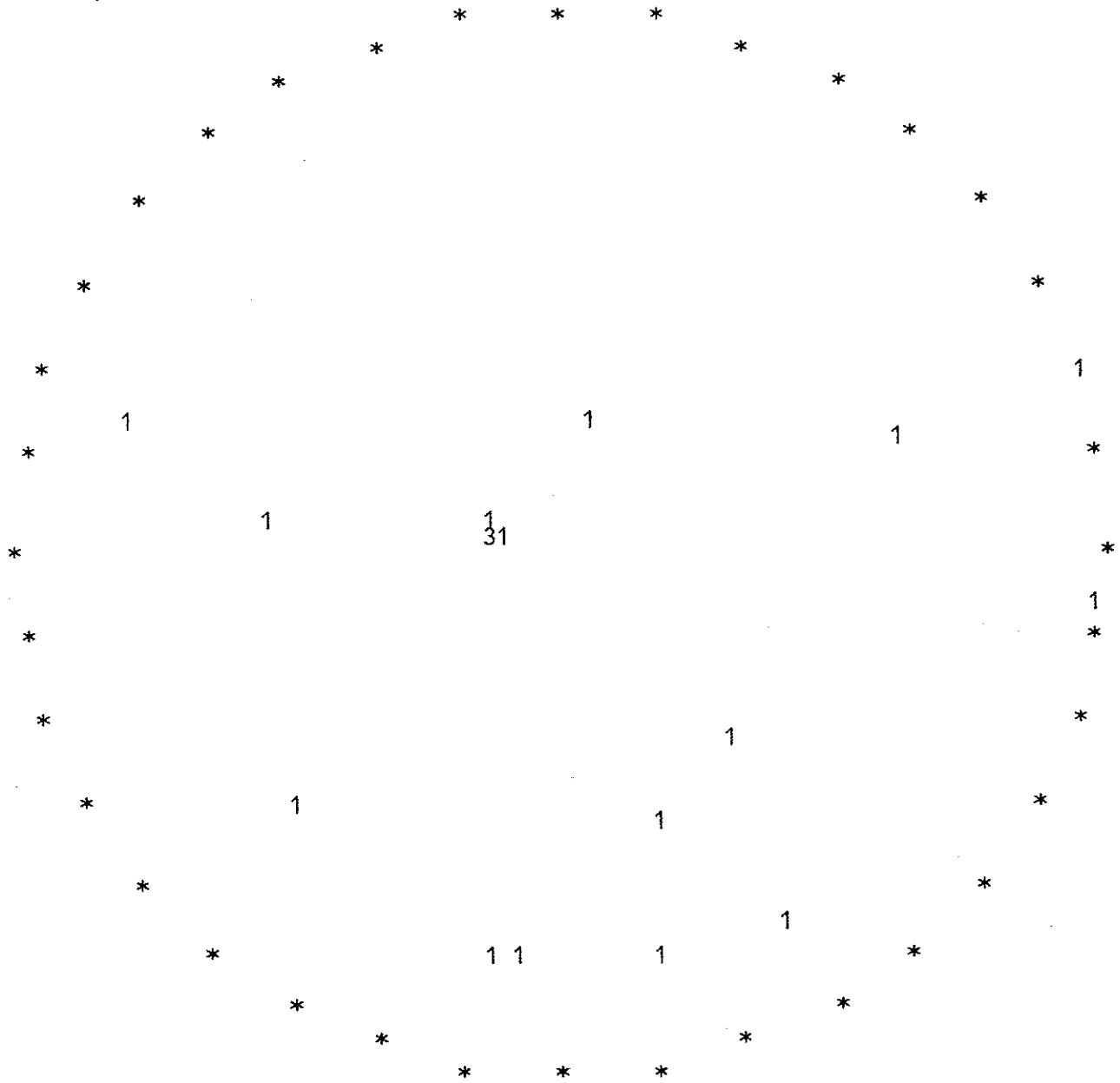


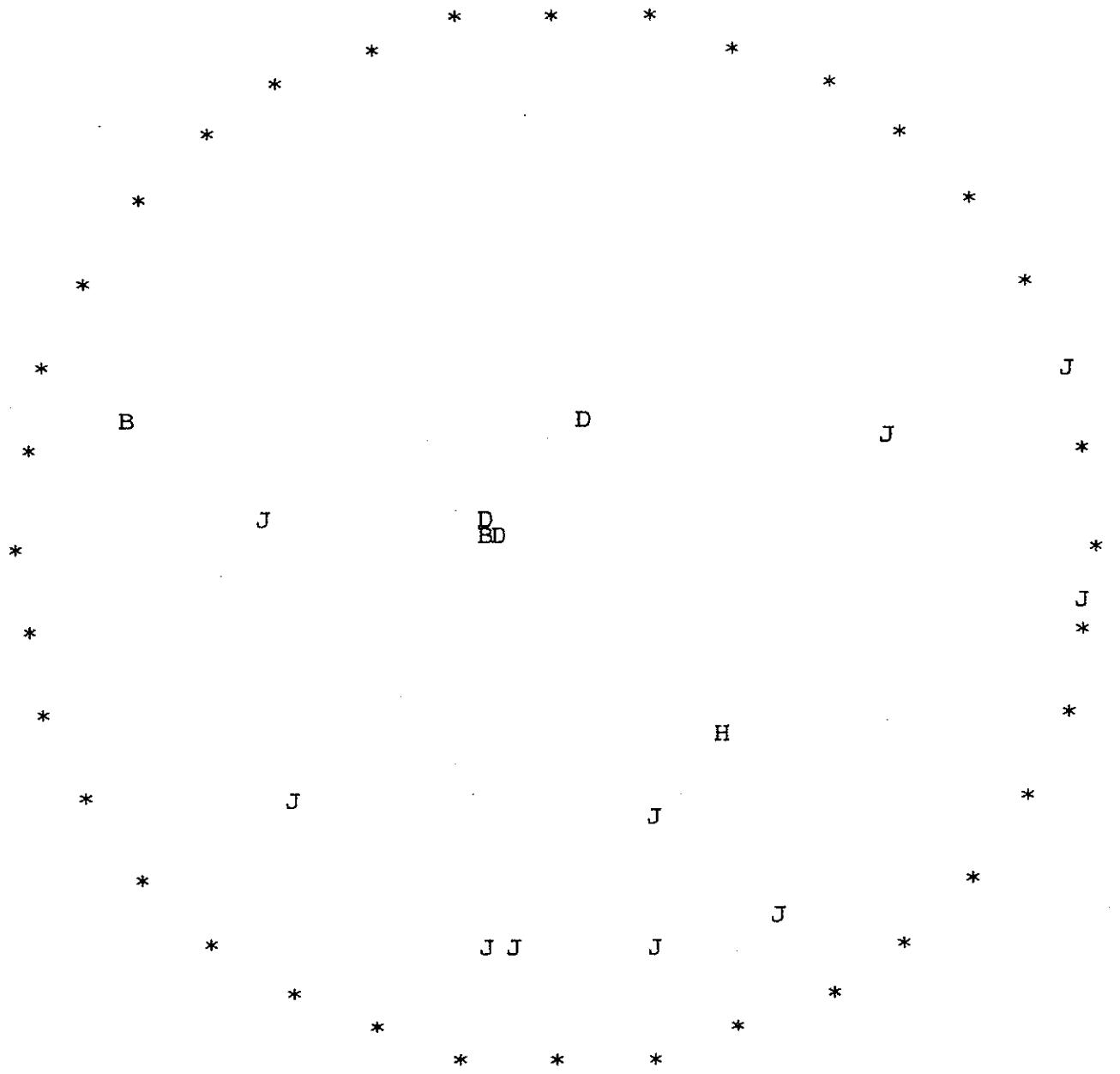
S8463/4 HORNSEY SHIRE COUNCIL -BOREHOLE 102 VEINS
 SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 10
 ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

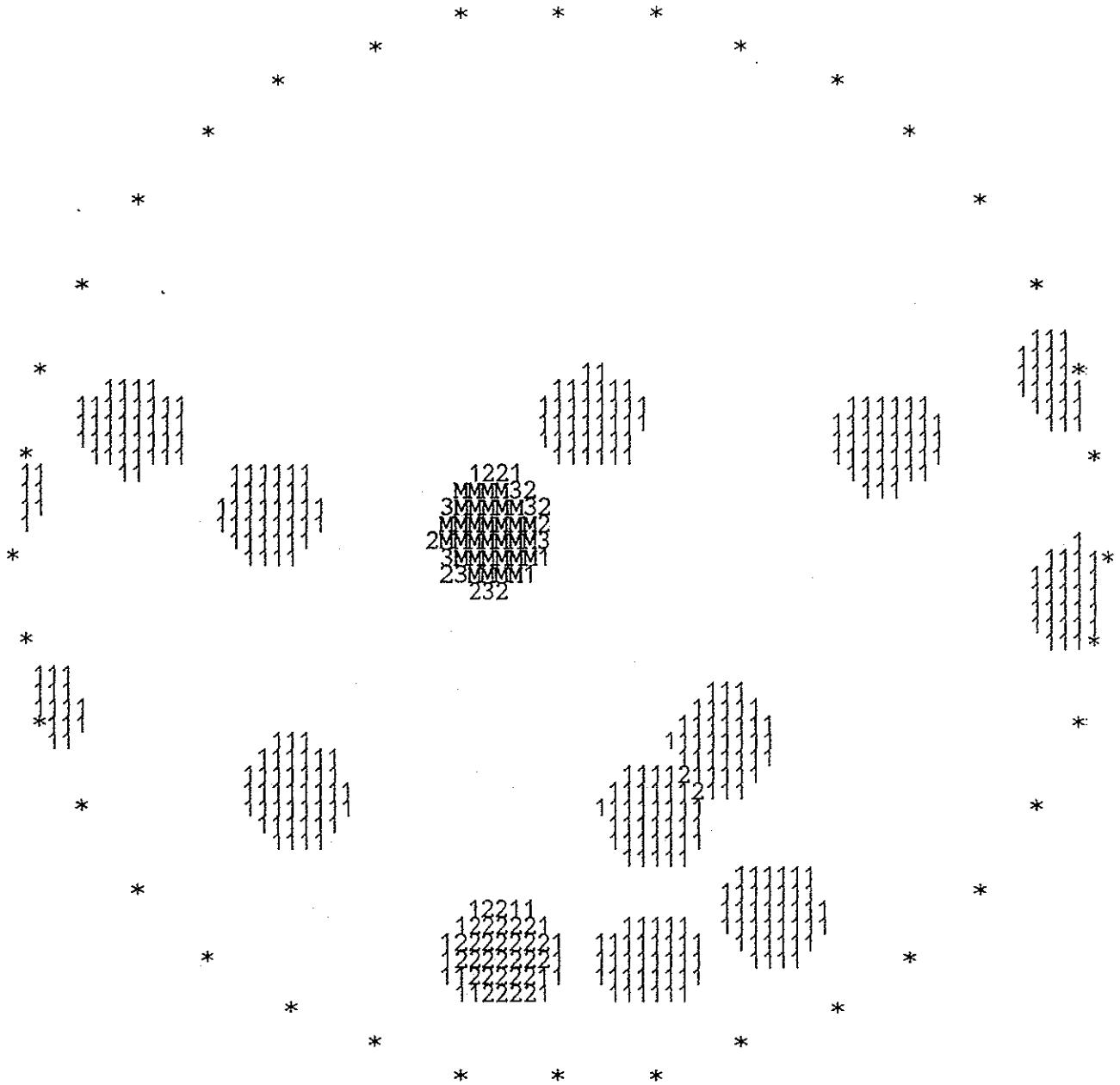
'1'	$\langle LT \rangle$	1%
'+'	$\langle LT \rangle$	5%
'1'	$\langle LT \rangle$	10%
'2'	$\langle LT \rangle$	15%
'3'	$\langle LT \rangle$	20%
'M'	MAX	= 30.0

S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 18
ROTATION ANGLES: 0 0 0





S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 18
ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 18

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	5%
'1'	<LT>	10%
'2'	<LT>	15%
'3'	<LT>	20%
'M'	MAX =	27.8

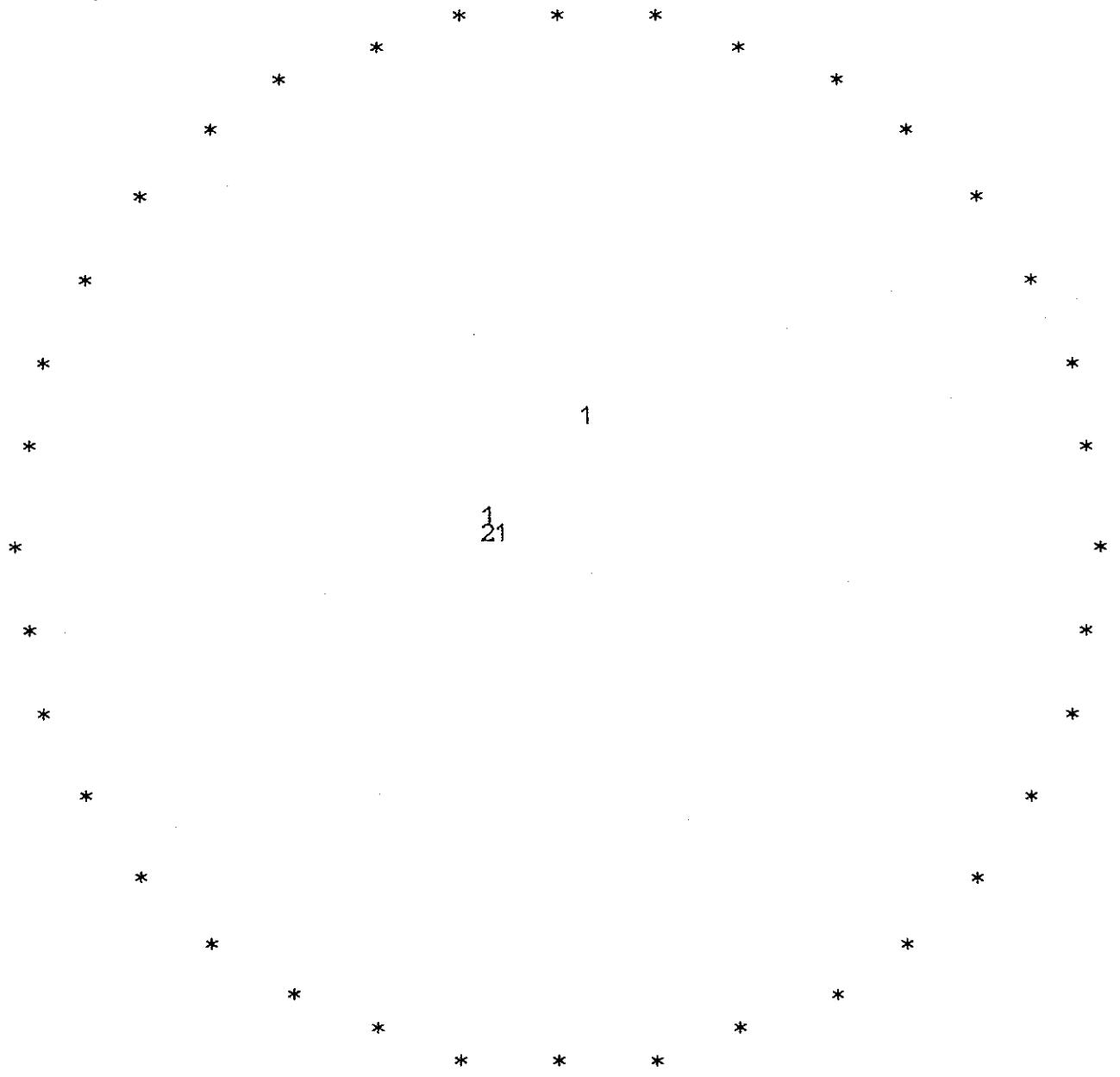
S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 JOINTS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 10
ROTATION ANGLES: 0 0 0

S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 JOINTS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 10
ROTATION ANGLES: 0 0 0

S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 JOINTS
 SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 10
 ROTATION ANGLES: 0 0 0

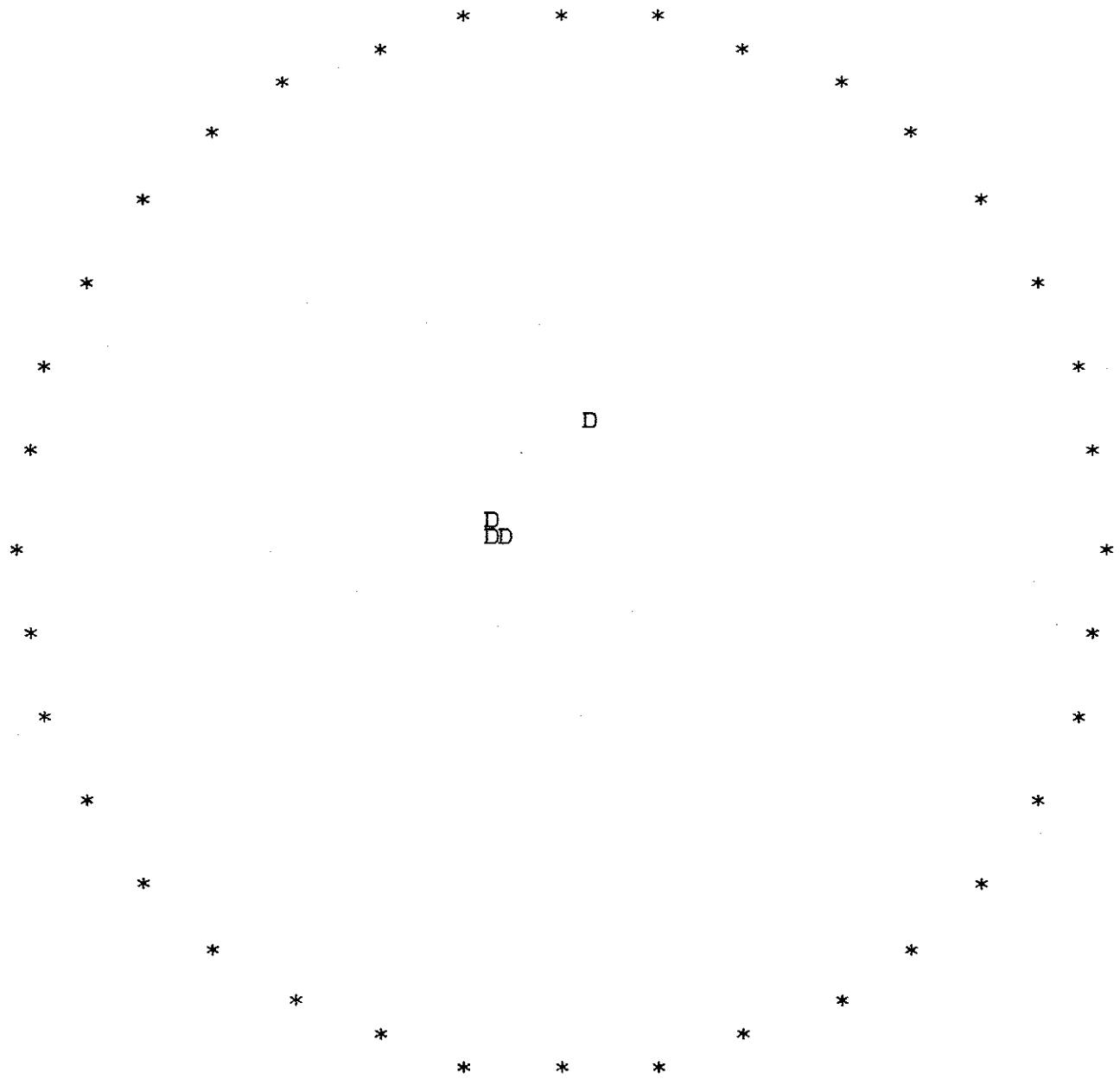
SHADING SYMBOLS

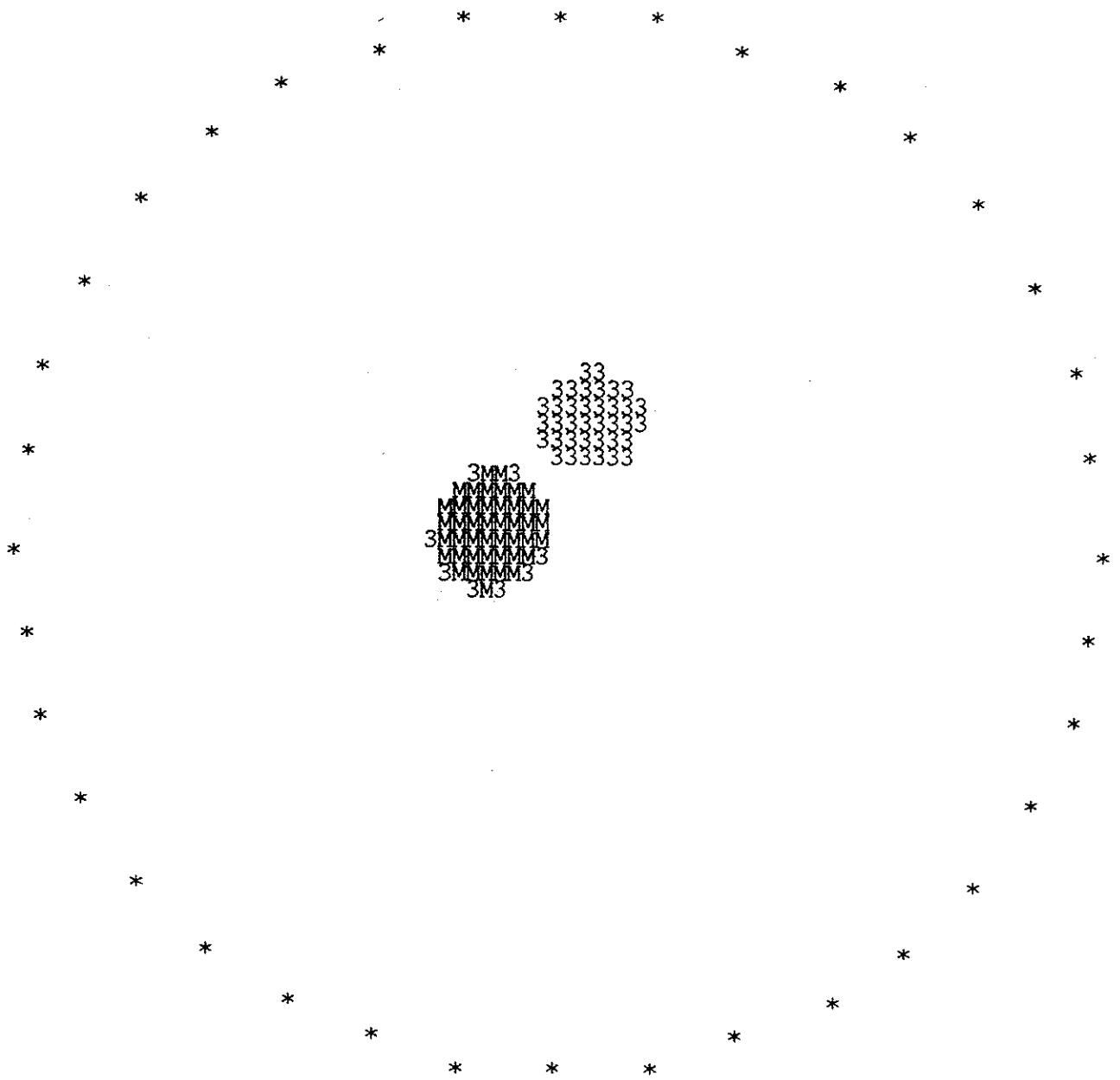
' 1	<LT>	1%
'+'	<LT>	4%
'1'	<LT>	8%
'2'	<LT>	12%
'3'	<LT>	16%
'M'	MAX =	20.0



S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 5
ROTATION ANGLES: 0 0 0

S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 BEDDINGS
SCATTER DIAGRAM - POLES TO PLANES
LOWER HEMISPHERE - EQUAL AREA PROJECTION
NO. OF MEASURED POLES: 5
ROTATION ANGLES: 0 0 0





S8463/4 HORNSBY SHIRE COUNCIL BOREHOLE 103 BEDDINGS

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 5

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

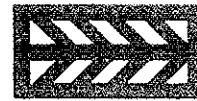
' '	<LT>	1%
'+'	<LT>	5%
'1'	<LT>	10%
'2'	<LT>	15%
'3'	<LT>	20%
'M'		MAX = 80.0



APPENDIX D

Coffey & Partners Pty. Ltd.

S8463/4-AD
3rd April, 1990



APPENDIX C

DATA HISTOGRAMS FOR SURFACE LINE MAPPING

geotechnical line mapping data histograms

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: UPPER BENCH OF EASTERN FACE

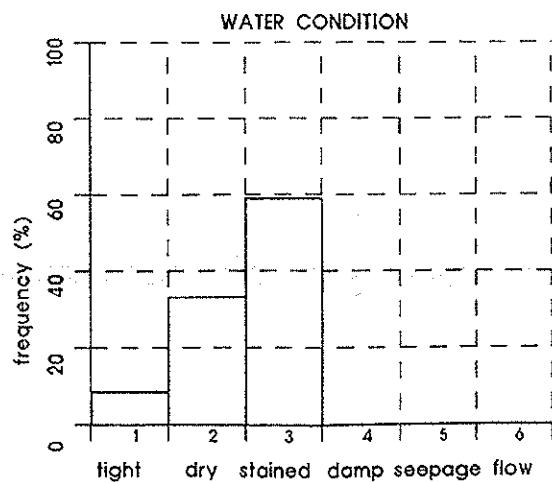
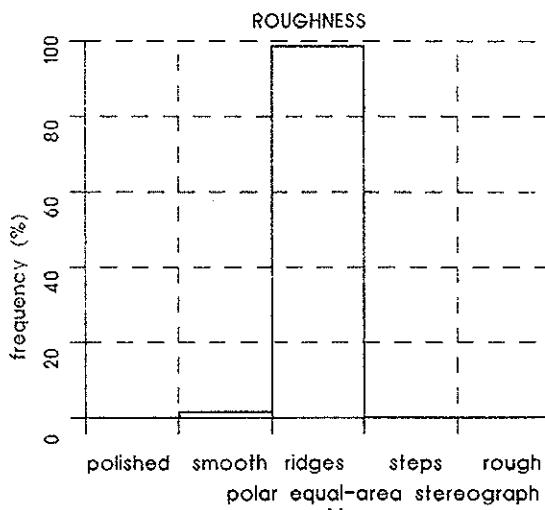
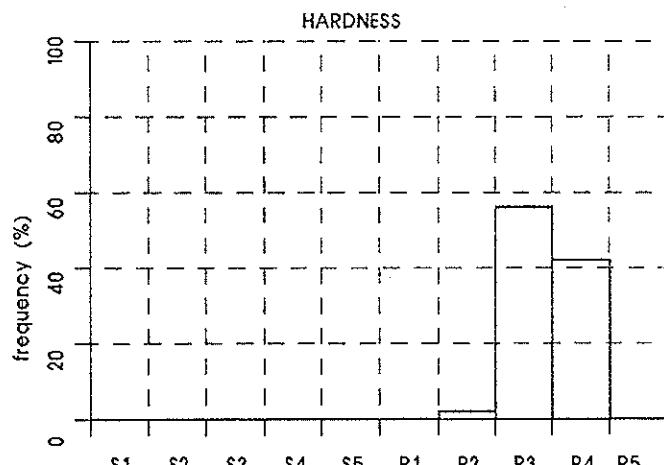
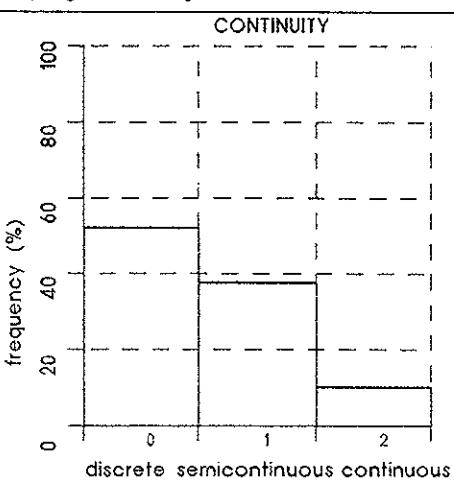
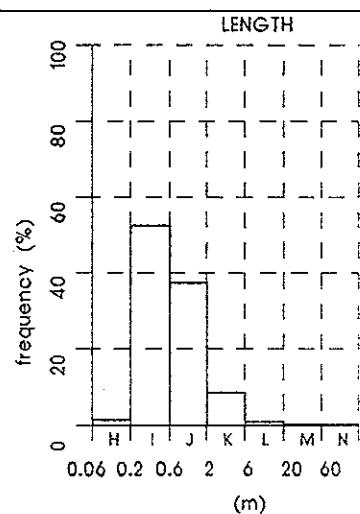
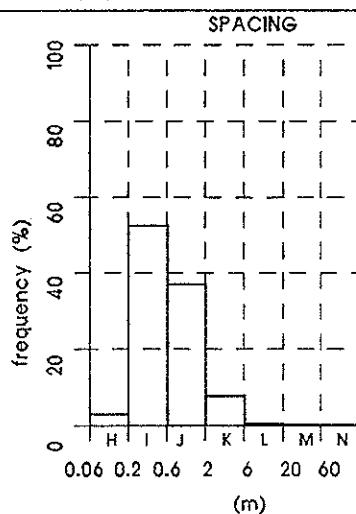
elevation: APPROX. RL. 90m

datum: AHD

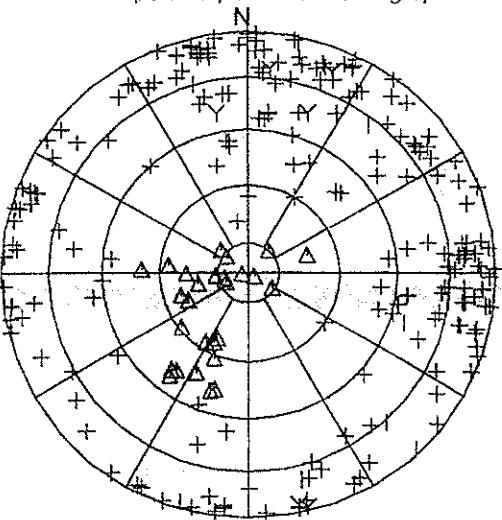
data selection

lithology type: all length: all hardness: all
discontinuity type: all continuity: all water: all

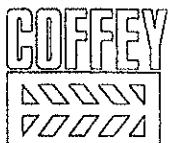
discontinuity orientation: all
trend: mean, range
plunge: mean, range



- +
- joint (JN)
- fault (FL)
- bedding (BG)
- shear (SR)
- unconformity (UC)
- boundary (BD)
- cleavage (CV)
- contact (CN)
- gneissosity (GS)
- schistosity (SC)
- vein (VN)
- other



geotechnical line mapping data histograms



line no:

1989/1

sheet 1 of 1

office job no: S8463/4

date: 08-11-89

logged by: SRM

checked by: PLV

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: UPPER BENCH OF EASTERN FACE

elevation: APPROX. RL. 90M

datum: A.H.D.

data selection

203 defects selected from a total of 252

discontinuity orientation: all

Lithology type: all

length

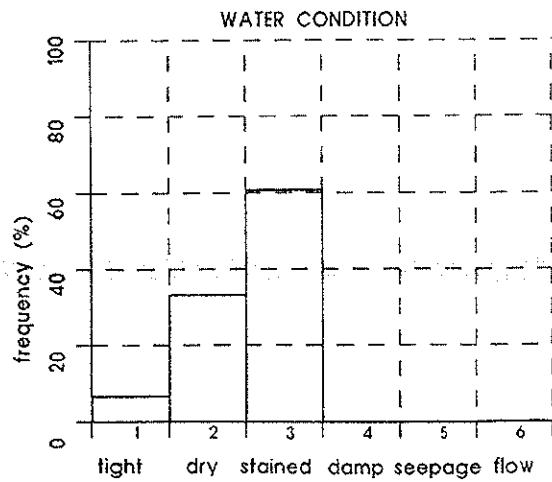
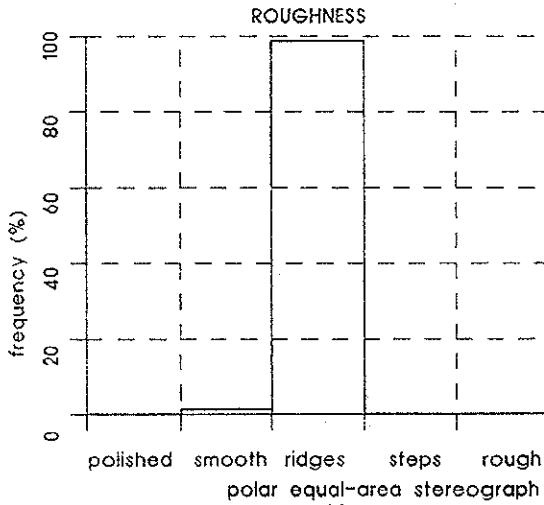
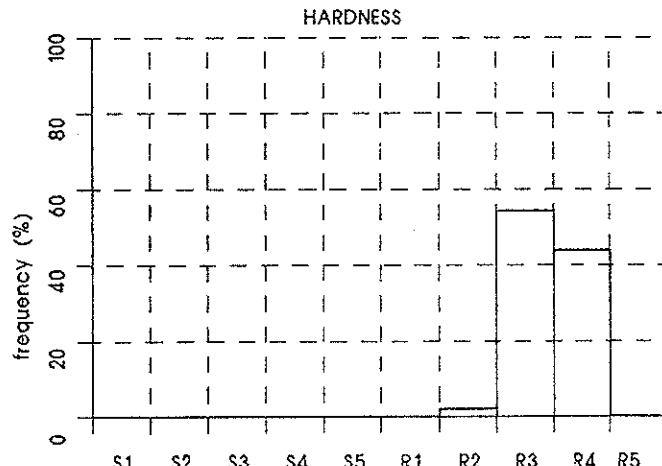
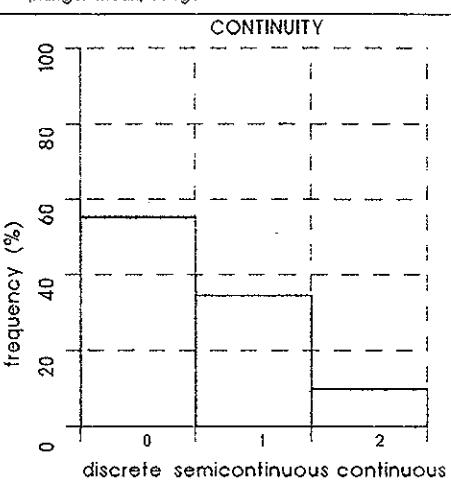
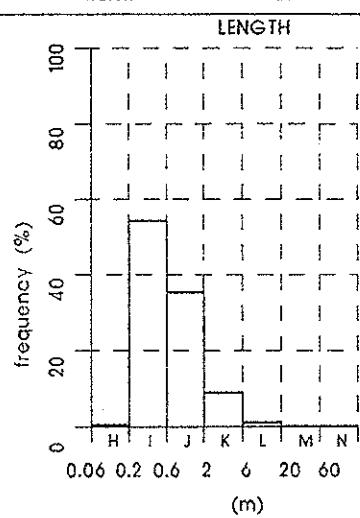
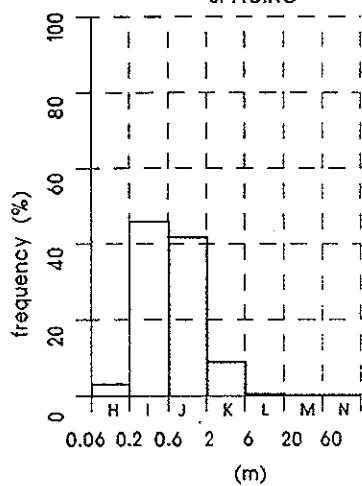
hard

all

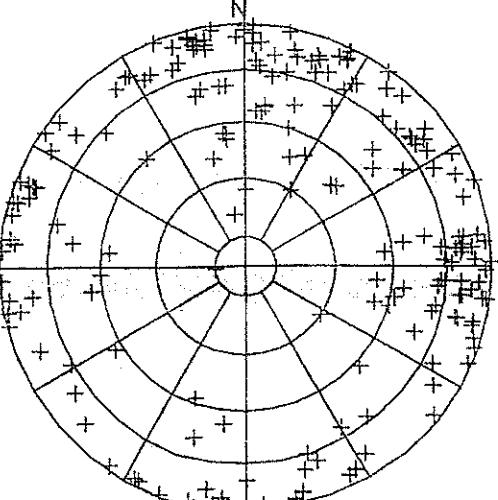
trend: mean, range

二

SPACING

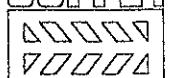


- + joint (JN)
 - X fault (FL)
 - △ bedding (BG)
 - shear (SR)
 - ☒ unconformity (UC)
 - boundary (BD)
 - ◊ cleavage (CV)
 - ↑ contact (CN)
 - X gneissosity (GS)
 - Y schistosity (SC)
 - V vein (VN)
 - | other



geotechnical line mapping data histograms

COFFEY



line no:

1989/1

sheet 1 of 1

office job no: S8463/4

date: 08-11-89

logged by: SRM

checked by: PLV

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: UPPER BENCH OF EASTERN FACE

elevation: APPROX. RL 90M

datum: A.H.D.

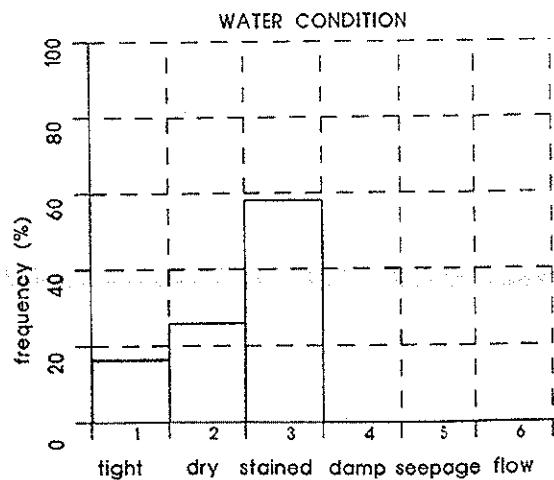
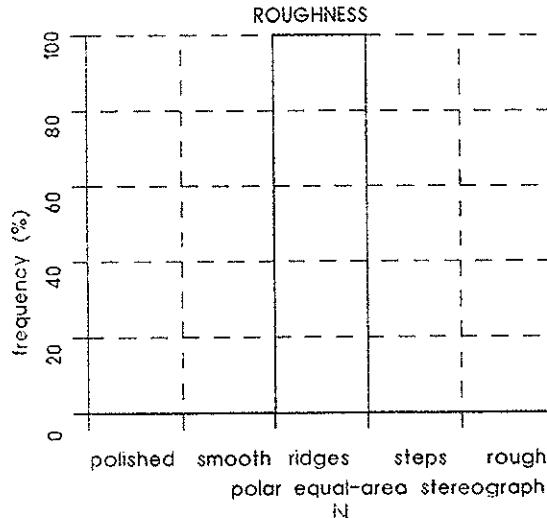
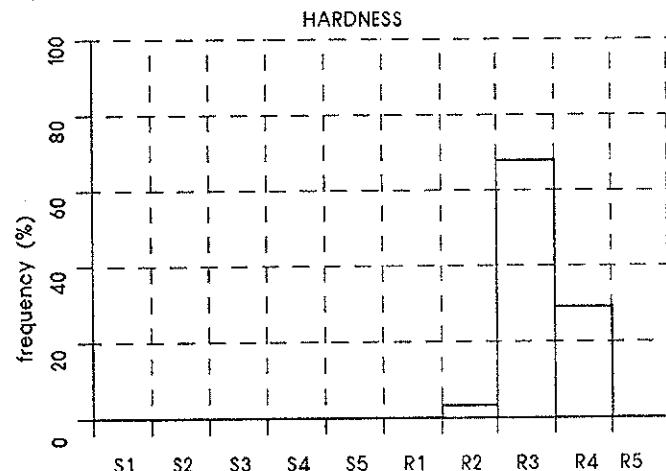
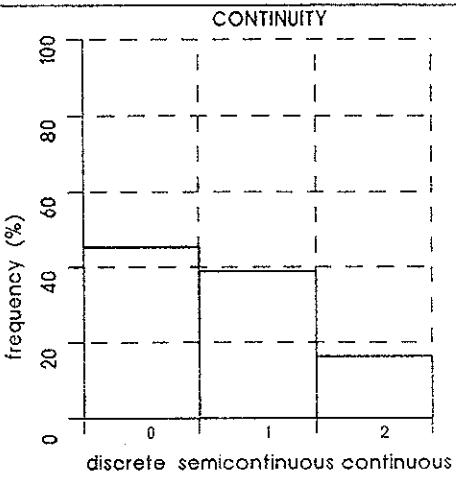
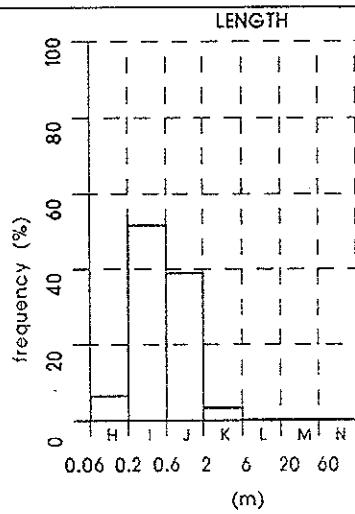
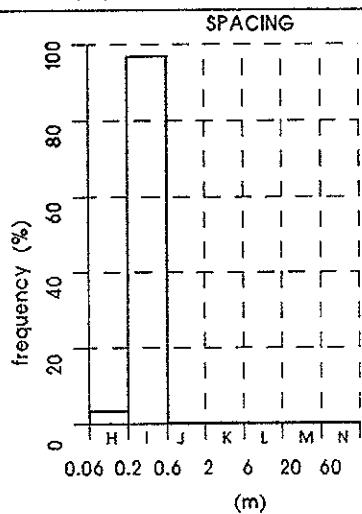
data selection

lithology type: all
discontinuity type: BG

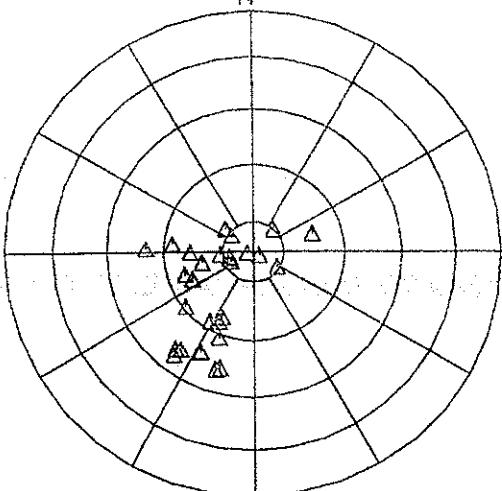
31 defects selected from a total of 252

length: all hardness: off
continuity: all water: off

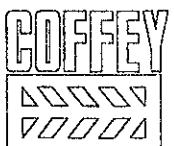
discontinuity orientation: all
trend: mean, range
plunge: mean, range



- + joint (JN)
- fault (FL)
- bedding (BG)
- △ shear (SR)
- ◊ unconformity (UC)
- × boundary (BD)
- ◆ cleavage (CV)
- ▽ contact (CN)
- ▲ gneissosity (GS)
- schistosity (SC)
- ◆ vein (VN)
- other



geotechnical line mapping data histograms



line no.

1989/1

sheet 1 of 1

office job no: S8463/4

date: 08-11-89

logged by: SRM

checked by: PLV

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

Identification: UPPER BENCH OF EASTERN FACE

elevation: APPROX. RL. 90M

Datum: 8. HD.

data selection

lithology type: all

31 defects selected from a total of 252

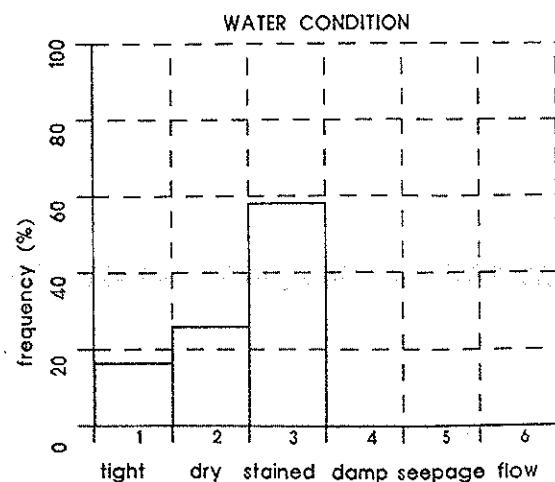
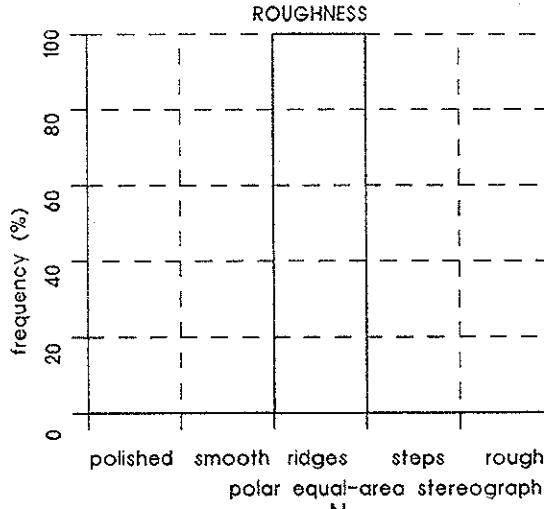
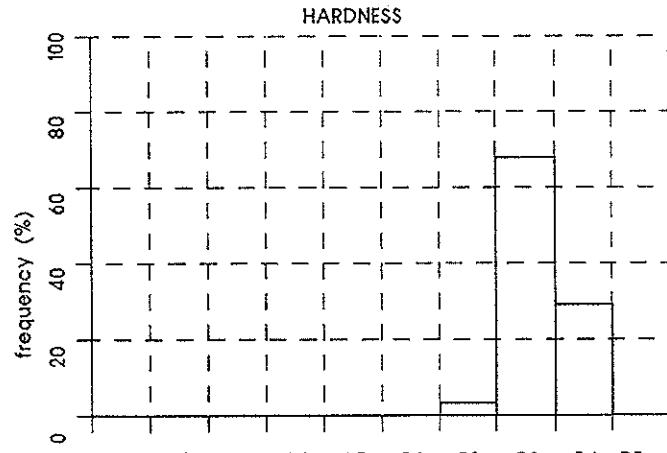
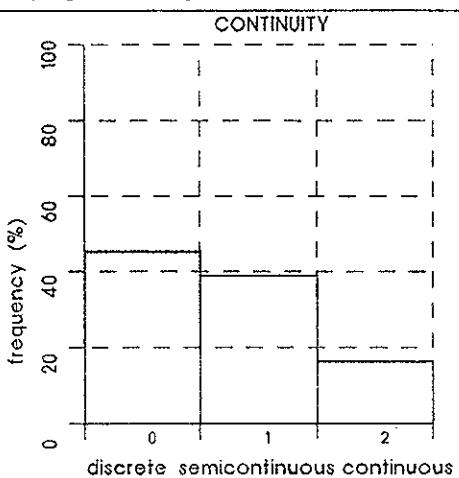
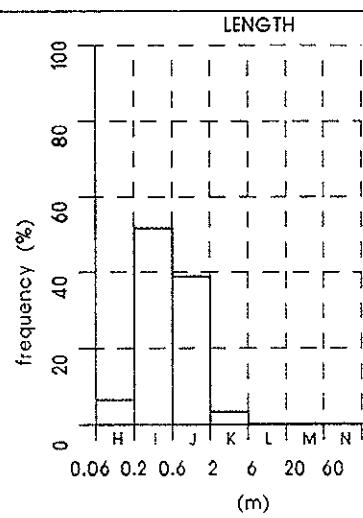
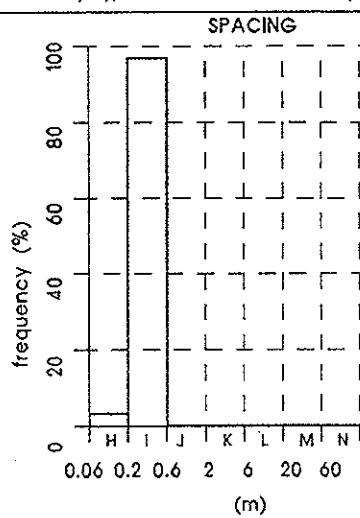
length:

hardness;

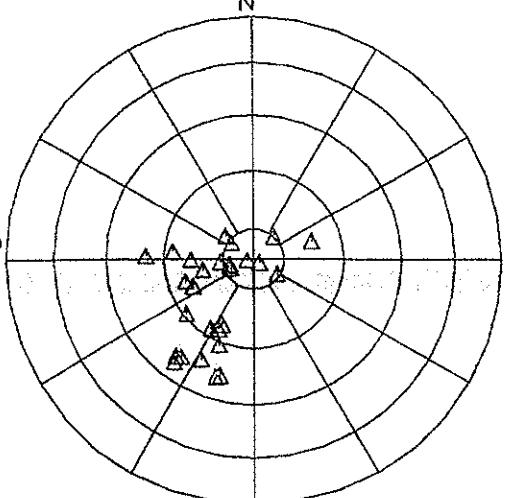
ardness; all

discontinuity orientation:

alt



- + joint (JN)
 - X fault (FL)
 - △ bedding (BG)
 - shear (SR)
 - ✗ unconformity (UC)
 - boundary (BD)
 - ◊ cleavage (CV)
 - ↑ contact (CN)
 - ✗ gneissosity (GS)
 - N schistosity (SC)
 - Y vein (VN)
 - | other



geotechnical line mapping data histograms



line no:
1989/2
sheet 1 of 1
office job no: S8463/4
date: 20-12-89
logged by: SRM
checked by: PLV

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: SECOND BENCH OF EASTERN FACE

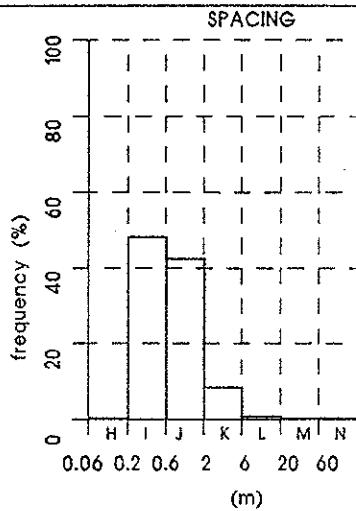
elevation: APPROX. RL. 70M

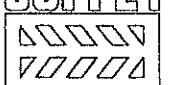
datum: A.H.D.

data selection

lithology type: all length: all hardness: all
discontinuity type: all continuity: all water: all

discontinuity orientation: all
trend: mean, range
plunge: mean, range





geotechnical line mapping data histograms

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: SECOND BENCH OF EASTERN FACE

elevation: APPROX. RL. 70M

datum: A.H.D.

data selection

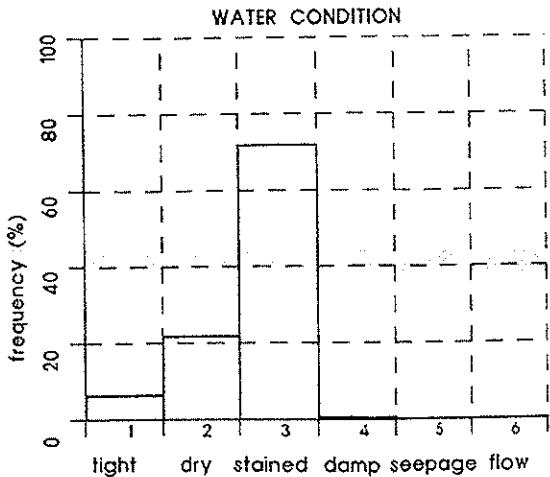
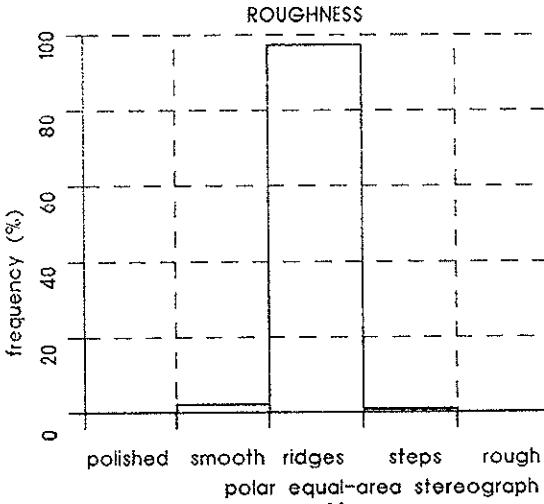
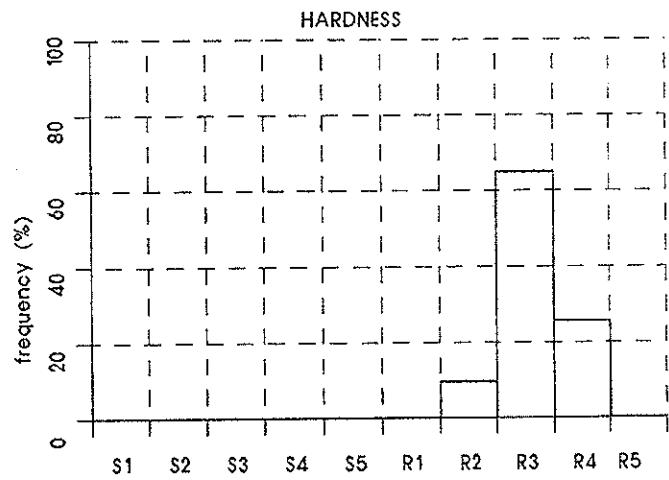
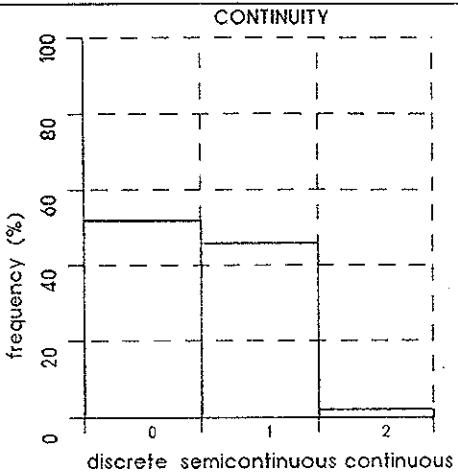
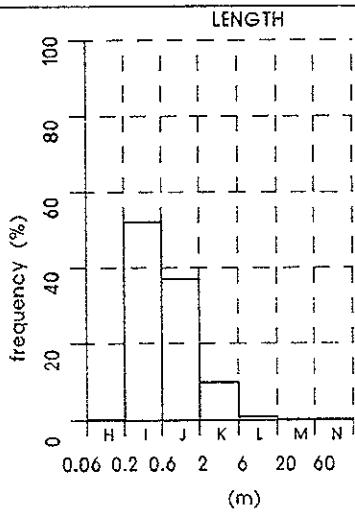
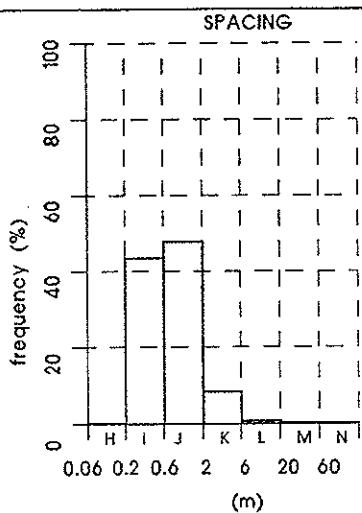
lithology type: all
discontinuity type: JN

367 defects selected from a total of 429

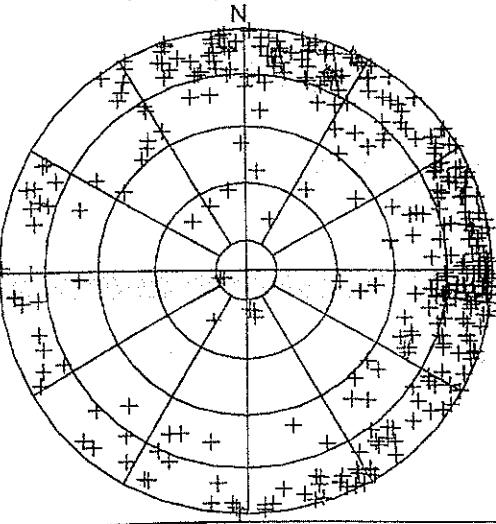
length: all
continuity: all
hardness: all
water: all

discontinuity orientation: all

trend: mean, range
plunge: mean, range



- + joint (JN)
- X fault (FL)
- △ bedding (BG)
- ◊ shear (SR)
- ◆ unconformity (UC)
- ▽ boundary (BD)
- ◆ cleavage (CV)
- × contact (CN)
- gneissosity (GS)
- schistosity (SC)
- ◆ vein (VN)
- other



geotechnical line mapping data histograms

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse fine data

identification: SECOND BENCH OF EASTERN FACE

elevation: APPROX. RL. 70M

datum: A.H.D.

data selection

49 defects selected from a total of 429

discontinuity orientation: all

lithology type:

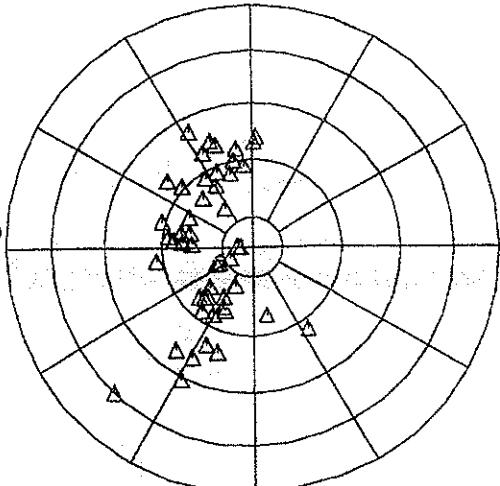
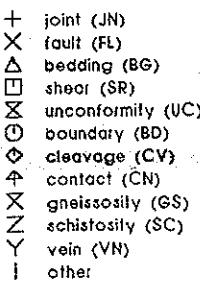
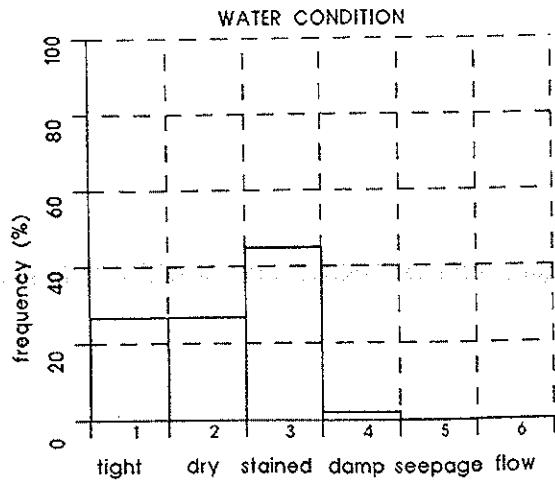
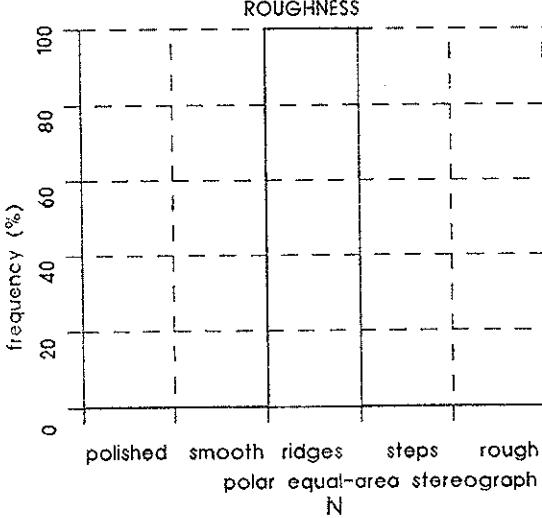
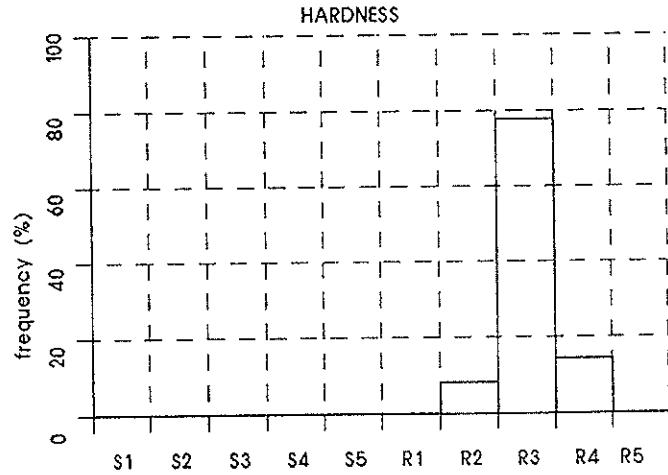
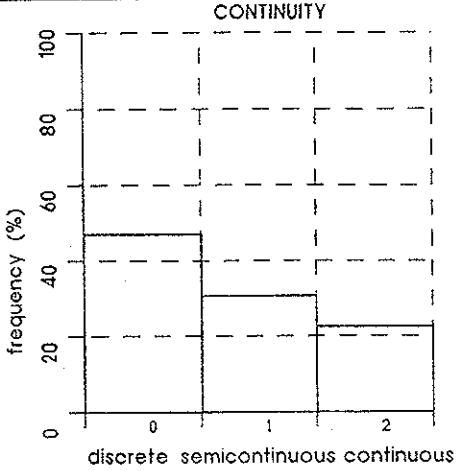
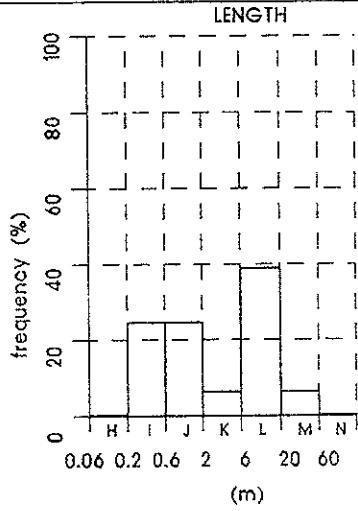
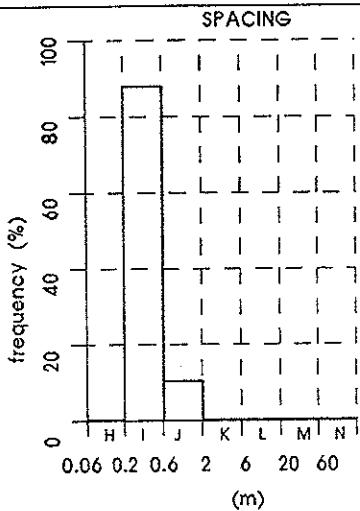
gth: all hardness: all

trend: mean, range

discontinuity type:

continuity: all water: all

plunge: mean, range



geotechnical line mapping data histograms

COFFEY



line no:

1989/3

sheet 1 of 1

office job no: S8463/4

date: 21-12-89

logged by: SRM

checked by: PLV

client: HORNSBY SHIRE COUNCIL
principal:
project: OLD MANS VALLEY
location: HORNSBY QUARRY

traverse line data

identification: TRAVERSE

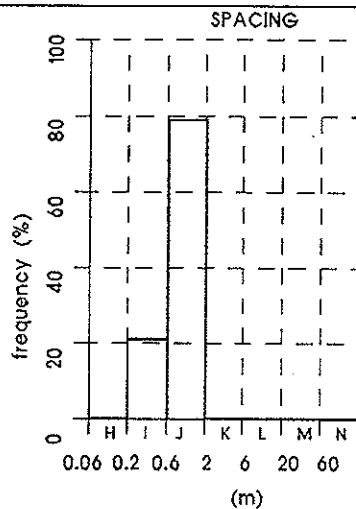
elevation: APPROX. RL. 40M

datum: A.H.D.

data selection

lithology type: all length: all hardness: all
discontinuity type: BG continuity: all water: all

discontinuity orientation: all
trend: mean, range
plunge: mean, range

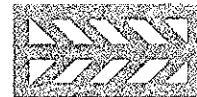




APPENDIX C

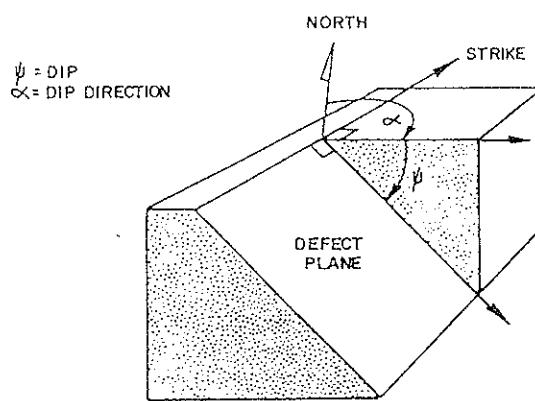
Coffey & Partners Pty. Ltd.

S8463/4-AD
3rd April, 1990

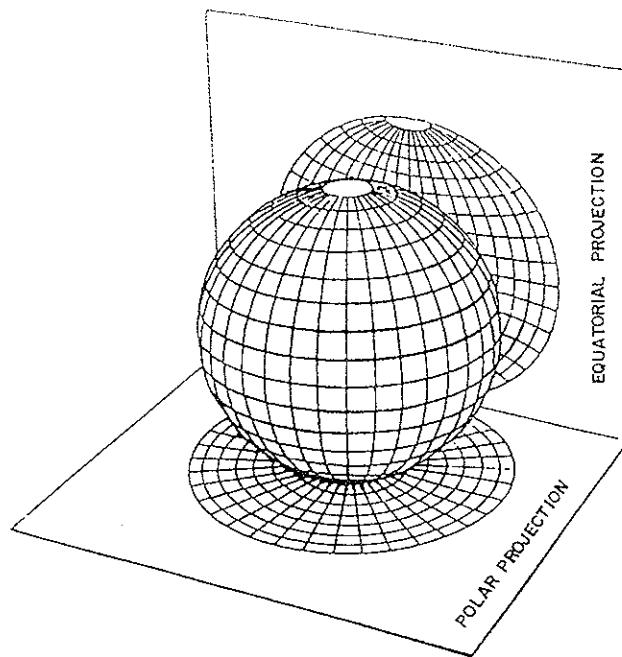


APPENDIX D

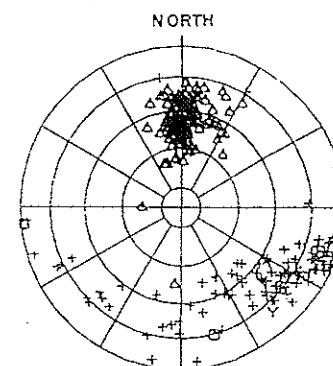
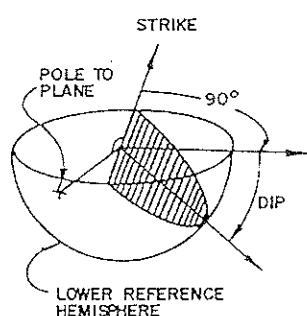
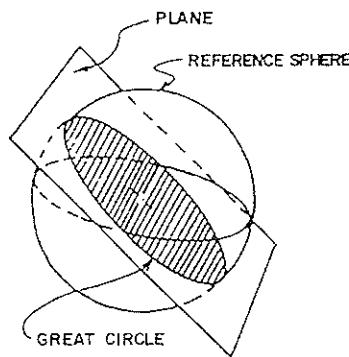
STEREOGRAPHIC PROJECTIONS FOR SURFACE LINE MAPPING



DEFINITION OF GEOMETRICAL TERMS

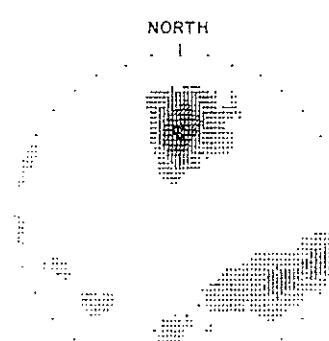
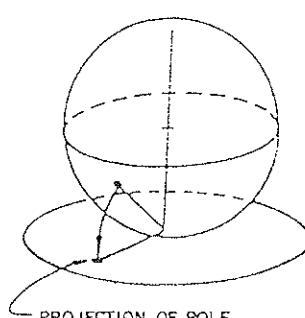


POLAR & EQUATORIAL PROJECTIONS



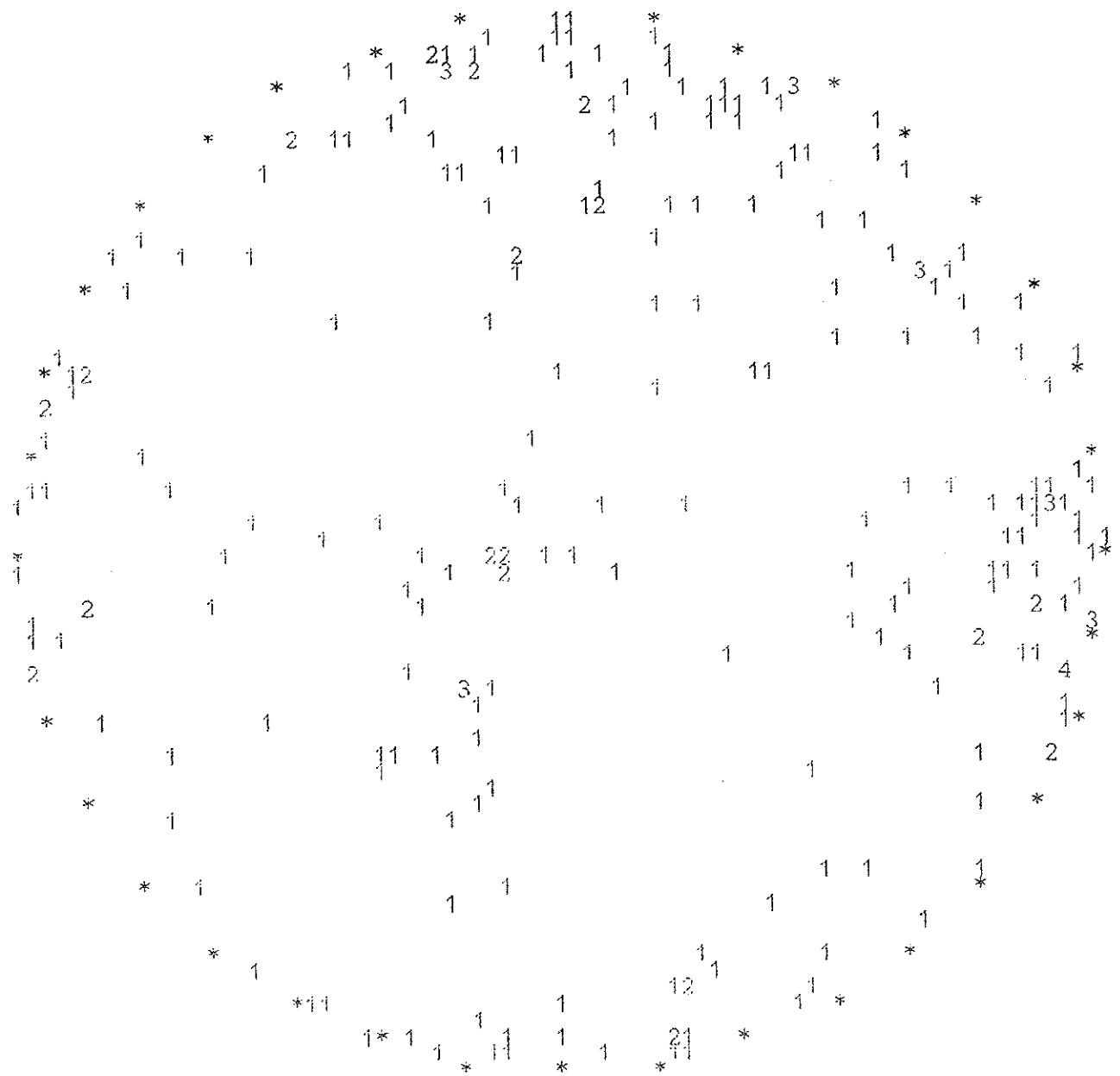
POLAR EQUAL-AREA STEREOGRAPHIC PROJECTION
DISPLAYING DEFECT TYPES

- +
- joint (JN)
- X
- fault (FL)
- △
- bedding (BG)
- shear (SR)
-
- unconformity (UC)
- ◊
- boundary (BD)
- ◆
- cleavage (CV)
-
- contact (CN)
- GS
- gneissosity (GS)
- SC
- schistosity (SC)
- VN
- vein (VN)
-
- other



EQUATORIAL EQUAL-AREA STEREOGRAPHIC PROJECTION
OF ABOVE CONTOURED

Coffey & Partners Pty Ltd		Consulting Engineers in the geotechnical sciences
drawn	PLV / LT	HORNSBY SHIRE COUNCIL OLD MANS VALLEY
approved		DEFINITION & PRESENTATION OF STRUCTURAL DEFECTS
date		
scale	NOT TO SCALE	COFFEY
		FIGURE DI
		job no S8463/4



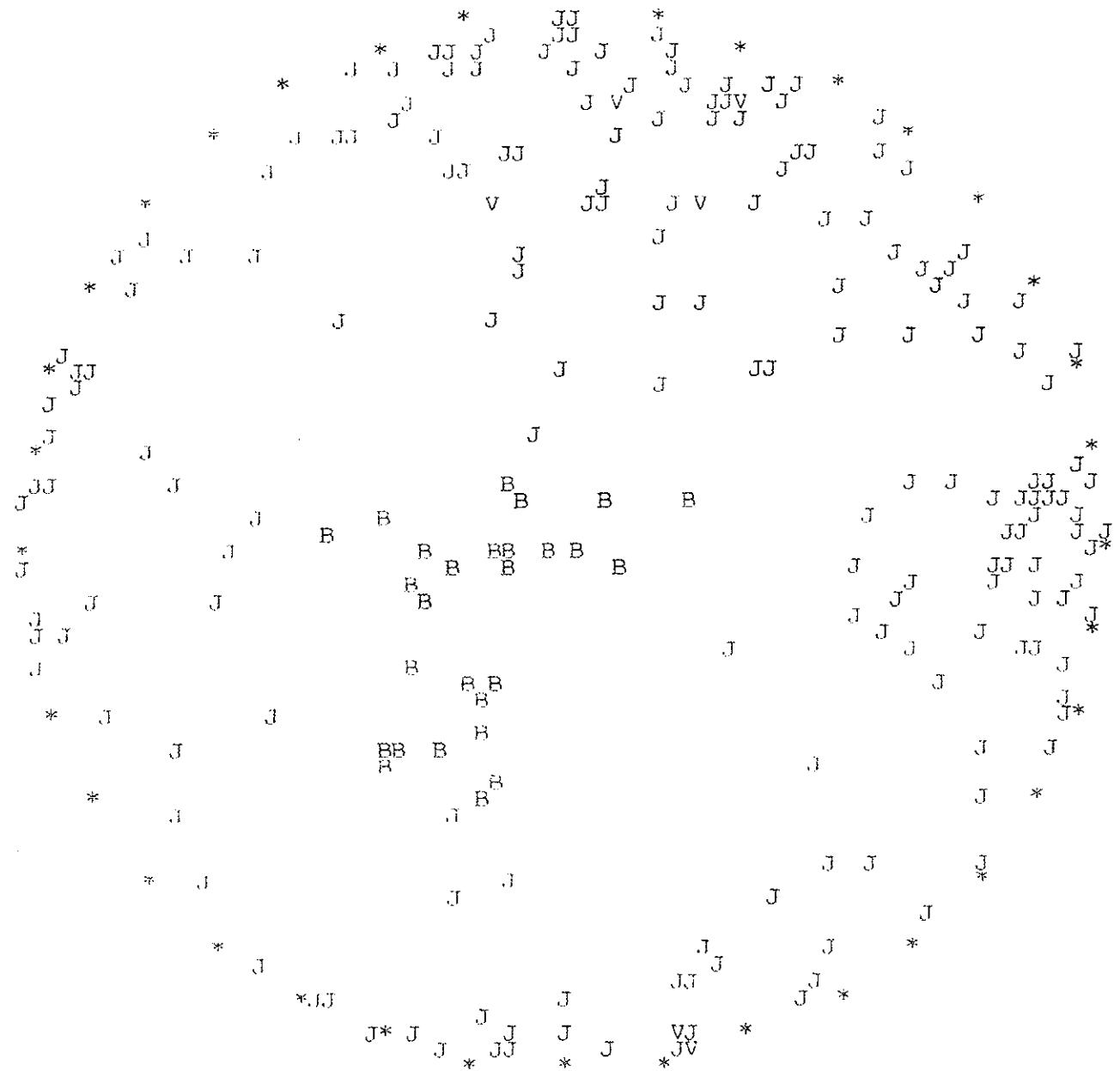
IS8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/1

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 252

ROTATION ANGLES: 0 0 0



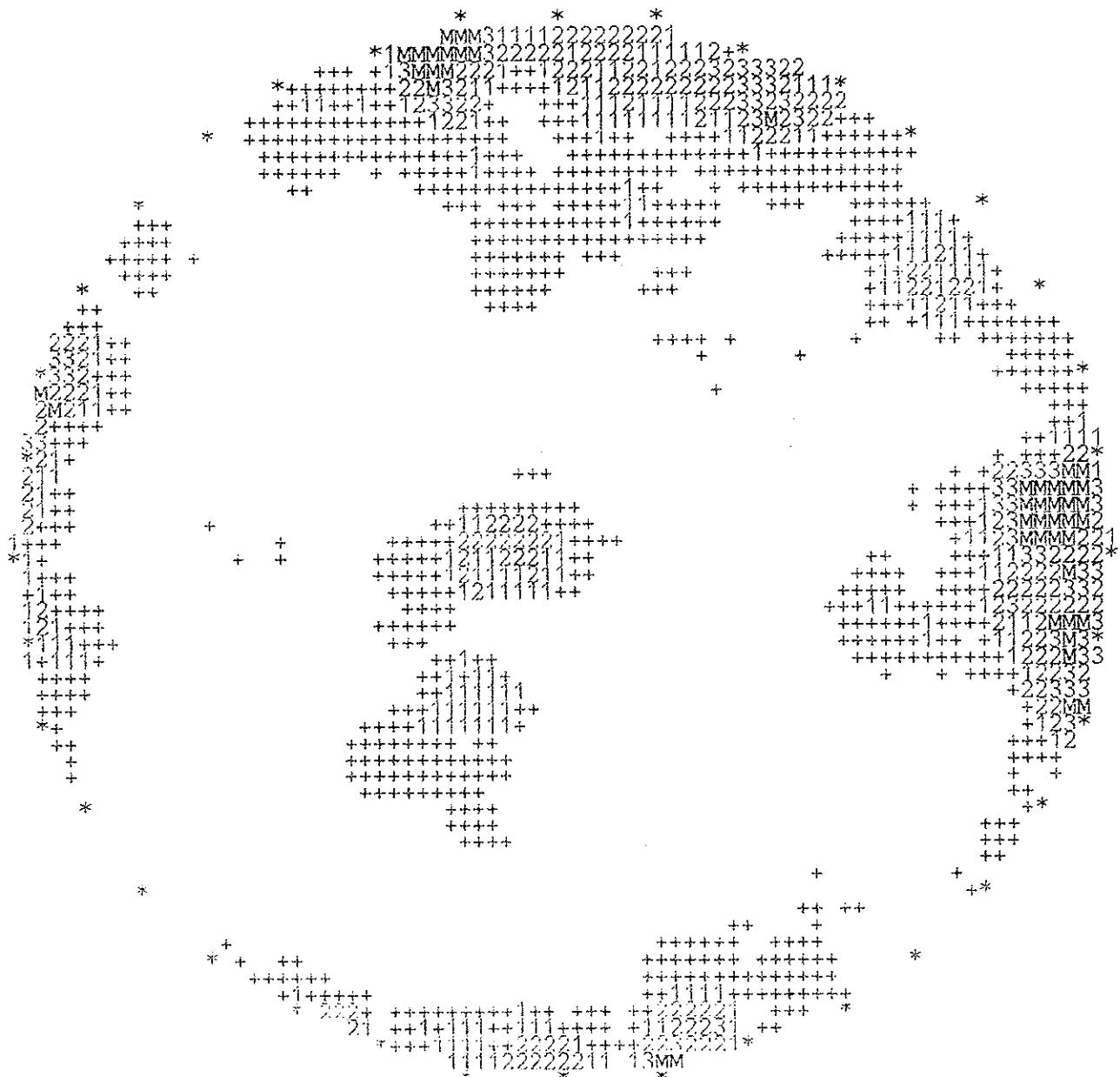
S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/1

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 252

ROTATION ANGLES: 0 0 0



88463/4 HORNSEY SHIRE (YOUNG) - TRAVERSE 1989/1

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

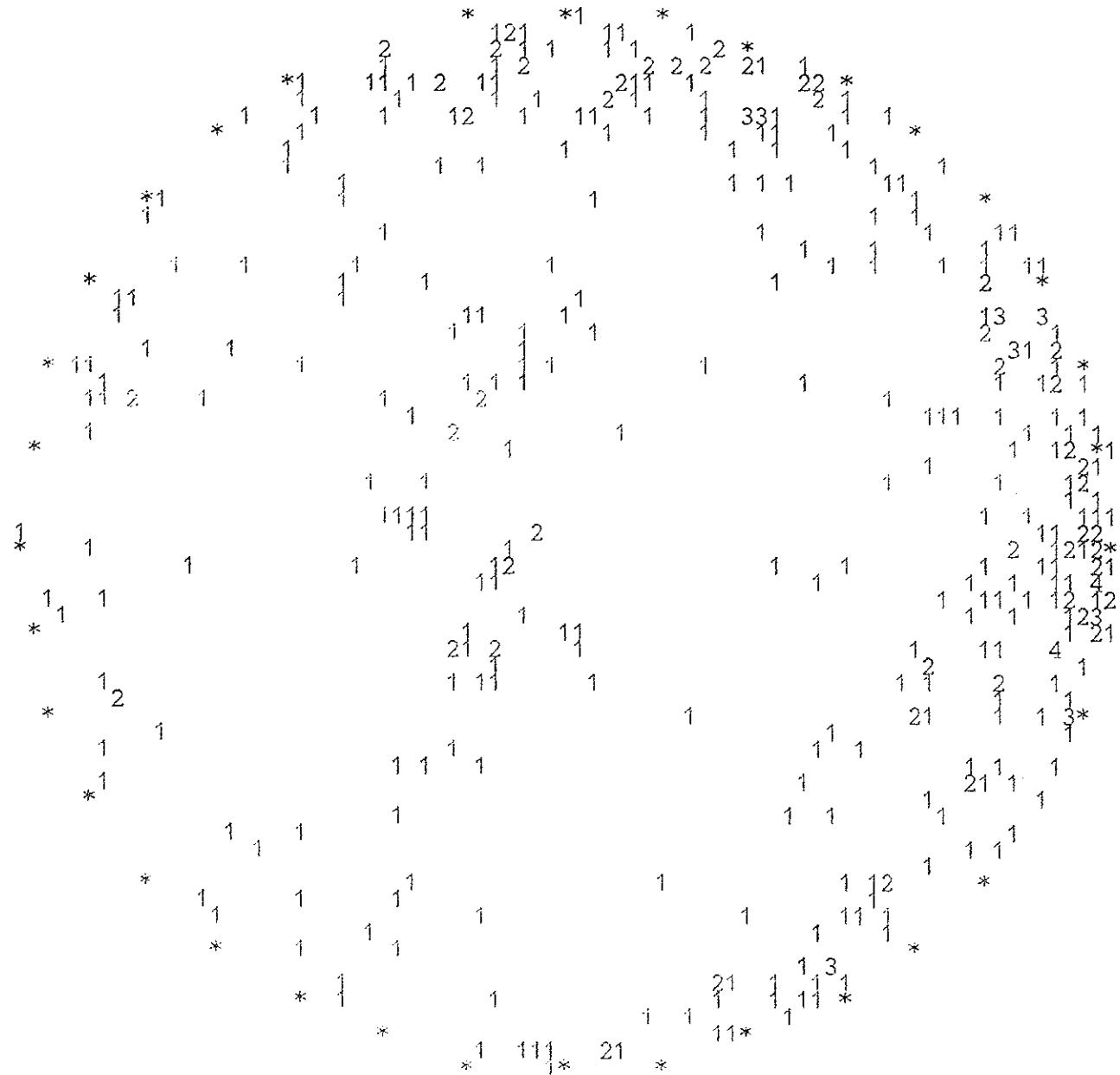
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 252

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<CLP>	1%
'+'	<CLP>	2*
'1'	<LT>	3%
'2'	<CLP>	4%
'3'	<LT>	5%
'M'	MAX =	6.7



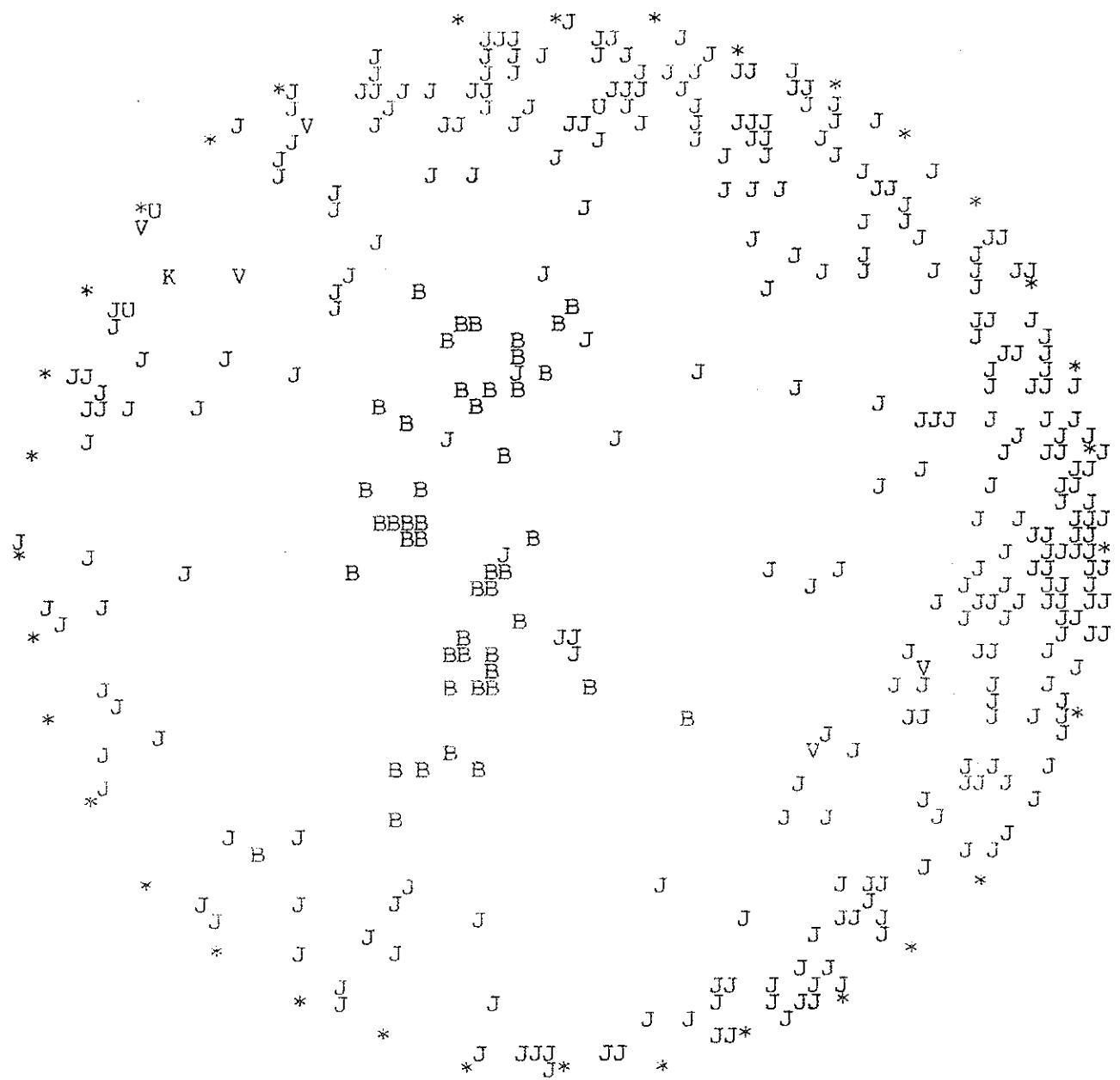
S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/2

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 429

ROTATION ANGLES: 0 0 0



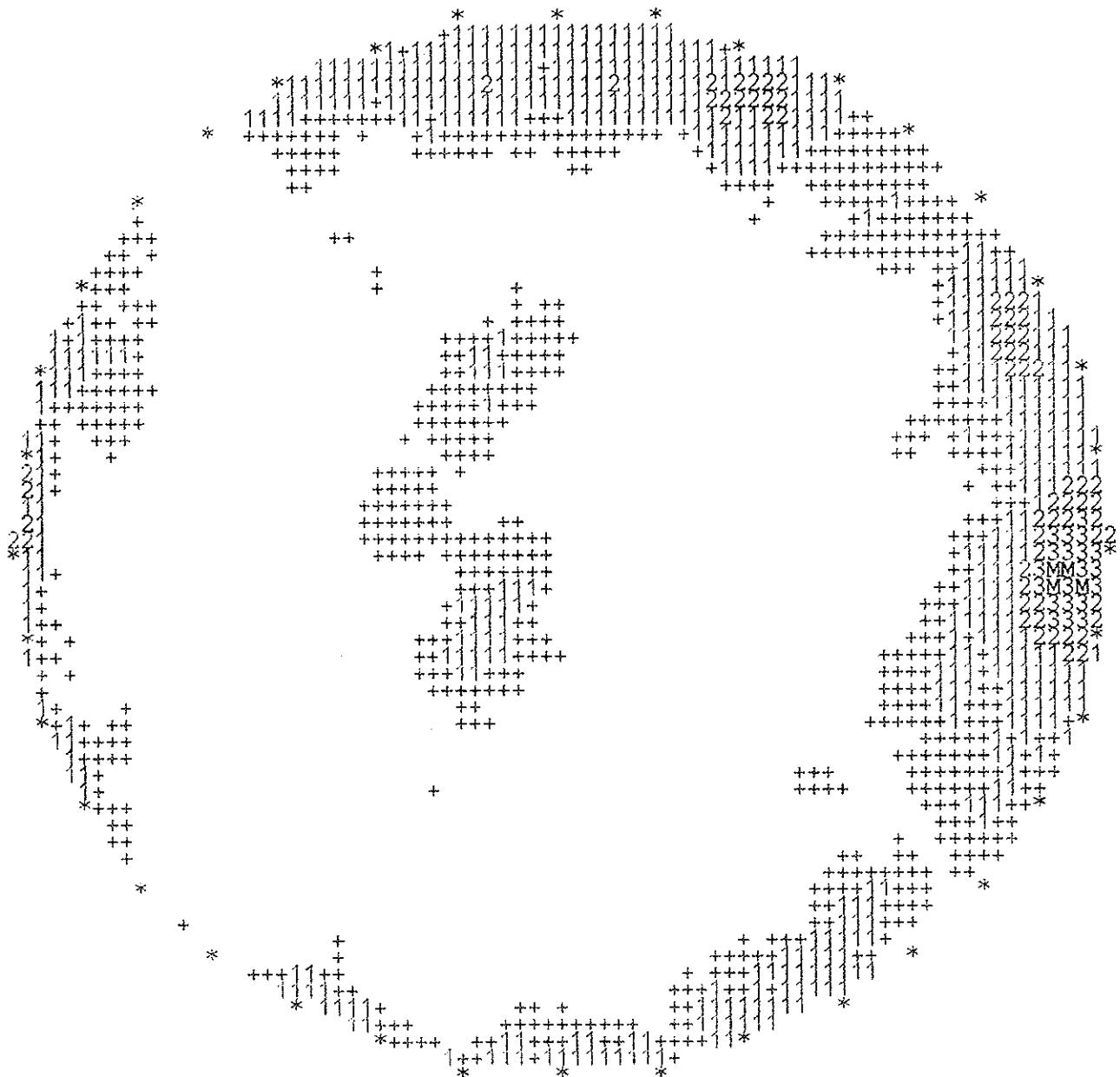
S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/2

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 429

ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/2

SCHMIDT METHOD - UNCORRECTED - POLES TO PLANES

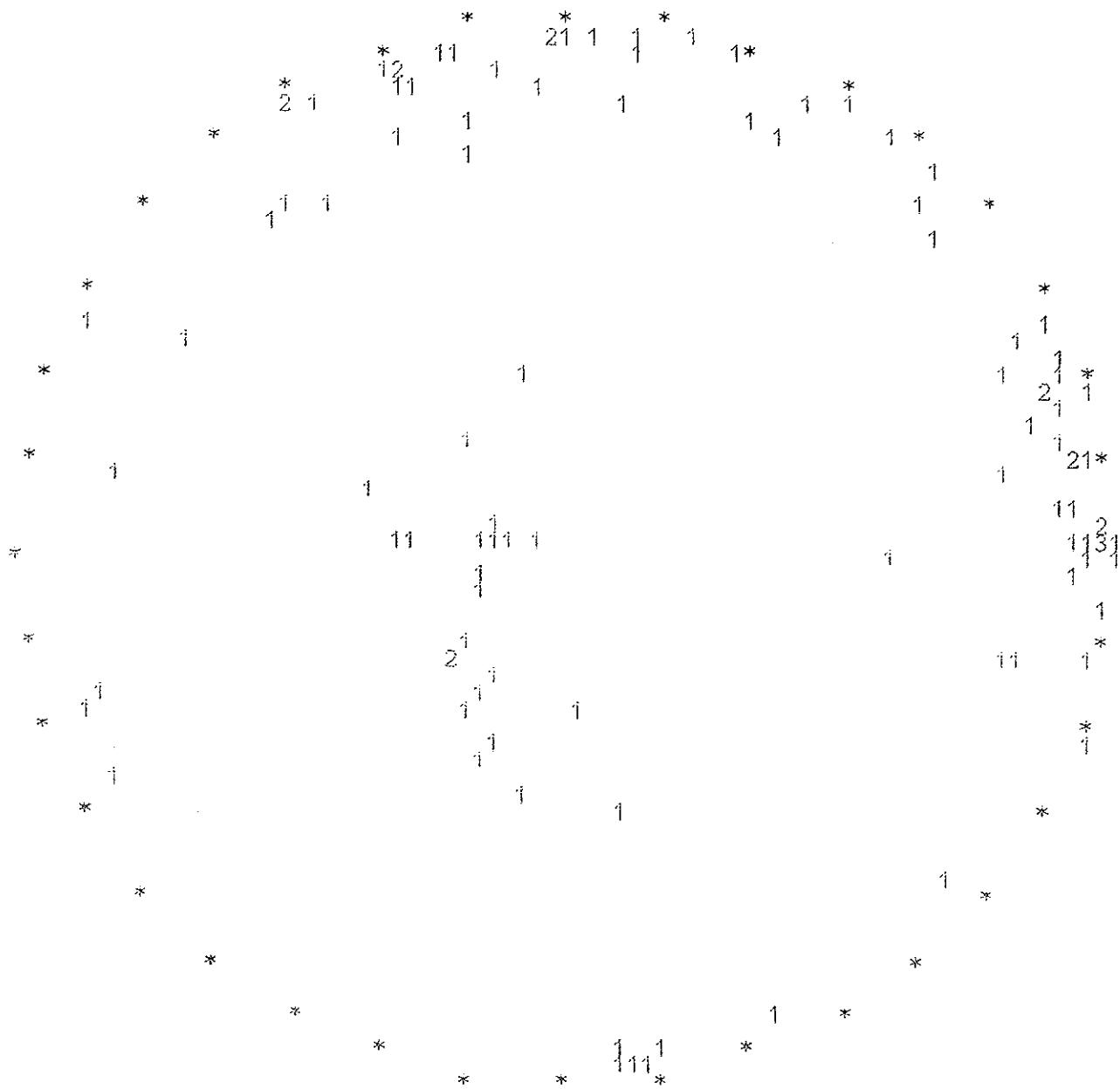
LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 429

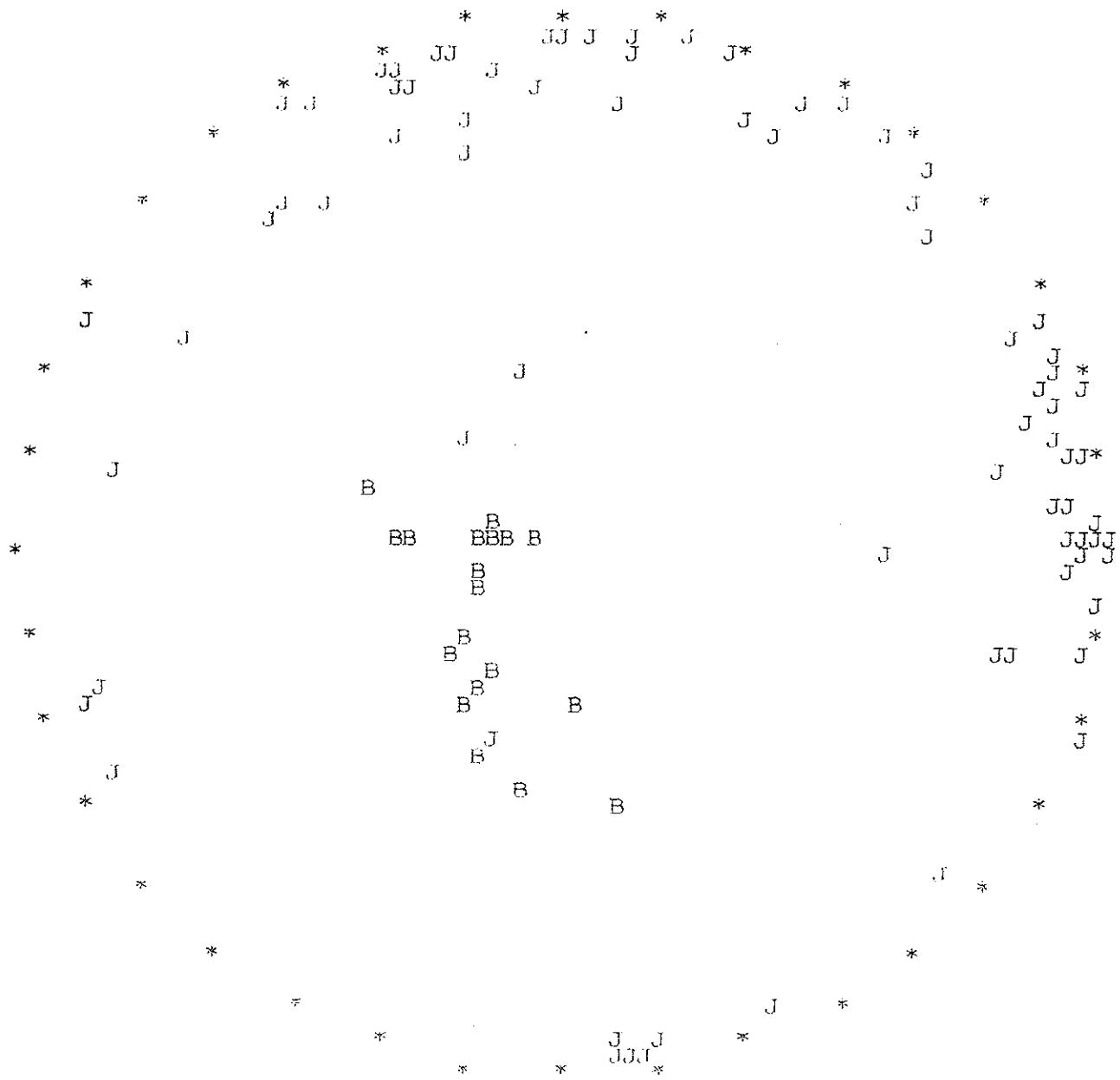
ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

'1'	<LT>	1%
'+'	<LT>	2%
'11'	<LT>	4%
'12'	<LT>	6%
'13'	<LT>	8%
'M'	MAX =	8.6



S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/3
 SCATTER DIAGRAM - POLES TO PLANES
 LOWER HEMISPHERE - EQUAL AREA PROJECTION
 NO. OF MEASURED POLES: 105
 ROTATION ANGLES: 0 0 0



S8463/4 HORNSBY SHIRE COUNCIL - TRAVERSE 1989/3

SCATTER DIAGRAM - POLES TO PLANES

LOWER HEMISPHERE - EQUAL AREA PROJECTION

NO. OF MEASURED POLES: 105

ROTATION ANGLES: 0 0 0



S8463/4 HORNSEY SHIRE (MONOT) - TRAVERSE 1989/3

SIMILAR METHOD - UNCORRECTED - POLES TO PLANES

EARTH HEMISPHERE - EQUAL AREA PROJECTION

N. OF MEASURED POLES: 105

ROTATION ANGLES: 0 0 0

SHADING SYMBOLS

\wedge	$\langle CLP \rangle$	1*
\wedge^+	$\langle CLP \rangle$	3*
$\wedge\wedge$	$\langle CLP \rangle$	6*
$\wedge\wedge$	$\langle CLP \rangle$	9*
$\wedge\wedge$	$\langle CLP \rangle$	12*
$\wedge\wedge$	MAX	= 12.4

Coffey & Partners Pty. Ltd.

S8463/4-AD
3rd April, 1990



APPENDIX E

TABULATION OF BEDDING, JOINT AND VEIN
ORIENTATIONS - CORED BOREHOLES

S8463/4-AD
3rd April, 1990



APPENDIX E
ORIENTATION OF BEDDING PLANE
PARTINGS IN CORED BOREHOLES

BOREHOLE NUMBER	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)
101	58.45	9	234
	59.2	15	260
	59.5	21	201
	59.6	17	196
	64.65	12	186
	65.70	18	136
	67.4	10	000
	68.0	29	352
	69.5	18	284
	69.8	19	282
	88.45	5	213
102	88.65	5	174
	13.35	28	122
	14.4	8	115
	14.5	10	115
	24.9	27	004
103	25.5	25	021
	77.65	20	194
	78.15	10	108
	80.35	10	100
	80.45	11	96
	81.35	9	106

S8463/4-AD
3rd April, 1990



APPENDIX E

ORIENTATION OF JOINTS IN

CORED BOREHOLES

BOREHOLE NUMBER	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)
101	28.0	12	224	28.2	35	201
	28.35	81	340	28.55	50	167
	28.70	35	102	28.85	70	107
	29.0	70	107	42.05	70	067
	42.3	30	342	42.9	69	079
	43.2	76	079	43.35	74	099
	43.55	80	295	43.65	82	302
	44.0	73	167	44.1	38	022
	50.2	80	015	50.3	79	010
	50.4	46	127	50.5	72	132
	50.6	54	337	50.7	88	59
	50.8	31	206	50.95	50	017
	51.25	55	059	51.35	87	059
	51.45	82	062	51.70	74	231
	52.10	76	224	52.25	72	000
	52.5	48	199	52.7	44	243
	52.9	35	239	53.2	69	224
	58.0	40	211	58.1	76	010
	58.2	81	040	58.3	78	094
	58.95	72	144	59.10	78	156
	60.3	61	119	60.5	89	039
	62.15	62	146	62.25	80	074
	62.3	46	272	64.3	81	213
	64.5	68	119	65.65	78	131
	66.3	62	144	66.4	61	151
	66.5	63	144	66.6	63	149
	67.9	15	297	71.5	18	198
	72.95	44	169	73.25	81	151
	73.85	83	017	81.3	83	064
	81.95	74	154	86.7	43	109
	88.25	40	176	88.75	35	135
	89.7	44	287	89.85	85	057

S8463/4-AD
3rd April, 1990

BOREHOLE NUMBER	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)
102	13.1	40	013	13.6	10	117
	13.8	75	253	14.1	48	316
	14.2	45	322	14.6	85	354
	14.7	44	319	14.8	77	214
	16.7	46	214	16.8	30	107
	17.1	39	219	17.4	28	125
	17.5	31	125	17.6	39	034
	17.7	38	031	17.8	35	029
	24.4	42	257	24.7	66	239
	25.95	60	284	26.75	67	349
	26.95	78	239	27.05	60	264
	27.05	60	264	27.90	40	041
	28.35	32	080	28.7	47	162
	28.8	21	036	29.0	73	132
	29.1	15	095	32.6	80	046
	32.7	47	344	38.7	64	324
	47.6	47	262	48.35	56	272
	49.0	49	269	61.3	56	080
	61.4	78	344	61.5	47	339
	61.6	43	339	62.2	74	322
	62.6	88	319	62.7	89	326
	62.9	43	322	64.0	30	026
	64.25	42	014	64.35	38	021
	64.45	38	021	64.65	84	262
	65.0	41	332	78.7	38	349
	78.85	31	336	79.0	30	339
	79.5	32	053	80.2	31	351
	80.75	36	349	80.85	34	349
	80.95	41	336	81.25	70	217
	81.55	8	034	81.85	60	276
	81.95	78	187	82.1	86	272
	82.2	86	272			
103	32.5	88	251	32.6	57	045
	32.75	85	276	32.85	44	096
	78.65	70	348	78.9	70	331
	79.4	68	009	79.6	67	006
	80.2	45	341	81.9	53	252

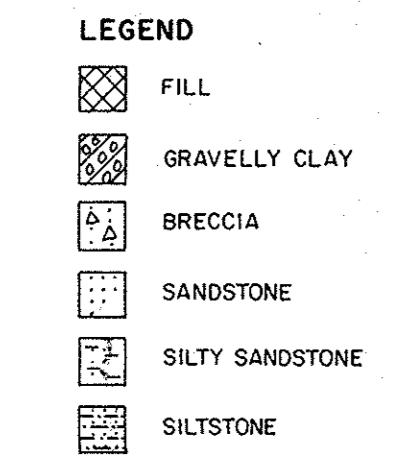
1
2
3
4
5
6
7
8
9
10
11
12
13
14
15
16
17
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
57
58
59
60
61
62
63
64
65
66
67
68
69
70
71
72
73
74
75
76
77
78
79
80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100

S8463/4-AD
3rd April, 1990

APPENDIX EORIENTATION OF CALCITE VEINSCORED BOREHOLES

BOREHOLE NUMBER	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)	DEPTH (m)	DIP ANGLE (deg)	DIP DIRECTION (deg/magnetic)
101	42.15	32	337	59.7	34	191
	59.8	31	120	59.9	33	204
	60.0	37	184	60.6	30	221
	60.85	88	029	61.40	32	034
	61.50	31	037	61.65	87	209
	61.90	19	191	62.7	32	017
	63.15	31	312	63.25	34	309
	63.35	72	049	63.45	33	317
	67.7	82	114	68.1	87	201
	68.7	30	234	69.6	82	074
	70.8	31	290	70.95	33	307
	71.2	32	037	71.35	78	193
	74.60	73	052	74.85	76	059
	76.2	75	062	77.2	73	054
	78.05	74	057	78.1	74	057
	81.85	80	106	82.7	81	184
	84.5	88	082	86.6	60	007
	88.55	70	292	88.95	87	094
	89.15	87	094	89.35	83	183
102	24.6	40	137	28.9	44	152
	61.7	74	269	61.9	78	274
	62.0	65	080	63.1	46	319
	63.65	47	324	65.2	42	319
	65.5	30	314	65.7	20	326





DEGREE OF WEATHERING

- EW EXTREMELY
- HW HIGHLY
- MW MODERATE
- SW SLIGHTLY
- Fr FRESH

GEOLOGICAL BOUNDARIES

- ACCURATE
- - APPROXIMATE
- ?— INFERRED

NOTE

FOR LOCATION OF CROSS-SECTIONS SEE
DRAWING NO S8463/4-1

